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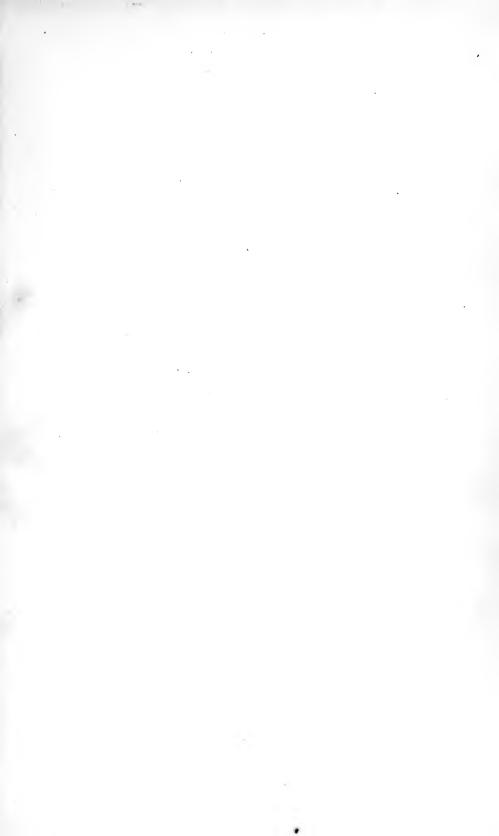
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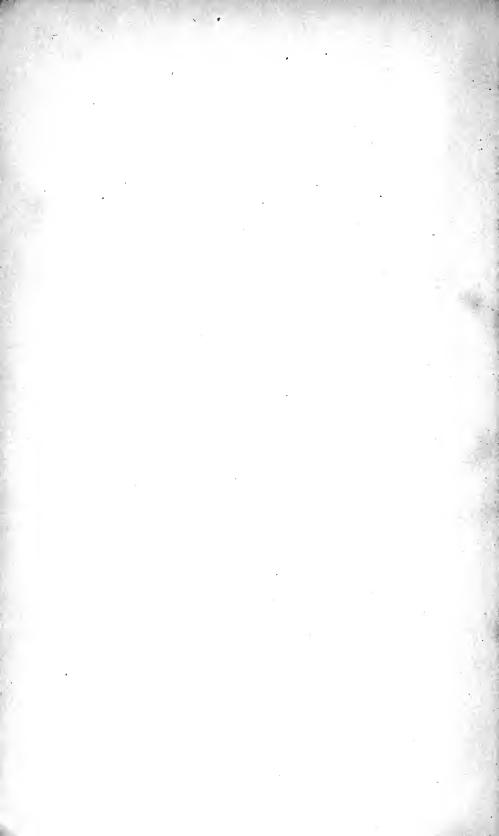
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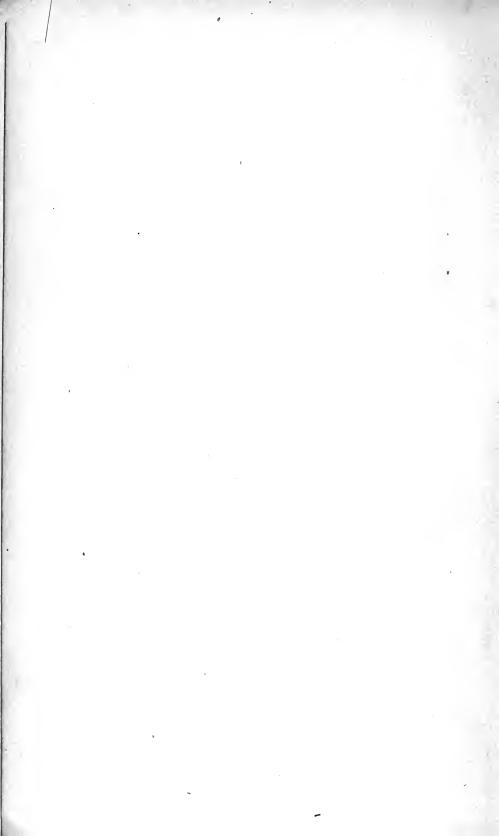
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OF

PLANE AND SPHERICAL

TRIGONOMETRY,

WITH THEIR APPLICATIONS TO

MENSURATION, SURVEYING, AND NAVIGATION.

BY ELIAS LOOMIS, LL.D.,

PROFESSOR OF NATURAL PHILOSOPHY AND ASTRONOMY IN YALE COLLEGE, AND AUTHOR OF A "COURSE OF MATHEMATICS."

TWENTY-FIFTH EDITION.

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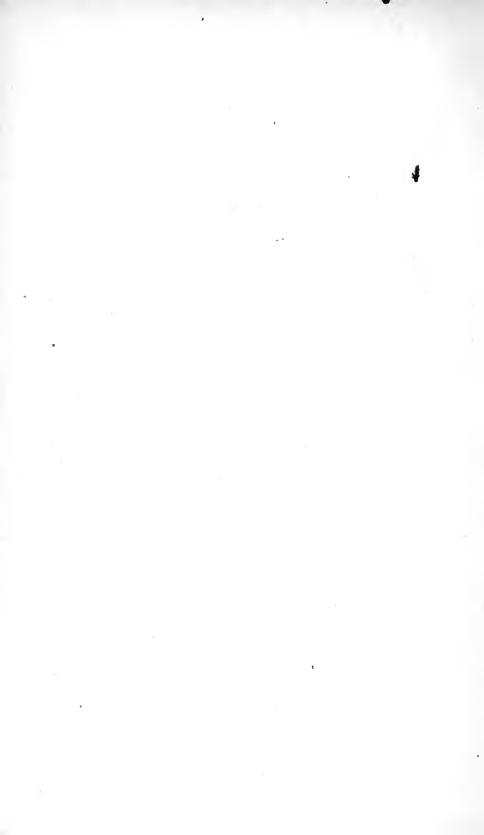
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PREFACE.

THE following treatise constitutes the third volume of a course of Mathematics designed for colleges and high schools, and is prepared upon substantially the same model as the works on Algebra and Geometry. It does not profess to embody every thing which is known on the subject of Trigonometry, but it contains those principles which are most important on account of their applications, or their connection with other parts of a course of mathematical study. The aim has been to render every principle intelligible, not by the repetition of superfluous words, but by the use of precise and appropriate Whenever it could conveniently be done, the most important principles have been reduced to the form of theorems or rules, which are distinguished by the use of italic letters, and are designed to be committed to memory. The most important instruments used in Surveying are fully described, and are illustrated by drawings.

The computations are all made by the aid of natural numbers, or with logarithms to six places; and by means of the accompanying tables, such computations can be performed with great facility and precision. This volume, having been used by several successive classes, has been subjected to the severest scrutiny, and the present edition embodies all the alterations which have been suggested by experience in the recitation room.



CONTENTS.

воок і.

THE NATURE AND PROPERTIES OF LOGARITHMS.	ts-e
Nature of Logarithms	7
Description of the Table of Logarithms	
Division by Logarithms	16
Involution by Logarithms	17
Evolution by Logarithms	
BOOK II.	
PLANE TRIGONOMETRY.	
Sines, Tangents, Secants, &c., defined	20
Explanation of the Trigonometrical Tables	
To find Sines and Tangents of small Arcs Solutions of Right-angled Triangles	
Solutions of Oblique-angled Triangles	
Instruments used in Drawing	42
Geometrical Construction of Triangles	
Trigonometrical Formulæ	
Computation of a Table of Sines, Cosines, &c	5 7
BOOK III.	
MENSURATION OF SURFACES AND SOLIDS.	
Areas of Figures bounded by Right Lines	59
Area of a Regular Polygon	64
Quadrature of the Circle and its Parts	
Rail-way Excavations or Embankments	
Regular Polyedrons	81
The three Round Bodies. Area of a Spherical Triangle.	
Area of a Spherical Triangle	03
BOOK IV.	
SURVEYING.	
Definitions	
Instruments for measuring Angles	91

CONTENTS.

v 1 0.1 v 1	Page 94
Explanation of the Vernier	94
Description of the Theodolite	97
Heights and Distances The Determination of Areas	103
Plotting a Survey	104
To find the Area of a Field	100
Trigonometrical Surveys	114
Variation of the Needle	117
	119
Leveling	123
Topographical Maps	123
Setting out Rail-way Curves	130
Surveying Harbors The Plane Table	132
To determine the Depth of Water.	133
10 determine the Depth of Water	199
BOOK V.	
NAVIGATION.	
Definitions, &c.	135
Plane Sailing	138
Traverse Sailing	141
Parallel Sailing	144
Middle Latitude Sailing	146
Mercator's Sailing	149
Nautical Charts	153
BOOK VI.	
SPHERICAL TRIGONOMETRY.	
Right-angled Spherical Triangles	155
Napier's Rule of the Circular Parts.	158
Examples of Right-angled Triangles	160
Oblique-angled Spherical Triangles	163
Examples of Oblique-angled Triangles	165
Trigonometrical Formulæ	171
Esiling on an Arc of a Great Circle	

TRIGONOMETRY.

* BOOK I.

THE NATURE AND PROPERTIES OF LOGARITHMS.

ARTICLE 1. Logarithms are numbers designed to diminish the labor of Multiplication and Division, by substituting in their stead Addition and Subtraction. All numbers are regarded as powers of some one number, which is called the *base* of the system; and the exponent of that power of the base which is equal to a given number, is called the logarithm of that number.

The base of the common system of logarithms (called, from their inventor, Briggs' logarithms) is the number 10. Hence all numbers are to be regarded as powers of 10. Thus, since $10^{\circ}=1$, 0 is the logarithm of 1 in Briggs' system;

$10^{\circ} = 1$,	0	is the	logarithm	of 1	in Briggs'	system
$10^{1}=10,$	1	"	"	10		66
$10^{\circ} = 100$,	2	"	"	100	"	44
$10^3 = 1000$,	3	"	"	1000	"	"
104=10000,	4	"	"	10,000	66	66
&c.,			&c.,		&c.	;

whence it appears that, in Briggs' system, the logarithm of every number between 1 and 10 is some number between 0 and 1, i. e., is a proper fraction. The logarithm of every number between 10 and 100 is some number between 1 and 2, i. e., is 1 plus a fraction. The logarithm of every number between 100 and 1000 is some number between 2 and 3, i. e., is 2 plus a fraction, and so on.

(2.) The preceding principles may be extended to fractions by means of negative exponents. Thus, since

$10^{-1}=0.1$,	-1 i	s th	e logarithm o	of 0.1	in Briggs'	system;
$10^{-2} = 0.01$,	-2	"	"	0.01	"	"
$10^{-3} = 0.001$,	-3	"	"	0.001	"	64
10-4=0.0001	-4	"		0.0001	. "	"
&c.,			&c., •		lio	

Hence it appears that the logarithm of every number between 1 and 0 1 is some number between 0 and -1, or may be represented by -1 plus a fraction; the logarithm of every number between 0.1 and .01 is some number between -1 and -2, or may be represented by -2 plus a fraction; the logarithm of every number between .01 and .001 is some number between -2 and -3, or is equal to -3 plus a fraction, and so on.

The logarithms of most numbers, therefore, consist of an in teger and a fraction. The integral part is called the *charac teristic*, and may be known from the following

Rule.

The characteristic of the logarithm of any number greater than unity, is one less than the number of integral figures in the given number.

Thus the logarithm of 297 is 2 plus a fraction; that is, the characteristic of the logarithm of 297 is 2, which is one less than the number of integral figures. The characteristic of the logarithm of 5673.29 is 3; that of 73254.1 is 4, &c.

The characteristic of the logarithm of a decimal fraction is a negative number, and is equal to the number of places by which its first significant figure is removed from the place of units.

Thus the logarithm of .0046 is -3 plus a fraction; that is, the characteristic of the logarithm is -3, the first significant figure, 4, being removed three places from units.

(3.) Since powers of the same quantity are multiplied by adding their exponents (Alg., Art. 50),

The logarithm of the product of two or more factors is equal to the sum of the logarithms of those factors.

Hence we see that if it is required to multiply two or more numbers by each other, we have only to add their logarithms: the sum will be the logarithm of their product. We then look in the table for the number answering to that logarithm, in order to obtain the required product.

Also, since powers of the same quantity are divided by subtracting their exponents (Alg., Art. 66),

The logarithm of the quotient of one number divided by an

other, is equal to the difference of the logarithms of those numbers.

Hence we see that if we wish to divide one number by another, we have only to subtract the logarithm of the divisor from that of the dividend; the difference will be the logarithm of their quotient.

(4.) Since, in Briggs' system, the logarithm of 10 is 1, if any number be multiplied or divided by 10, its logarithm will be increased or diminished by 1; and as this is an integer, it will only change the characteristic of the logarithm, without affecting the decimal part. Hence

The decimal part of the logarithm of any number is the same as that of the number multiplied or divided by 10, 100, 1000, &c.

Thus,	the	logarithm	of 65430	is	4.815777;
	"	"	6543	is	3.815777;
	"	"	654.3	is	2.815777;
	"	"	65.43	is	1.815777;
	"	"	6.543	is	0.815777;
	"	"	6543	is	$\bar{1}.815777;$
	"	"	06543	is	$\bar{2}.815777;$
	"	46	.006543	is	$\bar{3}.815777.$

The minus sign is here placed *over* the characteristic, to show that *that* alone is negative, while the decir; all part of the logarithm is positive.

TABLE OF LOGARITHMS.

(5.) A table of logarithms usually contains the logarithms of the entire series of natural numbers from 1 up to 10,000, and the larger tables extend to 100,000 or more. In the smaller tables the logarithms are usually given to five or six decimal places; the larger tables extend to seven, and sometimes eight or more places.

In the accompanying table, the logarithms of the first 100 numbers are given with their characteristics; but, for all other numbers, the decimal part only of the logarithm is given, while the characteristic is left to be supplied, according to the rule in Art. 2.

(6.) To find the Logarithm of any Number between 1 and 100

Look on the first page of the accompanying table, along the column of numbers under N., for the given number, and against it, in the next column, will be found the logarithm with its characteristic. Thus,

opposite 13 is 1.113943, which is the logarithm of 13; 65 is 1.812913, " 65.

To find the Logarithm of any Number consisting of three Figures.

Look on one of the pages of the table from 2 to 20, along the left-hand column, marked N., for the given number, and against it, in the column headed 0, will be found the decimal part of its logarithm. To this the characteristic must be prefixed, according to the rule in Art. 2. Thus

the logarithm of 347 will be found, from page 8, 2.540329; " " 871 " 18, 2.940018.

As the first two figures of the decimal are the same for several successive numbers in the table, they are not repeated for each logarithm separately, but are left to be supplied. Thus the decimal part of the logarithm of 339 is .530200. The first two figures of the decimal remain the same up to 347; they are therefore omitted in the table, and are to be supplied.

To find the Logarithm of any Number consisting of four Figures.

Find the three left-hand figures in the column marked N., as before, and the fourth figure at the head of one of the other columns. Opposite to the first three figures, and in the column under the fourth figure, will be found four figures of the logarithm, to which two figures from the column headed 0 are to be prefixed, as in the former case. The characteristic must be supplied according to Art. 2. Thus

the logarithm of 3456 is 3.538574; " 8765 is 3.942752.

In several of the columns headed 1, 2, 3, &c., small dots are found in the place of figures. This is to show that the two figures which are to be prefixed from the first column have changed, and they are to be taken from the horizontal line di-

N. J. S.

rectly below. The place of the dots is to be supplied with ciphers. •Thus

the logarithm of 2045 is 3.310693; " 9777 is 3.990206.

The two leading figures from the column 0 must also be taken from the horizontal line below, if any dots have been passed over on the same horizontal line. Thus

the logarithm of 1628 is 3.211654.

To find the Logarithm of any Number containing more than four Figures.

(7.) By inspecting the table, we shall find that, within certain limits, the differences of the logarithms are nearly proportional to the differences of their corresponding numbers. Thus

the logarithm of 7250 is 3.860338;

" 7251 is 3.860398; " 7252 is 3.860458;

" 7253 is 3.860518.

Here the difference between the successive logarithms, called the tabular difference, is constantly 60, corresponding to a difference of unity in the natural numbers. If, then, we suppose the logarithms to be proportional to their corresponding numbers (as they are nearly), a difference of 0.1 in the numbers should correspond to a difference of 6 in the logarithms; a difference of 0.2 in the numbers should correspond to a difference of 12 in the logarithms, &c. Hence

the logarithm of 7250.1 must be 3.860344; " 7250.2 " 3.860350;

3.860356.

7250.3

In order to facilitate the computation, the tabular difference is inserted on page 16 in the column headed D., and the proportional part for the fifth figure of the natural number is given at the bottom of the page. Thus, when the tabular difference is 60, the corrections for .1, .2, .3, &c., are seen to be 6, 12, 18, &c.

If the given number was 72501, the characteristic of its logarithm would be 4, but the decimal part would be the same as for 7250.1.

If it were required to find the correction for a sixth figure

in the natural number, it is readily obtained from the Proportional Parts in the table. The correction for a figure in the sixth place must be one tenth of the correction for the same figure if it stood in the fifth place. Thus, if the correction for .5 is 30, the correction for .05 is obviously 3.

As the differences change rapidly in the first part of the table, it was found inconvenient to give the proportional parts for each tabular difference; accordingly, for the first seven pages, they are only given for the *even* differences, but the proportional parts for the odd differences will be readily found by inspection.

Required the logarithm of 452789.

The logarithm of 452700 is 5.655810.

The tabular difference is 96.

Accordingly, the correction for the fifth figure, 8, is 77, and for the sixth figure, 9, is 8.6, or 9 nearly. Adding these corrections to the number before found, we obtain 5.655896.

The preceding logarithms do not pretend to be perfectly exact, but only the nearest numbers limited to six decimal places. Accordingly, when the fraction which is omitted exceeds half a unit in the sixth decimal place, the last figure must be increased by unity.

Required the logarithm of 8765432.

. The logarithr	n of 8765000 is	6.942752
Correction for	the fifth figure, 4,	20
"	" sixth figure, 3,	1.5
. "	" seventh figure, 2,	0.1
Therefore the loga	rithm of 8765432 is	$\overline{6.942774}$.
Required the logar	rithm of 234567.	
The logarithm	n of 234500 is	5.370143
Correction for	the fifth figure, 6,	111
"	" sixth figure, 7,	13
Therefore the loga	rithm of 234567 is	5.370267.

To find the Logarithm of a Decimal Fraction

(8.) According to Art. 4, the decimal part of the logarithm of any number is the same as that of the number multiplied or divided by 10, 100, 1000, &c. Hence, for a decimal frac-

tion, we find the logarithm as if the figures were integers, and prefix the characteristic according to the rule of Art. 2.

Examples.

The	logarithm of	345.6	is	2.538574;
"	"	87.65	is	1.942752;
"		2.345	is	0.370143;
"	"	.1234	is	$\bar{1}.091315$;
66	66	.005678	is	$\bar{3}.754195.$

To find the Logarithm of a Vulgar Fraction.

(9.) We may reduce the vulgar fraction to a decimal, and find its logarithm by the preceding article; or, since the value of a fraction is equal to the quotient of the numerator divided by the denominator, we may, according to Art. 3, subtract the logarithm of the denominator from that of the numerator; the difference will be the logarithm of the fraction.

Ex. 1. Find the logarithm of $\frac{3}{16}$, or 0.1875.

From the logarithm of 3, 0.477121, Take the logarithm of 16, 1.204120.

Leaves the logarithm of $\frac{3}{16}$, or .1875, $\overline{1}$.273001.

Ex. 2. The logarithm of $\frac{4}{55}$ is $\bar{2}.861697$.

Ex. 3. The logarithm of $\frac{1}{8} \frac{2}{7} \frac{3}{6}$ is $\overline{1}.147401$.

To find the Natural Number corresponding to any Logarithm.

(10.) Look in the table, in the column headed 0, for the first two figures of the logarithm, neglecting the characteristic; the other four figures are to be looked for in the same column, or in one of the nine following columns; and if they are exactly found, the first three figures of the corresponding number will be found opposite to them in the column headed N., and the fourth figure will be found at the top of the page. This number must be made to correspond with the characteristic of the given logarithm by pointing off decimals or annexing ciphers. Thus the natural number belonging to the log. 4.370143 is 23450:

" " 1.538574 is 34.56.

If the decimal part of the logarithm can not be exactly found in the table, look for the nearest less logarithm, and take out the four figures of the corresponding natural number as before; the additional figures may be obtained by means of the Proportional Parts at the bottom of the page.

Required the number belonging to the logarithm 4.368399. On page 6, we find the next less logarithm .368287.

The four corresponding figures of the natural number are 2335. Their logarithm is less than the one proposed by 112. The tabular difference is 186; and, by referring to the bottom of page 6, we find that, with a difference of 186, the figure corresponding to the proportional part 112 is 6. Hence the five figures of the natural number are 23356; and, since the characteristic of the proposed logarithm is 4, these five figures are all integral.

Required the number belonging to logarithm 5.345678. The next less logarithm in the table is 345570. Their difference is 108.

The first four figures of the natural number are 2216.

With the tabular difference 196, the fifth figure, corresponding to 108, is seen to be 5, with a remainder of 10. To find the sixth figure corresponding to this remainder 10, we may multiply it by 10, making 100, and search for 100 in the same line of proportional parts. We see that a difference of 100 would give us 5 in the fifth place of the natural number. Therefore, a difference of 10 must give us 5 in the sixth place of the natural number. Hence the required number is 221655

In the same manner we find

the number corresponding to log. 3.538672 is 3456.78;

" " 1.994605 is 98.7654; " " 1.647817 is .444444

MULTIPLICATION BY LOGARITHMS.

(11.) According to Art. 3, the logarithm of the product of two or more factors is equal to the sum of the logarithms of those factors. Hence, for multiplication by logarithms, we have the following

RULE.

Add the logarithms of the factors; the sum will be the log writhm of their product.

Ex. 1. Required the product of 57.98 by 18.

The logarithm of 57.98 is 1.763278 is 1.255273

The logarithm of the product 1043.64 is 3.018551

Ex. 2. Required the product of 397.65 by 43.78.

Ans., 17409.117.

Ex. 3. Required the continued product of 54.32, 6.543, and 12.345.

The word sum, in the preceding rule, is to be understood in its algebraic sense; therefore, if any of the characteristics of the logarithms are negative, we must take the difference between their sum and that of the positive characteristics, and prefix the sign of the greater. It should be remembered that the decimal part of the logarithm is invariably positive; hence that which is carried from the decimal part to the characteristic must be considered positive.

Ex. 4. Multiply 0.00563 by 17.

The logarithm of 0.00563 is $\overline{3}$,750508

" 17 is 1.230449

Product, 0.09571, whose logarithm is $\overline{2.980957}$.

Ex. 5. Multiply 0.3854 by 0.0576. Ans., 0.022199.

Ex. 6. Multiply 0.007853 by 0.00476.

Ans., 0.00003738.

Ex. 7. Find the continued product of 11.35, 0.072, and 0.017. (12.) Negative quantities may be multiplied by means of

logarithms in the same manner as positive, the proper sign being prefixed to the result according to the rules of Algebra. To distinguish the negative sign of a natural number from the negative characteristic of a logarithm, we append the letter n to the logarithm of a negative factor. Thus

the logarithm of -56 we write 1.748188 n.

Ex. 8. Multiply 53.46 by -29.47.

The logarithm of 53.46 is 1.728029

" -29.47 is 1.469380 n.

Product, -1575.47, log. 3.197409 n.

Ex. 9. Find the continued product of 372.1, -.0054, and -.175.6.

Ex. 10. Find the continued product of -0.137, -7.689, and -0.0376.

DIVISION BY LOGARITHMS

(13.) According to Art. 3, the logarithm of the quotient of one number divided by another is equal to the difference of the logarithms of those numbers. Hence, for division by logarithms, we have the following

RULE.

From the logarithm of the dividend, subtract the logarithm of the divisor; the difference will be the logarithm of the quotient.

Ex. 1. Required the quotient of 888.7 divided by 42.24.

The logarithm of 888.7 is 2.948755

" 42.24 is 1.625724

The quotient is 21.039, whose log. is 1.323031.

Ex. 2. Required the quotient of 3807.6 divided by 13.7.

Ans., 277.927.

The word difference, in the preceding rule, is to be understood in its algebraic sense; therefore, if the characteristic of one of the logarithms is negative, or the lower one is greater than the upper, we must change the sign of the subtrahend, and proceed as in addition. If unity is carried from the decimal part, this must be considered as positive, and must be united with the characteristic before its sign is changed.

Ex. 3. Required the quotient of 56.4 divided by 0.00015.

The logarithm of 56.4 is 1.751279
" 0.00015 is 4.176091

The quotient is 376000, whose log. is 5.575188.

This result may be verified in the same way as subtraction in common arithmetic. The remainder, added to the subtrahend, should be equal to the minuend. This precaution should always be observed when there is any doubt with regard to the sign of the result.

Ex. 4. Required the quotient of .8692 divided by 42.258.

Ans.

Ex. 5. Required the quotient of .74274 divided by .00928. Ex. 6. Required the quotient of 24.934 divided by .078541 Negative quantities may be divided by means of logarithms

in the same manner as positive, the proper sign being prefixed to the result according to the rules of Algebra.

Ex. 7. Required the quotient of -79.54 divided by 0.08321

Ex. 8. Required the quotient of -0.4753 divided by -36.74.

INVOLUTION BY LOGARITHMS.

(14.) It is proved in Algebra, Art. 340, that the logarithm of any power of a number is equal to the logarithm of that number multiplied by the exponent of the power. Hence, to involve a number by logarithms, we have the following

RULE.

Multiply the logarithm of the number by the exponent of the power required.

Ex. 1. Required the square of 428.

The logarithm of 428 is 2.631444

 2^{\cdot}

Square, 183184, log. 5.262888.

Ex. 2. Required the 20th power of 1.06.

The logarithm of 1.06 is 0.025306

20

20th power, 3.2071, log. 0.506120.

Ex. 3. Required the 5th power of 2.846.

It should be remembered, that what is carried from the decimal part of the logarithm is positive, whether the characteristic is positive or negative.

Ex. 4. Required the cube of .07654.

The logarithm of .07654 is $\overline{2}.883888$

3

Cube, .0004484, $\log \frac{\overline{4.651664}}{1.651664}$.

Ex. 5. Required the fourth power of 0.09874.

Ex. 6. Required the seventh power of 0.8952.

EVOLUTION BY LOGARITHMS.

(15.) It is proved in Algebra, Art. 341, that the logarithm of any root of a number is equal to the logarithm of that number divided by the index of the root. Hence, to extract the oot of a number by logarithms, we have the following

RULE.

Divide the logarithm of the number by the index of the root required.

Ex. 1. Required the cube root of 482.38.

The logarithm of 482.38 is 2.683389.

Dividing by 3, we have 0.894463, which corresponds to 7.842, which is therefore the root required.

Ex. 2. Required the 100th root of 365.

Ans., 1.0608.

When the characteristic of the logarithm is negative, and is not divisible by the given divisor, we may increase the characteristic by any number which will make it exactly divisible, provided we prefix an equal positive number to the decimal part of the logarithm.

Ex. 3. Required the seventh root of 0.005846.

The logarithm of 0.005846 is $\bar{3}.766859$, which may be written $\bar{7}+4.766859$.

Dividing by 7, we have $\overline{1}.680980$, which is the logarithm of 4797, which is, therefore, the root required.

This result may be verified by multiplying $\overline{1}.680980$ by 7, the result will be found to be $\overline{3}.766860$.

Ex. 4. Required the fifth root of 0.08452.

Ex. 5. Required the tenth root of 0.007815.

PROPORTION BY LOGARITHMS.

(16.) The fourth term of a proportion is found by multiply ing together the second and third terms, and dividing by the first. Hence, to find the fourth term of a proportion by logarithms,

Add the logarithms of the second and third terms, and from their sum subtract the logarithm of the first term.

Ex. 1. Find a fourth proportional to 72.34, 2.519, and 357.48

Ans., 12.448.

(17.) When one logarithm is to be subtracted from another, it may be more convenient to convert the subtraction into an addition, which may be done by first subtracting the given logarithm from 10, adding the difference to the other logarithm and afterward rejecting the 10.

The difference between a given logarithm and 10 is called its complement; and this is easily taken from the table by beginning at the left hand, subtracting each figure from 9, except the last significant figure on the right, which must be subtracted from 10.

To subtract one logarithm from another is the same as to add its complement, and then reject 10 from the result. For u-b is equivalent to 10-b+a-10.

To work a proportion, then, by logarithms, we must Add the complement of the logarithm of the first term to the logarithms of the second and third terms.

The characteristic must afterward be diminished by 10.

Ex. 2. Find a fourth proportional to 6853, 489, and 38750.

The complement of the logarithm of 6853 is 6.164119

The logarithm of 489 is 2.689309 " 38750 is 4.588272

The fourth term is 2765, whose logarithm is 3.441700.

One advantage of using the complement of the first term in working a proportion by logarithms is, that it enables us to exhibit the operation in a more compact form.

Ex. 3. Find a fourth proportional to 73.84, 658.3, and 4872.

Ans.

Ex. 4. Find a fourth proportional to 5.745, 781.2, and 54.27

BOOK II.

PLANE TRIGONOMETRY.

(18.) Trigonometry is the science which teaches how to determine the several parts of a triangle from having certain parts given.

Plane Trigonometry treats of plane triangles; Spherical Trigonometry treats of spherical triangles.

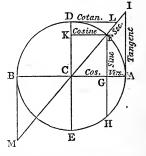
(19.) The circumference of every circle is supposed to be divided into 360 equal parts, called degrees; each degree into 60 minutes, and each minute into 60 seconds. Degrees, minutes, and seconds are designated by the characters °, ', ". Thus 23° 14′ 35" is read 23 degrees, 14 minutes, and 35 seconds.

Since an angle at the center of a circle is measured by the arc intercepted by its sides, a right angle is measured by 90°, two right angles by 180°, and four right angles are measured by 360°.

(20.) The complement of an arc is what remains after sub-

tracting the arc from 90°. Thus the arc DF is the complement of AF. The complement of 25° 15′ is 64° 45′.

In general, if we represent any arc by A, its complement is $90^{\circ}-A$. Hence, if an arc is greater than 90° , its complement must be negative. Thus, the complement of 100° 15' is -10° 15'. Since the two acute angles of a right-angled triangle are to-



gether equal to a right angle, each of them must be the complement of the other.

(21.) The supplement of an arc is what remains after subtracting the arc from 180°. Thus the arc BDF is the supplement of the arc AF. The supplement of 25° 15′ is 154° 45′.

In general, if we represent any are by A, its supplement is

- 180° —A. Hence, if an arc is greater than 180° , its supplement must be negative. Thus the supplement of 200° is -20° . Since in every triangle the sum of the three angles is 180° , either angle is the supplement of the sum of the other two.
- (22.) The sine of an arc is the perpendicular let fall from one extremity of the arc on the radius passing through the other extremity. Thus FG is the sine of the arc AF, or of the angle ACF.

Every sine is half the chord of double the arc. Thus the sine FG is the half of FH, which is the chord of the arc FAH, double of FA. The chord which subtends the sixth part of the circumference, or the chord of 60°, is equal to the radius (Geom., Prop. IV., B. VI.); hence the sine of 30° is equal to half of the radius.

- (23.) The *versed sine* of an arc is that part of the diameter intercepted between the sine and the arc. Thus GA is the versed sine of the arc AF.
- (24). The tangent of an arc is the line which touches it at one extremity, and is terminated by a line drawn from the center through the other extremity. Thus AI is the tangent of the arc AF, or of the angle ACF.
- (25.) The secant of an arc is the line drawn from the center of the circle through one extremity of the arc, and is limited by the tangent drawn through the other extremity.

Thus CI is the secant of the arc AF, or of the angle ACF.

(26.) The *cosine* of an arc is the sine of the complement of that arc. Thus the arc DF, being the complement of AF, FK is the sine of the arc DF, or the cosine of the arc AF.

The cotangent of an arc is the tangent of the complement of that arc. Thus DL is the tangent of the arc DF, or the cotangent of the arc AF.

The cosecant of an arc is the secant of the complement of that arc. Thus CL is the secant of the arc DF, or the cosecant of the arc AF.

In general, if we represent any angle by A, cos. $A=sine (90^{\circ}-A)$. cot. $A=tang. (90^{\circ}-A)$. cosec. $A=sec. (90^{\circ}-A)$.

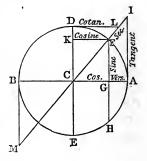
Since, in a right-angled triangle, either of the acute angles

is the complement of the other, the sine, tangent, and secant of one of these angles is the cosine, cotangent, and cosecan of the other.

(27.) The sine, tangent, and secant of an arc are equal to the sine, tangent, and secant of its supplement. Thus FG is

the sine of the arc AF, or of its supplement, BDF. Also, AI, the tangent of the arc AF, is equal to BM, the tangent of the arc BDF. And CI, the secant of the arc AF, is equal to CM, the secant of the arc BDF.

The versed sine of an acute angle, ACF, is equal to the radius *minus* the cosine CG. The versed sine of an obtuse angle, BCF, is equal to radius *plus* the cosine CG; that is, to BG.



- (28.) The relations of the sine, cosine, &c., to each other, may be derived from the proportions of the sides of similar triangles. Thus the triangles CGF, CAI, CDL, being similar, we have,
- 1. CG: GF:: CA: AI; that is, representing the arc by A, and the radius of the circle by R, cos. A: sin. A:: R: tang. A.

Whence tang.
$$A = \frac{R \sin. A}{\cos. A}$$
.

2. CG :: CF : CA : CI; that is, cos. A : R :: R : sec. A. Whence sec. $A = \frac{R^2}{\cos A}$.

3 GF: CG:: CD: DL; that is, sin. A: cos. A:: R: cot. A

Whence cot. $A = \frac{R \cos. A}{\sin. A}$.

4 GF: CF:: CD: CL; that is, sin. A:R::R: cosec. A.

Whence cosec. A=\frac{R^2}{\sin. A}.

5. AI: AC:: CD: DL; that is, tang. A: R:: R: cot. A.

Whence tang. A. = $\frac{R^2}{\cot A}$.

The preceding values of tangent and cotangent, secant and cosecant will be frequently referred to hereafter, and should be carefully committed to memory.

Also, in the right-angled triangle CGF, we find CG²+GF³=UF²; that is, sin. ²A+cos. ²A=R²; or,

The square of the sine of an arc, together with the square of its cosine, is equal to the square of the radius.

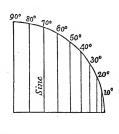
Hence sin.
$$A=\pm\sqrt{R^2-\cos^2 A}$$
.
And cos. $A=\pm\sqrt{R^2-\sin^2 A}$.

(29.) A table of *natural sines*, tangents, &c., is a table giving the lengths of those lines for different angles in a circle whose radius is unity.

Thus, if we describe a circle with a radius of one inch, and divide the circumference into equal parts of ten degrees, we shall find

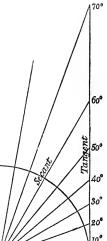
the sine of 10° equals 0.174 inch;

"	"	20°	"	0.342	"
"	"	30°	"	0.500	"
"	"	40°	"	0.643	"
"	"	50°	"	0.766	. "
"	"	60°	"	0.866	"
"	"	70°	"	0.940	"
"	"	80°	"	0.985	"
60	66	90°	66	1.000	"



If we draw the tangents of the same arcs, we shall find the tangent of 10° equals 0.176 inch;

	0		1		
"	66	20°	66	0.364	"
"	"	30°	"	0.577	"
"	"	40°	66	0.839	"
"	66	45°	"	1.000	"
"	"	50°	"	1.192	"
66	"	60°	"	1.732	"
46	"	70°	66	2.747	"
66	"	80°	"	5.671	"
"	"	90°	"	infinit	e.



Also, if we draw the secants of the same arcs, we shall find that

the secant of 10° equals 1.015 inch;

"	"	20°	"	1.064	66
46	"	90°	"	1.155	"
66	66	40°	"	1.305	66

the secant of 50° equals 1.556 inch;
" " 60° " 2.000 "
" " 70° " 2.924 "
" " 80° " 5.759 "
" " 90° " infinite.

In the accompanying table, pages 116-133, the sines, cosines, tangents, and cotangents are given for every minute of the quadrant to six places of figures.

(30.) To find from the table the natural sine, cosine, &c., of an arc or angle.

If a sine is required, look for the degrees at the top of the page, and for the minutes on the left; then, directly under the given number of degrees at the top of the page, and opposite to the minutes on the left, will be found the sine required. Since the radius of the circle is supposed to be unity, the sine of every arc below 90° is less than unity. The sines are expressed in decimal parts of radius; and, although the decimal point is not written in the table, it must always be prefixed. As the first two figures remain the same for a great many numbers in the table, they are only inserted for every ten minutes, and the vacant places must be supplied from the two leading figures next preceding. Thus, on

page 120, the sine of 25° 11′ is 0.425516;
page 126, " " 51° 34′ is 0.783332, &c.

The tangents are found in a similar manner. Thus
the tangent of 31° 44′ is 0.618417;
" " 65° 27′ is 2.18923.

The same number in the table is both the sine of an arc and the cosine of its complement. The degrees for the cosines must be sought at the bottom of the page, and the minutes on the right. Thus,

on page 130, the cosine of 16° 42′ is 0.957822; on page 118, " " 73° 17′ is 0.287639, &c.

The cotangents are found in the same manner. Thus the cotangent of 19° 16′ is 2.86089; " 54° 53′ is 0.703246.

It is not necessary to extend the tables beyond a quadrant, because the sine of an angle is equal to that of its supplement (Art. 27). Thus

```
the sine of 143° 24′ is 0.596225; 

" cosine of 151° 23′ is 0.877844; 

" tangent of 132° 36′ is 1.08749; 

" cotangent of 116° 7′ is 0.490256, &c.
```

(31.) If a sine is required for an arc consisting of degrees, minutes, and *seconds*, we must make an allowance for the seconds in the same manner as was directed in the case of logarithms, Art. 7; for, within certain limits, the differences of the sines are proportional to the differences of the corresponding arcs. Thus

```
the sine of 34° 25′ is .565207; " " 34° 26′ is .565447.
```

The difference of the sines corresponding to one minute of arc, or 60 seconds, is .000240. The proportional part for 1' is found by dividing the tabular difference by 60, and the quotient, .000004, is placed at the bottom of page 122, in the column headed 34°. The correction for any number of seconds will be found by multiplying the proportional part for 1" by the number of seconds.

Required the natural sine of 34° 25′ 37″.

The proportional part for 1", being multiplied by 37, becomes 148, which is the correction for 37". Adding this to the sine of 34° 25', we find

```
the sine of 34^{\circ}\ 25'\ 37'' is .565355.
```

Since the proportional part for 1" is given to hundredths of a unit in the sixth place of figures, after we have multiplied by the given number of seconds, we must reject the last two figures of the product.

In the same manner we find

the cosine of 56° 34' 28'' is .550853.

It will be observed, that since the cosines decrease while the arcs increase, the correction for the 28" is to be subtracted from the cosine of 56° 34".

In the same manner we find

```
the natural sine of 27° 17′ 12″ is 0.458443;

" " cosine of 45° 23′ 23″ is 0.702281;

" tangent of 63⁴ 32′ 34″ is 2.00945;

" cotangent of 81° 48′ 56″ is 0.143825
```

(32.) To find the number of degrees, minutes, and seconds telonging to a given sine or tangent.

If the given sine or tangent is found exactly in the table, the corresponding degrees will be found at the top of the page, and the minutes on the left hand. But when the given number is not found exactly in the table, look for the sine or tangent which is next less than the proposed one, and take out the corresponding degrees and minutes. Find, also, the difference between this tabular number and the number proposed, and divide it by the proportional part for 1" found at the bot tom of the page; the quotient will be the required number of seconds.

Required the arc whose sine is .750000.

The next less sine in the table is .749919, the arc corresponding to which is 48° 35′. The difference between this sine and that proposed is 81, which, divided by 3.21, gives 25. Hence the required arc is 48° 35′ 25″.

In the same manner we find

the arc whose tangent is 2.00000 is 63° 26′ 6″.

If a cosine or cotangent is required, we must look for the number in the table which is next greater than the one proposed, and then proceed as for a sine or tangent. Thus

the arc whose cosine is .40000 is 66° 25′ 18″; " " cotangent is 1.99468 is 26° 37′ 34″.

(33.) On pages 134-5 will be found a table of natural secants for every ten minutes of the quadrant, carried to seven places of figures. The degrees are arranged in order in the first vertical column on the left, and the minutes at the top of the page. Thus

the secant of 21° 20′ is 1.073561; " " 81° 50′ is 7.039622.

If a secant is required for a number of minutes not given in the table, the correction for the odd minutes may be found by means of the last vertical column on the right, which shows the proportional part for one minute.

Let it be required to find the secant of 30° 33'

The secant of 30° 30′ is 1.160592.

The correction for 1' is 198.9, which, multiplied by 3, be-

comes 597. Adding this to the number before found, we obtain 1.161189.

For a cosecant, the degrees must be sought in the righthand vertical column, and the minutes at the bottom of the page. Thus

the cosecant of 47° 40′ is 1.352742; " 38° 33′ is 1.604626.

(34.) When the natural sines, tangents, &c., are used in proportions, it is necessary to perform the tedious operations of multiplication and division. It is, therefore, generally preferable to employ the *logarithms* of the sines; and, for convenience, these numbers are arranged in a separate table, called *logarithmic sines*, &c. Thus

the natural sine of $14^{\circ} 30'$ is 0.250380. Its logarithm, found from page 6, is $\overline{1}.398600$.

The characteristic of the logarithm is negative, as must be the case with all the sines, since they are less than unity. To avoid the introduction of negative numbers in the table, we increase the characteristic by 10, making 9.398600, and this is the number found on page 38 for the logarithmic sine of 14° 30′. The radius of the table of logarithmic sines is therefore, properly, 10,000,000,000,000, whose logarithm is 10.

(35.) The accompanying table contains the logarithmic sines and tangents for every ten seconds of the quadrant. The degrees and seconds are placed at the top of the page, and the minutes in the left vertical column. After the first two degrees, the three leading figures in the table of sines are only given in the column headed 0", and are to be prefixed to the numbers in the other columns, as in the table of logarithms of numbers. Also, where the leading figures change, this change is indicated by dots, as in the former table. The correction for any number of seconds less than 10 is given at the bottom of the page.

(36.) To find the logarithmic sine or tangent of a given arc.

Look for the degrees at the top of the page, the minutes on the left hand, and the next less number of seconds at the top; then, under the seconds, and opposite to the minutes, will be tound four figures, to which the three leading figures are to be prefixed from the column headed 0"; to this add the proportional part for the odd seconds at the bottom of the page.

Required the logarithmic sine of 24° 27′ 34″.

The logarithmic sine of 24° 27′ 30″ is 9.617033 Proportional part for 4″ is 18

Logarithmic sine of 24° 27′ 34″ is 9.617051.

Required the logarithmic tangent of 73° 35′ 43″.

The logarithmic tangent 73° 35′ 40″ is 10.531031
Proportional part for 3″ is 23

Logarithmic tangent of 73° 35′ 43″ is 10.531054.

When a cosine is required, the degrees and seconds must be sought at the bottom of the page, and the minutes on the right, and the correction for the odd seconds must be subtracted from the number in the table.

Required the logarithmic cosine of 59° 33′ 47″.

The logarithmic cosine of 59° 33′ 40″ is 9.704682 Proportional part for 7″ is 25

Logarithmic cosine of 59° 33′ 47″ is 9.704657.

So, also, the logarithmic cotangent of 37° 27′ 14″ is found to be 10.115744.

It will be observed that for the cosines and cotangents, the seconds are numbered from 10" to 60", so that if it is required to find the cosine of 25° 25′ 0" we must look for 25° 24′ 60"; and so, also, for the cotangents.

(37.) The proportional parts given at the bottom of each page correspond to the degrees at the top of the page, increased by 30', and are not strictly applicable to any other number of minutes; nevertheless, the differences of the sines change so slowly, except near the commencement of the quadrant, that the error resulting from using these numbers for every part of the page will seldom exceed a unit in the sixth decimal place. For the first two degrees, the differences change so rapidly that the proportional part for 1" is given for each minute in the right-hand column of the page. The correction for any number of seconds less than ten will be found by multiplying the proportional part for 1" by the given number of seconds.

Required the logarithmic sine of 1° 17′ 33″.

The logarithmic sine of 1° 17' 30'' is 8.352991.

The correction for 3" is found by multiplying 93.4 by 3 which gives 280. Adding this to the above tabular number, we obtain for

the sine of 1° 17′ 33″, 8.353271.

A similar method may be employed for several of the first degrees of the quadrant, if the proportional parts at the bottom of the page are not thought sufficiently precise. This correction may, however, be obtained pretty nearly by inspection, from comparing the proportional parts for two successive degrees. Thus, on page 26, the correction for 1", corresponding to the sine of 2° 30', is 48; the correction for 1", corresponding to the sine of 3° 30', is 34. Hence the correction for 1", corresponding to the sine of 3° 0', must be about 41; and, in the same manner, we may proceed for any other part of the table.

(38.) Near the close of the quadrant, the tangents vary so rapidly that the same arrangement of the table is adopted as for the commencement of the quadrant. For the last, as well as the first two degrees of the quadrant, the proportional part 10 1" is given for each minute separately. These proportional parts are computed for the minutes placed opposite to them, increased by 30", and are not strictly applicable to any other number of seconds; nevertheless, the differences for the most part change so slowly, that the error resulting from using these numbers for every part of the same horizontal line is quite small. When great accuracy is required, the table on page 114 may be employed for arcs near the limits of the quadrant. This table furnishes the differences between the logarithmic sines and the logarithms of the arcs expressed in seconds. Thus

the logarithmic sine of 0° 5', from page 22, is 7.162696 the logarithm of 300'' (=5') is 2.477121 the difference is 4.685575.

This is the number found on page 114, under the heading log. sine A-log. A'', opposite to 5 min.; and, in a similar manner, the other numbers in the same column are obtained. These numbers vary quite slowly for two degrees; and hence, to find the logarithmic sine of an arc less than two degrees we have

but to add the logarithm of the arc expressed in seconds to the appropriate number found in this table.

Required the logarithmic sine of 0° 7′ 22″.

Tabular number from page 114, 4.685575The logarithm of 442'' is 2.645422Logarithmic sine of 0° 7' 22" is 7.330997.

The logarithmic tangent of an arc less than two degrees is found in a similar manner.

Required the logarithmic tangent of 0° 27′ 36″.

 Tabular number from page 114,
 4.685584

 The logarithm of 1656" is
 3.219060

 The logarithm of 1656" is
 3.219060

Logarithmic tangent of 0° 27′ 36″ is 7.904644.

The column headed log. cot. A+log. A'', is found by adding the logarithmic cotangent to the logarithm of the arc expressed in seconds. Hence, to find the logarithmic cotangent of an arc less than two degrees, we must subtract from the tabular number the logarithm of the arc in seconds.

Required the logarithmic cotangent of 0° 27′ 36″.

 Tabular number from page 114,
 15.314416

 The logarithm of 1656" is
 3.219060

Logarithmic cotangent of 0° 27′ 36″ is 12.095356.

The same method will, of course, furnish cosines and cotan gents of arcs near 90°.

(39.) The secants and cosecants are omitted in this table, since they are easily derived from the cosines and sines. We

have found, Art. 28, secant $=\frac{R^2}{\text{cosine}}$; or, taking the logarithms,

log. secant = 2. log. R-log. cosine

=20-log. cosine.

Also, cosecant = $\frac{R^2}{\sin \theta}$

or log. cosecant =20-log. sine. That is,

The logarithmic secant is found by subtracting the logarithmic cosine from 20; and the logarithmic cosecant is found by subtracting the logarithmic sine from 20.

Thus we have found the logarithmic sine of $24^{\circ}\ 27'\ 34'$ to be 9.617051.

Hence the logarithmic cosecant of 24° 27′ 34" is 10.382949

The logarithmic cosine of 54° 12' 40" is 9.767008. Hence the logarithmic secant of 54° 12' 40" is 10.232992.

(40.) To find the arc corresponding to a given logarithmic sine or tangent.

If the given number is found exactly in the table, the corresponding degrees and seconds will be found at the top of the page, and the minutes on the left. But when the given number is not found exactly in the table, look for the sine or tangent which is next less than the proposed one, and take out the corresponding degrees, minutes, and seconds. Find, also, the difference between this tabular number and the number proposed, and corresponding to this difference, at the bottom of the page, will be found a certain number of seconds which is to be added to the arc before found.

Required the arc corresponding to the logarithmic sine 9.750000.

The next less sine in the table is 9.749987.

The arc corresponding to which is 34° 13′ 0″.

The difference between its sine and the one proposed is 13, corresponding to which, at the bottom of the page, we find 4'' nearly. Hence the required arc is 34° 13' 4".

In the same manner, we find the arc corresponding to logarithmic tangent 10.250000 to be 60° 38′ 57″.

When the arc falls within the first two degrees of the quadrant, the odd seconds may be found by dividing the difference between the tabular number and the one proposed, by the proportional part for 1". We thus find the arc corresponding to logarithmic sine 8.400000 to be 1° 26′ 22" nearly.

We may employ the same method for the last two degrees of the quadrant when a tangent is given; but near the limits of the quadrant it is better to employ the auxiliary table on page 114. The tabular number on page 114 is equal to log. sin. A—log. A". Hence log. sin. A—tabular number =log. A"; that is, if we subtract the corresponding tabular number on page 114, from the given logarithmic sine, the remainder will be the logarithm of the arc expressed in seconds.

Required the arc corresponding to logarithmic sine 7.000000. We see, from page 22, that the arc must be nearly 3'; the corresponding tabular number on page 114 is 4.685575

or

The difference is 2.314425.

which is the logarithm of 206."265.

Hence the required arc is 3' 26."265.

Required the arc corresponding to log. sine 8.000000.

We see from page 22, that the arc is about 34'. responding tabular number from page 114 is 4.685568, which, subtracted from 8.000000, leaves 3.314432, which is the logarithm of 2062."68. Hence the required arc is

34′ 22.′′68.

In the same manner, we find the arc corresponding to loga rithmic tangent 8.184608 to be 0° 52′ 35″.

SULUTIONS OF RIGHT-ANGLED TRIANGLES.

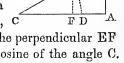
THEOREM I.

(41.) In any right-angled triangle, radius is to the hypothenuse as the sine of either acute angle is to the opposite side. or the cosine of either acute angle to the adjacent side.

Let the triangle CAB be right angled at A, then will

R:CB::sin. C:BA::cos. C:CA.

From the point C as a center, with a radius equal to the radius of the tables, C



describe the arc DE, and on AC let fall the perpendicular EF Then EF will be the sine, and CF the cosine of the angle C. Because the triangles CAB, CFE are similar, we have

CE : CB :: EF : BA,

or R:CB::sin. C:BA.Also, CE : CB :: CF : CA, R: CB:: cos. C: CA.

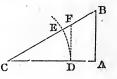
THEOREM II.

(42.) In any right-angled triangle, radius is to either side as the tangent of the adjacent acute angle is to the opposite side, or the secant of the same angle to the hypothenuse.

Let the triangle CAB be right angled at A, then will

R:CA::tang. C:AB::sec. C:CB.

From the point C as a center, with a radius equal to the radius of the tables,



describe the arc DE, and from the point D draw DF perpendicular to CA. Then DF will be the tangent, and CF the secant of the angle C. Because the triangles CAB, CDF are similar, we have CD: CA::DF:AB,

or R: CA:: tang. C: AB.
Also, CD: CA:: CF: CB,
or R: CA:: sec. C: CB.

(43.) In every plane triangle there are six parts: three sides and three angles. Of these, any three being given, provided one of them is a side, the others may be determined. In a right-angled triangle, one of the six parts, viz., the right angle, is always given; and if one of the acute angles is given, the other is, of course, known. Hence the number of parts to be considered in a right-angled triangle is reduced to four, any two of which being given, the others may be found.

It is desirable to have appropriate names by which to designate each of the parts of a triangle. One of the sides adjacent to the right angle being called the base, the other side adjacent to the right angle may be called the perpendicular. The three sides will then be called the hypothenuse, base, and perpendicular. The base and perpendicular are sometimes called the legs of the triangle. Of the two acute angles, that which is adjacent to the base may be called the angle at the base, and the other the angle at the perpendicular.

We may, therefore, have four cases, according as there are given,

- 1. The hypothenuse and the angles;
- 2. The hypothenuse and a leg;
- 3. One leg and the angles; or,
- 4. The two legs.

All of these cases may be solved by the two preceding theorems.

CASE I.

(44.) Given the hypothenuse and the angles, to find the base and perpendicular.

This case is solved by Theorem I.

Radius: hypothenuse:: sine of the angle at the base: perpendicular;

:: cosine of the angle at the base : base

Ex. 1. Given the hypothenuse 275, and the angle at the base 57° 23′, to find the base and perpendicular.

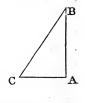
The natural sine of 57° 23' is .842296;

cosine " .539016.

Hence 1:275::.842296:231.631=AB.

1:275::.539016:148.229=AC.

The computation is here made by natural numbers. If we work the proportion by logarithms, we shall have



Radius,	10.000000
Is to the hypothenuse 275	2.439333
As the sine of C 57° 23'	9.925465
To the perpendicular 231.63	2.364798.
Also, Radius,	10.000000
Is to the hypothenuse 275	2.439333
As the cosine of C 57° 23'	9.731602
To the base 148.23	2 170935

Ex. 2. Given the hypothenuse 67.43, and the angle at the perpendicular 38° 43′, to find the base and perpendicular.

Ans. The base is 42.175, and perpendicular 52.612.

The student should work this and the following examples both by natural numbers and by logarithms, until he has made himself perfectly familiar with both methods. He may then employ either method, as may appear to him most expeditious

Case II.

(45.) Given the hypothenuse and one leg, to find the angles and the other leg.

This case is solved by Theorem I.

Hypothenuse: radius::base: cosine of the angle at the base.
Radius: hypothenuse:: sine of the angle at the base:
perpendicular.

When the perpendicular is given, perpendicular must be substituted for base in this proportion.

Ex. 1. Given the hypothenuse 54.32, and the base 32.11, to find the angles and the perpendicular.

By natural numbers, we have

54.32:1::32.11:.591127, which is the cosine of 53° 45 47", the angle at the base.

Also, 1:54.32::.806580:43.813=the perpendicular.

The computation may be performed more expeditiously by logarithms, as in the former case.

Ex. 2. Given the hypothenuse 332.49, and the perpendicular 98.399, to find the angles and the base.

Ans. The angles are 17° 12' 51'' and 72° 47' 9''; the base, 317.6.

CASE III.

(46.) Given one leg and the angles, to find the other leg and hypothenuse.

This case is solved by Theorem II.

Radius: base::tangent of the angle at the base: the perpen dicular.

:: secant of the angle at the base: hypothenuse.

When the perpendicular is given, perpendicular must be substituted for base in this proportion.

Ex. 1. Given the base 222, and the angle at the base 25° 15°, to find the perpendicular and hypothenuse.

By natural numbers, we have

1:222:: .471631:104.70, perpendicular;

:: 1.105638 : 245.45, hypothenuse.

The computation should also be performed by logarithms, as in Case I.

Ex. 2. Given the perpendicular 125, and the angle at the perpendicular 51° 19′, to find the hypothenuse and base.

Ans. Hypothenuse, 199.99; base, 156.12.

CASE IV.

(47.) Given the two legs, to find the angles and hypothenuse. This case is solved by Theorem II.

Base: radius:: perpendicular: tangent of the angle at the base. Radius: base:: secant of the angle at the base: hypothenusc.

Ex. 1. Given the base 123, and perpendicular 765, to find the angles and hypothenuse.

By natural numbers, we have

123:1::765:6.219512, which is the tangent of 80° 51 57", the angle at the base.

1: 123::: 6.299338: 774.82, hypothenuse.

The computation may also be made by logarithms, as in Case I.

Ex. 2. Given the base 53, and perpendicular 67, to find the angles and hypothenuse.

Ans. The angles are 51° 39′ 16″ and 38° 20′ 44″; hypothenuse, 85.428.

Examples for Practice.

1. Given the base 777, and perpendicular 345, to find the hypothenuse and angles.

This example, it will be seen, falls under Case IV.

- 2. Given the hypothenuse 324, and the angle at the base 48° 17′, to find the base and perpendicular.
- 3. Given the perpendicular 543, and the angle at the base 72° 45′, to find the hypothenuse and base.
- 4. Given the hypothenuse 666, and base 432, to find the angles and perpendicular.
- 5. Given the base 634, and the angle at the base 53° 27′, to find the hypothenuse and perpendicular.
- 6. Given the hypothenuse 1234, and perpendicular 555, to find the base and angles.
- (48.) When two sides of a right-angled triangle are given, the third may be found by means of the property that the square of the hypothenuse is equal to the sum of the squares of the other two sides.

Hence, representing the hypothenuse, base, and perpendicular by the initial letters of these words, we have

$$h = \sqrt{b^2 + p^2}$$
; $b = \sqrt{h^2 - p^2}$; $p = \sqrt{h^2 - b^2}$.

Ex. 1. If the base is 2720, and the perpendicular 3104, what is the hypothenuse?

Ans., 4127.1.

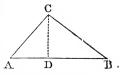
Ex. 2. If the hypothenuse is 514, and the perpendicular 432, what is the base?

SOLUTIONS OF OBLIQUE-ANGLED TRIANGLES.

THEOREM I.

(49.) In any plane triangle, the sines of the angles are proportional to the opposite sides.

Let ABC be any triangle, and from one of its angles, as C, let CD be drawn perpendicular to AB. Then, because the triangle ACD is right angled at D, we have



R : sin. A :: AC : CD; whence $R \times CD = sin. A \times AC$.

For the same reason,

 $R : \sin B :: BC : CD$; whence $R \times CD = \sin B \times BC$.

Therefore, $\sin . A \times AC = \sin . B \times BC$, $\sin . A : \sin . B :: BC : AC$.

THEOREM II.

(50.) In any plane triangle, the sum of any two sides is to their difference, as the tangent of half the sum of the opposite angles is to the tangent of half their difference.

Let ABC be any triangle; then will

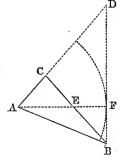
$$CB+CA:CB-CA::tang.\frac{A+B}{2}:tang.\frac{A-B}{2}.$$

Produce AC to D, making CD equal to CB, and join D3. Take CE equal to CA, draw AE, and produce it to F. Then AD is the *sum* of CB and CA, and BE is their *difference*.

The sum of the two angles CAE, CEA, is equal to the sum of CAB, CBA, each being the supplement of ACB (Geom.,

Prop. 27, B. I.). But, since CA is equal to CE, the angle CAE is equal to the angle CEA; therefore, CAE is the half sum of the angles CAB, CBA. Also, if from the greater of the two angles CAB, CBA, there be taken their half sum, the remainder, FAB, will be their half difference (Algebra, p. 68).

Since CD is equal to CB, the angle ADF is equal to the angle EBF; also, the angle CAE is equal to AEC, which is equal



to the vertical angle BEF. Therefore, the two triangles DAF, BEF, are mutually equiangular; hence the two angles at F are equal, and AF is perpendicular to DB. If, then, AF be made radius, DF will be the tangent of DAF, and BF will be the tangent of BAF. But, by similar triangles, we have

AD: BE:: DF: BF; that is, CB+CA: CB-CA:: tang. $\frac{A+B}{2}$: tang. $\frac{A-B}{2}$.

THEOREM III.

(51.) If from any angle of a triangle a perpendicular be drawn to the opposite side or base, the whole base will be to the sum of the other two sides, as the difference of those two sides is to the difference of the segments of the base.

For demonstration, see Geometry, Prop. 31, Cor., B. IV.

- (52). In every plane triangle, three parts must be given to enable us to determine the others; and of the given parts, one, at least, must be a side. For if the angles only are given, these might belong to an infinite number of different triangles. In solving oblique-angled triangles, four different cases may therefore be presented. There may be given,
 - 1. Two angles and a side;
 - 2. Two sides and an angle opposite one of them;
 - 3. Two sides and the included angle; or,
 - 4. The three sides.

We shall represent the three angles of the proposed triangle by A, B, C, and the sides opposite them, respectively, by a, b, c

Case I.

(53.) Given two angles and a side, to find the third angle and the other two sides.

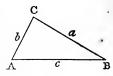
To find the third angle, add the given angles together, and subtract their sum from 180°.

The required sides may be found by Theorem I. The proportion will be,

The sine of the angle opposite the given side: the given side: the sine of the angle opposite the required side: the required side.

Ex. 1. In the triangle ABC, there are given the angle A, 57° 15′, the angle B, 35° 30′, and the side c, 364, to find the other parts.

The sum of the given angles, subtracted A



from 180°, leaves 87° 15′ for the angle C. Then, to find the side a, we say, $\sin C : c :: \sin A : a$.

By natural numbers,

.998848:364::.841039:306.49=a.

This proportion is most easily worked by logarithms, thus.

As the sine of the angle C, 87° 15', comp., 0.000500 Is to the side c, 364, 2.561101 So is the sine of the angle A, 57° 15', 9.924816

To the side a, 306.49, $\overline{2.486417}$.

To find the side b:

 $\sin C: c: \sin B: b.$

By natural numbers,

.998848:364:..580703:211.62=b.

The work by logarithms is as follows:

sin. C, 87° 15′, comp.,

c, 364,

c: sin. B, 35° 30′,

d. 0.000500

2.561101

2.763954

2.325555.

Ex. 2. In the triangle ABC, there are given the angle A, 49° 25', the angle C, 63° 48', and the side c, 275, to find the other parts. Ans., B=66° 47'; a=232.766; b=281.67.

CASE II.

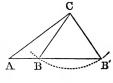
(54.) Given two sides and an angle opposite one of them, to find the third side and the remaining angles.

One of the required angles is found by Theorem I. The proportion is,

The side opposite the given angle: the sine of that angle: the other given side: the sine of the opposite angle.

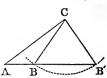
The third angle is found by subtracting the sum of the other two from 180°; and the third side is found as in Case I.

If the side BC, opposite the given angle A, is shorter than the other given side AC, the solution will be *ambiguous*; that is, two different triangles, ABC, AB'C, may be formed, each of which will satisfy A the conditions of the problem.



The numerical result is also ambiguous, for the fourth term

of the first proportion is a sine of an angle. the sine either of the acute angle AB'C, or of its supplement, the obtuse angle ABC (Art. 27). In practice, however, there will generally be some circumstance to determine whether the required angle is acute or A



But this may be

obtuse. If the given angle is obtuse, there can be no ambiguity in the solution, for then the remaining angles must of course be acute.

Ex. 1. In a triangle, ABC, there are given AC, 458, BC 307, and the angle Λ , 28° 45′, to find the other parts.

To find the angle B:

By natural numbers,

307: .480989:: 458: .717566, sin. B, the arc corresponding to which is 45° 51′ 14″, or 134° 8′ 46″.

This proportion is most easily worked by logarithms, thus

BC, 307, comp.,	7.512862
: sin. A, 28° 45′,	9.682135
:: AC, 458,	2.660865
: sin. B, 45° 51′ 14″, or 134° 8′ 46″,	9.855862.

The angle ABC is 134° 8′ 46″, and the angle AB′C, 45° 5 . 14″. Hence the angle ACB is 17° 6′ 14″, and the angle ACB

105° 23′ 46″.

To find the side AB:

By logarithms,

sin. A, 28° 45′, comp.,	0.317865
: CB, 307,	2.487138
:: sin. ACB, 17° 6′ 14″,	9.468502
: AB, 187.72,	2.273505

To find the side AB':

$$\sin$$
 A: CB':: \sin ACB': AB'.

By logarithms,

sin. A, 28° 45′, comp.,	0.317865
: CB', 307,	2.487138
:: sin. ACB', 105° 23′ 46″,	9.984128
: AB', 615.36,	2.789131.

Ex. 2. In a triangle, ABC, there are given AB, 532, BC, 358, and the angle C, 107° 40′, to find the other parts.

Ans. A=39° 52′ 52″; B=32° 27′ 8″; AC=299.6.

In this example there is no ambiguity, because the given angle is obtuse.

CASE III.

(55.) Given two sides and the included angle, to find the third side and the remaining angles.

The sum of the required angles is found by subtracting the given angle from 180°. The difference of the required angles is then found by Theorem II. Half the difference added to half the sum gives the greater angle, and, subtracted, gives the less angle. The third side is then found by Theorem I.

Ex. 1. In the triangle ABC, the angle A is given 53° 8', the side c, 420, and the side b, 535, to find the remaining parts.

The sum of the angles $B+C=180^{\circ}-53^{\circ}$ 8'=126° 52'. Half their sum is 63° 26'.

Then, by Theorem II.,

535+420:535-420:: tang. $63^{\circ} 26':$ tang. $13^{\circ} 32 25'',$ which is half the difference of the two required angles.

Hence the angle B is 76° 58' 25'', and the angle C, 49° 53 35''.

To find the side a:

 $\sin C : c :: \sin A : a = 439.32.$

Ex. 2. Given the side c, 176, a, 133, and the included angle B, 73°, to find the remaining parts.

Ans., b=187.022, the angle C, 64° 9′ 3″, and A, 42° 50′ 57″.

CASE IV.

(56.) Given the three sides, to find the angles.

Let fall a perpendicular upon the longest side from the opposite angle, dividing the given triangle into two right-angled triangles. The two segments of the base may be found by Theorem III. There will then be given the hypothenuse and one side of a right-angled triangle to find the angles.

Ex. 1. In the triangle ABC, the side a is 261, the side b, 345, and c, 395. What are the angles?

Let fall the perpendicular CD upon AB.

Then, by Theorem III.,

AB : AC + CB :: AC - CB : AD - DB;

or 395:606::84:128.87.

Half the difference of the segments added to half their sum gives the greater segment, and subtracted gives the less segment.

Therefore, AD is 261.935, and BD, 133.065.

Then, in each of the right-angled triangles, ACD, BCD, we have given the A D B hypothenuse and base, to find the angles by Case II. of right-angled triangles. Hence

$$AC : R :: AD : \cos A = 40^{\circ} 36' 13'';$$

$$BC : R :: BD : \cos B = 59^{\circ} 20' 52'$$
.

Therefore the angle C=80° 2′ 55″.

Ex. 2. If the three sides of a triangle are 150, 140, and 130, what are the angles?

Ans., 67° 22′ 48″, 59° 29′ 23″, and 53° 7′ 49″

Examples for Practice.

1. Given two sides of a triangle, 478 and 567, and the in cluded angle, 47° 30′, to find the remaining parts.

2. Given the angle A, 56° 34', the opposite side, a, 735, and the side b, 576, to find the remaining parts.

3. Given the angle A, 65° 40', the angle B, 74° 20', and the side a, 275, to find the remaining parts.

4. Given the three sides, 742, 657, and 379, to find the angles.

5. Given the angle A, 116° 32', the opposite side, a, 492, and the side c, 295, to find the remaining parts.

6. Given the angle C, 56° 18', the opposite side, c, 184, and the side b, 219, to find the remaining parts.

This problem admits of two answers.

INSTRUMENTS USED IN DRAWING.

(57.) The following are some of the most important instruments used in drawing.

I. The dividers consist of two legs, revolving upon a pivot at one extremity. The joints should be composed of two dif-

ferent metals, of unequal hardness: one part, for example, of

steel, and the other of brass or silver, in order that they may move upon each other with greater



freedom. The points should be of tempered steel, and when the dividers are closed, they should meet with great exactness. The dividers are often furnished with various appendages, which are exceedingly convenient in drawing. Sometimes one of the legs is furnished with an adjusting screw, by which a slow motion may be given to one of the points, in which case they are called hair compasses. It is also useful to have a movable leg, which may be removed at pleasure, and other parts fitted to its place; as, for example, a long beam for drawing large circles, a pencil point for drawing circles with a pencil, an ink point for drawing black circles, &c.

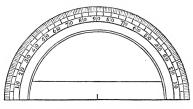
(58.) II. The parallel rule consists of two flat rules, made of wood or ivory, and connected together by two cross-bars of



equal length, and parallel to each other. This instrument is useful for drawing a line parallel to a given line, through a given point. For this purpose, place the edge of one of the flat rules against the given line, and move the other rule until its edge coincides with the given point. A line drawn along its edge will be parallel to the given line.

(59.) III. The protractor is used to lay down or to measure

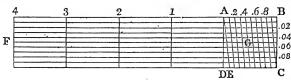
angles. It consists of a semicircle, usually of brass, and is divided into degrees, and sometimes smaller portions, the center of the circle being indicated by a small notch.



To lay down an angle with the protractor, draw a base line, and apply to it the edge of the protractor, so that its center shall fall at the angular point Count the degrees contained

in the proposed angle on the limb of the circle, and mark the extremity of the arc with a fine dot. Remove the instrument, and through the dot draw a line from the angular point; it will give the angle required. In a similar manner, the inclination of any two lines may be measured with the protractor.

(60.) IV. The plane scale is a ruler, frequently two feet in length, containing a line of equal parts, chords, sines, tan gents, &c. For a scale of equal parts, a line is divided intinches and tenths of an inch, or half inches and twentieths. When smaller fractions are required, they are obtained by means of the diagonal scale, which is constructed in the following manner. Describe a square inch, ABCD, and divide



each of its sides into ten equal parts. Draw diagonal lines from the first point of division on the upper line, to the second on the lower; from the second on the upper line, to the third on the lower, and so on. Draw, also, other lines parallel to AB, through the points of division of BC. Then, in the triangle ADE, the base, DE, is one tenth of an inch; and, since the line AD is divided into ten equal parts, and through the points of division lines are drawn parallel to the base, forming nine smaller triangles, the base of the least is one tenth of DE, that is, .01 of an inch; the base of the second is .02 of an inch; the third, .03, and so on. Thus the diagonal scale furnishes us *hundredths* of an inch. To take off from the scale a line of given length, as, for example, 4.45 inches, place one foot of the dividers at F, on the sixth horizontal line, and extend the other foot to G, the fifth diagonal line.

A half inch or less is frequently subdivided in the same manner.

(61.) A line of chords, commonly marked cho., is found on most plane scales, and is useful in setting off angles. To form this line, describe a circle with any convenient radius, and divide the circumference into degrees. Let the length of the

chords for every degree of the quadrant be determined and laid off on a scale: this is called a line of chords.

Since the chord of 60° is equal to radius, in order to lay

Chords	10	20	30	40	5	0	69	70	80	90		
Sines	10	20	30	40	50	50 70	90	30	40		50 Secants	60
Tang.	10	20		30		40		50	0		60	

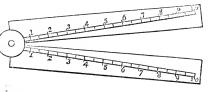
down an angle, we take from the scale the chord of 60°, and with this radius describe an arc of a circle. Then take from the scale the chord of the given angle, and set it off upon the former arc. Through these two points of division draw lines to the center of the circle, and they will contain the required angle.

The line of sines, commonly marked sin., exhibits the lengths of the sines to every degree of the quadrant, to the same radius as the line of chords. The line of tangents and the line of secants are constructed in the same manner. Since the sine of 90° is equal to radius, and the secant of 0° is the same, the graduation on the line of secants begins where the line of sines ends.

On the back side of the plane scale are often found lines representing the logarithms of numbers, sines, tangents, &c. This is called Gunter's Scale.

(62.) V. The Sector is a very convenient instrument in

drawing. It consists of two equal arms, movable about a pivot as a center, having several scales drawn on the faces, some single, oth-

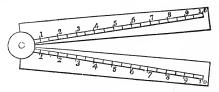


ers double. The single scales are like those upon a common Gunter's scale. The double scales are those which proceed from the center, each being laid twice on the same face of the instrument, viz., once on each leg. The double scales are a scale of lines, marked Lin. or L.; the scale of chords, sines, &c. On each arm of the sector there is a diagonal line, which diverges from the central point like the radius of a circle, and these diagonal lines are divided into equal parts.

The advantage of the sector is to enable us to draw a line

upon paper to any scale; as, for example, a scale of 6 feet to the inch. For this purpose, take an inch with the dividers from the scale of inches; then, placing one foot of the dividers at 6 on one arm of the sector, open the sector until the other foot reaches to the same number on the other arm. Now, re-

garding the lines on the sector as the sides of a triangle, of which the line measured from 6 on one arm to 6 on the other arm is the base, it is



plain that if any other line be measured across the angle of the sector, the bases of the triangles thus formed will be proportional to their sides. Therefore, a line of 7 feet will be represented by the distance from 7 to 7, and so on for other lines.

The sector also contains a line of chords, arranged like the line of equal parts already mentioned. Two lines of chords are drawn, one on each arm of the sector, diverging from the central point. This double line of chords is more convenient than the single one upon the plane scale, because it furnishes chords to any radius. If it be required to lay down any angle, as, for example, an angle of 25°, describe a circle with any convenient radius. Open the sector so that the distance from 60 to 60, on the line of chords, shall be equal to this radius. Then, preserving the same opening of the sector, place one foot of the dividers upon the division 25 on one scale, and extend the other foot to the same number upon the other scale: this distance will be the chord of 25 degrees, which must be set off upon the circle first described.

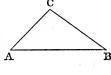
The lines of sines, tangents, &c., are arranged in the same manner.

(63.) By means of the instruments now enumerated, all the cases in Plane Trigonometry may be solved mechanically. The sides and angles which are given are laid down according to the preceding directions, and the required parts are then measured from the same scale. The student will do well to exercise himself upon the following problems:

I. Given the angles and one side of a triangle, to find, by construction, the other two sides.

Draw an indefinite straight line, and from the scale of equal parts lay off a portion, AB, equal to the given side. From each extremity lay off an angle equal to one of the adjacent angles, by means of a protractor or a scale of chords. Extend the two lines till they intersect, and measure their lengths upon the same scale of equal parts which was used in laying off the base.

Ex. 1. Given the angle A, 45° 30′, the angle B, 35° 20′, and the side AB, 43° rods, to construct the triangle, and find the lengths of the sides AC and BC.



The triangle ABC may be constructed of any dimensions whatever; all which is essential is that its angles be made equal to the given angles. We may construct the triangle upon a scale of 100 rods to an inch, in which case the side AB will be represented by 4.32 inches; or we may construct it upon a scale of 200 rods to an inch; that is, 100 rods to a half inch, which is very conveniently done from a scale on which a half inch is divided like that described in Art. 60; or we may use any other scale at pleasure. It should, however, be remembered, that the required sides must be measured upon the same scale as the given sides.

Ex. 2. Given the angle A, 48°, the angle C, 113°, and the side AC, 795, to construct the triangle.

II. Given two sides and an angle opposite one of them, to find the other parts.

Draw the side which is adjacent to the given angle. From one end of it lay off the given angle, and extend a line indefinitely for the required side. From the other extremity of the first side, with the remaining given side for radius, describe an arc cutting the indefinite line. The point of intersection will determine the third angle of the triangle.

Ex. 1. Given the angle A, 74° 45′, the side AC, 432, and the side BC, 475, to construct the triangle, and find the other parts.

Ex. 2. Given the angle A, 105°, the side BC, 498, and the side AC, 375, to construct the triangle.

III. Given two sides and the included angle, to find the other parts.

Draw one of the given sides. From one end of it lay off the given angle, and draw the other given side, making the required angle with the first side. Then connect the extremities of the two sides, and there will be formed the triangle required

Ex. 1. Given the angle A, 37° 25′, the side AC, 675, and the side AB, 417, to construct the triangle, and find the other parts.

Ex. 2. Given the angle A, 75°, the side AC, 543, and the side AB, 721, to construct the triangle.

IV. Given the three sides, to find the angles.

Draw one of the sides as a base; and from one extremity of the base, with a radius equal to the second side, describe an arc of a circle. From the other end of the base, with a radius equal to the third side, describe a second arc intersecting the former; the point of intersection will be the third angle of the triangle.

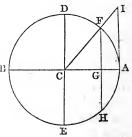
Ex. 1. Given AB, 678, AC, 598, and BC, 435, to find the angles.

Ex. 2. Given the three sides 476, 287, and 354, to find the angles.

Values of the Sines, Cosines, &c., of certain Angles

(64.) We propose now to examine the changes which the

sines, cosines, &c., undergo in the different quadrants of a circle. Draw two diameters, AB, DE, perpendicular to each other, and suppose one of them to occupy a horizontal position, the other a vertical. The angle ACD is called the first quadrant, the angle DCB the second quadrant, the angle BCE the third quadrant, and the an-



gle ECA the *fourth* quadrant; that is, the first quadrant is above the horizontal diameter, and on the right of the vertical diameter; the second quadrant is above the horizontal diameter, and on the left of the vertical, and so on.

Suppose one extremity of the arc remains fixed in A, while the other extremity, marked F, runs round the entire circumference in the direction ADBE. When the point F is at A, or when the arc AF is zero, the sine is zero. As the point F advances toward D, the sine increases; and when the arc AF becomes 45°, the triangle CFG being isosceles, we have FG: $CF: 1: \sqrt{2}$ (Geom., Prop. 11, Cor. 3, B. IV.); or $\sin . 45^\circ : R: 1: \sqrt{2}$.

Hence,
$$\sin 45^{\circ} = \frac{R}{\sqrt{2}} = \frac{1}{2} R \sqrt{2}$$
.

The sine of 30° is equal to half radius (Art. 22). Also, since sin. $A = \sqrt{R^2 - \cos^2 A}$, the sine of 60°, which is equal to the cosine of 30°, $= \sqrt{R^2 - \frac{1}{4}R^2} = \sqrt{\frac{3}{4}R^2} = \frac{1}{2}R\sqrt{3}$.

The arc AF continuing to increase, the sine also increases till F arrives at D, at which point the sine is equal to the radius; that is, the sine of 90°=R.

As the point F advances from D toward B, the sines diminish, and become zero at B; that is, the sine of 180°=0.

In the third quadrant, the sine increases again, becomes equal to radius at E, and is reduced to zero at A.

- (65.) When the point F is at A, the cosine is equal to radius. As the point F advances toward D, the cosine decreases, and the cosine of 45° =sine 45° = $\frac{1}{2}$ R $\sqrt{2}$. The arc continuing to increase, the cosine diminishes till F arrives at D, at which point the cosine becomes equal to zero. The cosine in the second quadrant increases, and becomes equal to radius at B; in the third quadrant it decreases, and becomes zero at E; in the fourth quadrant it increases again, and becomes equal to radius at A.
- (66.) The tangent begins with zero at A, increases with the arc, and at 45° becomes equal to radius. As the point F approaches D, the tangent increases very rapidly; and when the difference between the arc and 90° is less than any assignable quantity, the tangent is greater than any assignable quantity. Hence the tangent of 90° is said to be infinite.

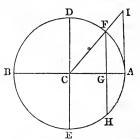
In the second quadrant the tangent is at first infinitely great, and rapidly diminishes till at B it is reduced to zero. In the third quadrant it increases again, becomes infinite at E, and is reduced to zero at A.

The cotangent is equal to zero at D and E, and is infinite at A and B.

(67.) The secant begins with radius at A, increases through

the first quadrant, and becomes infinite at D; diminishes in

the second quadrant, till at B it is equal to the radius; increases again in the third quadrant, and becomes infinite at E; decreases in the fourth quadrant, and becomes equal to the B radius at A.



The cosecant is equal to radius at D and E, and is infinite at A and B.

gebraic signs by which these lines are to be distinguished. In the first and second quadrants, the sines fall above the diameter AB, while in the third and fourth quadrants they fall below. This opposition of directions ought to be distinguished by the algebraic signs; and if one of these directions is regarded as positive, the other ought to be considered as negative. It is generally agreed to consider those sines which fall above the horizontal diameter as positive; consequently, those which fall below must be regarded as negative. That is, the sines are positive in the first and second quadrants, and negative in the third and fourth.

In the first quadrant the cosine falls on the *right* of DE, but in the second quadrant it falls on the *left*. These two lines should obviously have opposite signs, and it is generally agreed to consider those which fall to the right of the vertical diameter as positive; consequently, those which fall to the left must be considered negative. That is, the cosines are positive in the first and fourth quadrants, and negative in the second and third.

(69.) The signs of the tangents are derived from those of the sines and cosines. For tang. $=\frac{R.\sin.}{\cos}$ (Art. 28). Hence, when the sine and cosine have like algebraic signs, the tangent will be positive; when unlike, negative. That is, the tangent is positive in the first and third quadrants, and negative in the second and fourth.

Also, cotangent $=\frac{R^2}{\tan g}$. (Art. 28); hence the tangent and satisfactor that always the same sign.

We have seen that sec. $=\frac{R^2}{\cos}$; hence the secant must have the same sign as the cosine.

Also, cosec. $=\frac{R^2}{\sin}$; hence the cosecant must have the same sign as the sine.

(70.) The preceding results are exhibited in the following tables, which should be made perfectly familiar:

		•	•		
		First quad.	Second quad.	Third quad.	Fourth quad
Sine and cos	secant,	+	+	_	_
Cosine and a	secant,	+		-	+
Tangent and	l cotangent	, +		+	_
	0°	90°	180°	270°	360∘
Sine,	0	+R	0	-R	0
Cosine,	+R	0	-R	0	+R
Tangent,	0	∞	0	∞	0
Cotangent,	∞	0	oo	0	∞
Secant,	+R	∞	-R	∞	+R
Cosecant,	∞	+R	∞	-R	∞

(71.) In Astronomy we frequently have occasion to consider arcs greater than 360°. But if an entire circumference, or any number of circumferences, be added to any arc, it will terminate in the same point as before. Hence, if C represent an entire circumference, or 360°, and A any arc whatever, we shall have

$$\sin A = \sin (C+A) = \sin (2C+A) = \sin (3C+A) =$$
, &c.

The same is true of the cosine, tangent, &c.

We generally consider those arcs as positive which are estimated from A in the direction ADBE. If, then, an arc were estimated in the direction AEBD, it should be considered as negative; that is, if the arc AF be considered positive, AH must be considered negative. But the latter belongs to the fourth quadrant; hence its sine is negative. Therefore, $\sin(-A) = -\sin A$.

The cosine CG is the same for both the arcs AF and AH.

Hence,
$$\cos \cdot (-A) = \cos \cdot A$$
.
Also, $\tan \cdot (-A) = -\tan \cdot A$.
And $\cot \cdot (-A) = -\cot \cdot A$.

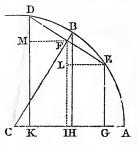
TRIGONOMETRICAL FORMULÆ.

(72.) Expressions for the sine and cosine of the sum and difference of two arcs.

Let AB and BD represent any two given arcs; take BE

equal to BD: it is required to find an expression for the sine of AD, the sum, and of AE, the difference of these arcs.

Put AB=a, and BD=b; then AD=a+b, and AE=a-b. Draw the chord DE, and the radius CB, which may be represented by R. Since DB is by construction equal to BE, DF is equal to FE, and therefore DE is perpendic-



ular to CB. Let fall the perpendiculars EG, BH, FI, and DK upon AC, and draw EL, FM parallel to AC.

Because the triangles BCH, FCI are similar, we have

$$CB : CF :: BH : FI ; or R : cos. b :: sin. a : FI.$$

Therefore,
$$FI = \frac{\sin a \cos b}{R}$$
.

Also,
$$CB : CF :: CH : CI$$
; or $R : cos. b :: cos. a : CI$.

Therefore,
$$CI = \frac{\cos a \cos b}{R}$$
.

The triangles DFM, CBH, having their sides perpendicular each to each, are similar, and give the proportions.

$$CB : DF :: CH : DM$$
; or $R : \sin b :: \cos a : DM$.

Hence
$$DM = \frac{\cos a \sin b}{R}$$
.

Also,
$$CB : DF :: BH : FM$$
; or $R : \sin b :: \sin a : FM$.

Hence
$$FM = \frac{\sin a \sin b}{R}.$$
But
$$FI + DM = DK = \sin (a+b);$$
and
$$CI - FM = CK = \cos (a+b).$$
Also,
$$FI - FL = EG = \sin (a-b);$$
and
$$CI + EL = CG = \cos (a-b).$$
Hence,
$$\sin (a+b) = \frac{\sin a \cos b + \cos a \sin b}{R}$$
(1)
$$\cos (a+b) = \frac{\cos a \cos b - \sin a \sin b}{R}$$
(2)

$$\sin (a-b) = \frac{\sin a \cos b - \cos a \sin b}{R}$$
 (3)
$$\cos (a-b) = \frac{\cos a \cos b + \sin a \sin b}{R}$$
 (4)

(73.) Expressions for the sine and cosine of a double arc. If, in the formulas of the preceding article, we make b=a the first and second will become

$$\sin 2a = \frac{2 \sin a \cos a}{R},$$

 $\cos 2a = \frac{\cos^2 a - \sin^2 a}{R}.$

Making radius equal to unity, and substituting the values of sin. a, cos. a. &c., from Art. 28, we obtain

sin.
$$2a = \frac{2 \text{ tang. } a}{1 + \text{tang. }^2 a}$$

cos. $2a = \frac{1 - \text{tang. }^2 a}{1 + \text{tang. }^2 a}$

(74.) Expressions for the sine and cosine of half a given arc.

If we put $\frac{1}{2}a$ for a in the preceding equations, we obtain

$$\sin a = \frac{2 \sin \frac{1}{2} a \cos \frac{1}{2} a}{R},$$

$$\cos a = \frac{\cos \frac{21}{2} a - \sin \frac{21}{2} a}{R}.$$

We may also find the sine and cosine of $\frac{1}{2}a$ in terms of a. Since the sum of the squares of the sine and cosine is equal to the square of radius, we have

$$\cos^{2} \frac{1}{2}a + \sin^{2} \frac{1}{2}a = R^{2}$$
.

And, from the preceding equation,

$$\cos^{2} \frac{1}{2}a - \sin^{2} \frac{1}{2}a = R \cos a.$$

If we subtract one of these from the other, we have $2 \sin^2 a = R^2 - R \cos a$.

And, adding the same equations,

$$2 \cos^{2} \frac{1}{2}a = R^{2} + R \cos a$$
.

Hence,
$$\sin \frac{1}{2}a = \sqrt{\frac{1}{2}R^2 - \frac{1}{2}R \cos a};$$

 $\cos \frac{1}{2}a = \sqrt{\frac{1}{2}R^2 + \frac{1}{2}R \cos a}.$

(75.) Expressions for the products of sines and cosines. By adding and subtracting the formulas of Art. 72, we obtain

$$\sin (a+b) + \sin (a-b) = \frac{2}{R} \sin a \cos b.$$

 $\sin (a+b) - \sin (a-b) = \frac{2}{R} \cos a \sin b;$
 $\cos (a+b) + \cos (a-b) = \frac{2}{R} \cos a \cos b;$
 $\cos (a-b) - \cos (a+b) = \frac{2}{R} \sin a \sin b.$

If, in these formulas, we make a+b=A, and a-b=B; that is, $a=\frac{1}{2}(A+B)$, and $b=\frac{1}{2}(A-B)$, we shall have

sin. A+sin. B=
$$\frac{2}{R}$$
 sin. $\frac{1}{2}$ (A+B) cos. $\frac{1}{2}$ (A-B) (1)

sin. A-sin. B=
$$\frac{2}{R}$$
 sin. $\frac{1}{2}$ (A-B) cos. $\frac{1}{2}$ (A+B) (2)

cos. A+cos. B=
$$\frac{2}{R}$$
 cos. $\frac{1}{2}$ (A+B) cos. $\frac{1}{2}$ (A-B) (3)

cos. B-cos. A=
$$\frac{2}{R}$$
 sin. $\frac{1}{2}$ (A+B) sin. $\frac{1}{2}$ (A-B) (4)

(76.) Dividing formula (1) by (2), and considering that $\frac{\sin a}{\cos a} = \frac{\tan a}{R}$ (Art. 28), we have

$$\frac{\sin. A + \sin. B}{\sin. A - \sin. B} = \frac{\sin. \frac{1}{2}(A + B) \cos. \frac{1}{2}(A - B)}{\sin. \frac{1}{2}(A - B) \cos. \frac{1}{2}(A + B)} = \frac{\tan g. \frac{1}{2}(A + B)}{\tan g. \frac{1}{2}(A - B)};$$
that is,

The sum of the sines of two arcs is to their difference, as the tangent of half the sum of those arcs is to the tangent of half their difference.

Dividing formula (3) by (4), and considering that $\frac{\cos}{\sin} = \frac{\cot}{R}$

$$=\frac{R}{\text{tang.}}$$
 (Art. 28), we have

$$\frac{\cos. A + \cos. B}{\cos. B - \cos. A} = \frac{\cos. \frac{1}{2}(A+B) \cos. \frac{1}{2}(A-B)}{\sin. \frac{1}{2}(A+B) \sin. \frac{1}{2}(A-B)} = \frac{\cot. \frac{1}{2}(A+B)}{\tang. \frac{1}{2}(A-B)};$$
that is,

The sum of the cosines of two arcs is to their difference, as the cotangent of half the sum of those arcs is to the tang at of half their difference.

From the first formula of Art. 74, by substituting A + B for ι , we have

$$\sin (A+B) = \frac{2 \sin \frac{1}{2}(A+B) \times \cos \frac{1}{2}(A+B)}{R}$$
.

Dividing formula (1), Art. 75, by this, we obtain

$$\frac{\sin. A + \sin. B}{\sin. (A+B)} = \frac{\sin. \frac{1}{2}(A+B) \cos. \frac{1}{2}(A-B)}{\sin. \frac{1}{2}(A+B) \cos. \frac{1}{2}(A+B)} = \frac{\cos. \frac{1}{2}(A-B)}{\cos. \frac{1}{2}(A+B)};$$
that is,

The sum of the sines of two arcs is to the sine of their sum, as the cosine of half the difference of those arcs is to the cosine of half their sum.

If we divide equation (1), Art. 72, by equation (3), we shall have

$$\frac{\sin. (a+b)}{\sin. (a-b)} = \frac{\sin. a \cos. b + \cos. a \sin. b}{\sin. a \cos. b - \cos. a \sin. b}$$

By dividing both numerator and denominator of the second member by $\cos a \cos b$, and substituting $\frac{\tan g}{R}$ for $\frac{\sin c}{\cos b}$, we ob-

tain
$$\frac{\sin (a+b)}{\sin (a-b)} = \frac{\tan a + \tan b}{\tan a - \tan b}; \text{ that is,}$$

The sine of the sum of two arcs is to the sine of their difference, as the sum of the tangents of those arcs is to the difference of the tangents.

From equation (3), Art. 72, by dividing each member by $\cos a \cos b$, we obtain

$$\frac{\sin. (a-b)}{\cos. a \cos. b} = \frac{\sin. a \cos. b - \cos. a \sin. b}{R \cos. a \cos. b} = \frac{\tan a - \tan b}{R^2};$$
that is,

The sine of the difference of two arcs is to the product of their cosines, as the difference of their tangents is to the square of radius.

(77.) Expressions for the tangents of arcs.

If we take the expression tang. $(a+b) = \frac{R \sin (a+b)}{\cos (a+b)}$ (Art. 28), and substitute for sin. (a+b) and cos. (a+b) their values given in Art. 72, we shall find

tang.
$$(a+b) = \frac{R (\sin a \cos b + \cos a \sin b)}{\cos a \cos b - \sin a \sin b}$$
.

But sin
$$a = \frac{\cos a \tan a}{R}$$
, and sin. $b = \frac{\cos b \tan b}{R}$ (Art. 28)

If we substitute these values in the preceding equation, and divide all the terms by $\cos a \cos b$, we shall have

tang.
$$(a+b) = \frac{R^2 \text{ (tang. } a+\text{tang. } b)}{R^2-\text{tang. } a \text{ tang. } b}$$

In like manner we shall find

tang.
$$(a-b) = \frac{R^2 \text{ (tang. } a-\text{tang. } b)}{R^2 + \text{tang. } a \text{ tang. } b}$$
.

Suppose b=a, then

tang.
$$2a = \frac{2R^2 \text{ tang. } a}{R^2 - \tan g.^2 a}$$

Suppose b=2a, then

tang.
$$3a = \frac{R^2 \text{ (tang. } a + \text{tang. } 2a)}{R^2 - \text{tang. } a \text{ tang. } 2a}$$

In the same manner we find

$$\cot (a+b) = \frac{\cot a \cot b - R^2}{\cot b + \cot a},$$

$$\cot (a-b) = \frac{\cot a \cot b + R^2}{\cot b - \cot a}.$$

(78.) When the three sides of a triangle are given, the angles may be found by the formula

$$\sin \frac{1}{2} A = R \sqrt{\frac{(S-b)(S-c)}{bc}},$$

where S represents half the sum of the sides a, b, and c.

Demonstration.

Let ABC be any triangle; then (Geom., Prop. 12, B. IV.), $BC^2 = AB^2 + AC^2 - 2AB \times AD$.

Hence,
$$AD = \frac{AB^2 + AC^2 - BC^2}{2AB}$$
.

But in the right-angled triangle ACD, we have

$$R:AC::\cos. A:AD.$$
 Hence,
$$\cos. A = \frac{R \times AD}{AC};$$

or, by substituting the value of AD,

cos. A=R
$$\times \frac{AB^2+AC^2-BC^2}{2AB\times AC}$$

Let a, b, c represent the sides opposite the angles A, B, C;

then,
$$\cos A = R \times \frac{b^2 + c^2 - a^2}{2bc}.$$

By Art. 74, we have $2 \sin^{2} A = R^{2} - R \cos A$.

Substituting for cos. A its value given above, we obtain

$$2 \sin^{2} \frac{1}{2} A = R^{2} - R^{2} \times \frac{b^{2} + c^{2} - a^{2}}{2bc} = R^{2} \times \frac{2bc + a^{2} - b^{2} - c^{2}}{2bc}$$

$$= \frac{R^{2} \times (a + b - c) (a + c - b)}{2bc}.$$

Put $S=\frac{1}{2}(a+\dot{b}+c)$, and we obtain, after reduction,

$$\sin \frac{1}{2} A = R \sqrt{\frac{(S-b)(S-c)}{bc}}.$$

In the same manner we find

sin.
$$\frac{1}{2}$$
B=R $\sqrt{\frac{(S-a)(S-c)}{ac}}$.
sin. $\frac{1}{2}$ C=R $\sqrt{\frac{(S-a)(S-b)}{ab}}$.

Ex. 1. What are the angles of a plane triangle whose sides are 432, 543, and 654?

Here S=814.5; S-
$$b$$
=382.5; S- c =271.5.

$\log. 382.5$		2.582631
log. 271.5		2.433770
$\log. b, 432$	comp.	7.364516
$\log. c, 543$	comp.	7.265200
	2)	19.646117
$\ln \frac{1}{2}A$, 41° 42′ 36 $\frac{1}{2}$ ″.	_	9.823058.

 $\sin \frac{1}{2}A$, 41° 42′ 36½″. 9.823058 Angle A=83° 25′ 13″.

In a similar manner we find the angle $B=41^{\circ}$ 0' 39", and the angle $C=55^{\circ}$ 34' 8".

Ex. 2. What are the angles of a plane triangle whose sides are 245, 219, and 91?

(79.) On the computation of a table of sines, cosines, &c.

In computing a table of sines and cosines, we begin with finding the sine and cosine of one minute, and thence deduce the sines and cosines of larger arcs. The sine of so small an angle as one minute is nearly equal to the corresponding arc. The radius being taken as unity, the semicircumference is

known to be 3.14159. This being divided successively by 180 and 60, gives .0002908882 for the arc of one minute, which may be regarded as the sine of one minute.

The cosine of
$$1' = \sqrt{1 - \sin^2 2} = 0.9999999577$$
.

The sines of very small angles are nearly proportional to the angles themselves. We might then obtain several other sines by direct proportion. This method will give the sines correct to five decimal places, as far as two degrees. By the following method they may be obtained with greater accuracy for the entire quadrant.

By Art. 75, we have, by transposition, $\sin(a+b)=2\sin a\cos b-\sin(a-b)$,

$$\cos((a+b)) = 2 \cos a \cos b - \cos((a-b))$$
.

If we make a=b, 2b, 3b, &c., successively, we shall have

$$\sin 2b = 2 \sin b \cos b$$
;

$$\sin 3b=2 \sin 2b \cos b-\sin b$$

$$\sin 4b = 2 \sin 3b \cos b - \sin 2b$$
,

$$\cos 2b = 2 \cos b \cos b - 1;$$

$$\cos .3b = 2 \cos .2b \cos .b - \cos .b;$$

$$\cos .4b=2 \cos .3b \cos .b-\cos .2b,$$
 &c., &c.

Whence, making b=1', we have

$$\sin 2 = 2 \sin 1' \cos 1' = .000582$$

$$\sin 3'=2 \sin 2' \cos 1'-\sin 1'=.000873;$$

$$\sin 4 = 2 \sin 3 \cos 1 - \sin 2 = .000076$$

 $\sin 4 = 2 \sin 3 \cos 1 - \sin 2 = .001164$,

$$\cos 2' = 2 \cos 1' \cos 1' - 1 = 0.9999999;$$

$$\cos 3' = 2 \cos 2' \cos 1' - \cos 1' = 0.999999;$$

$$\cos 4' = 2 \cos 3' \cos 1' - \cos 2' = 0.999999,$$

The tangents, cotangents, secants, and cosecants are easily terived from the sines and cosines. Thus,

tang.
$$1' = \frac{\sin \cdot 1'}{\cos \cdot 1'}$$
 cot. $1' = \frac{\cos \cdot 1'}{\sin \cdot 1};$
sec. $1' = \frac{1}{\cos \cdot 1};$ cosec. $1' = \frac{1}{\sin \cdot 1'};$
&c.,

BCOK III.

MENSURATION OF SURFACES.

(80.) The area of a figure is the space contained within the line or lines by which it is bounded. This area is determined by finding how many times the figure contains some other surface, which is assumed as the unit of measure. This unit is commonly a square; such as a square inch, a square foot, a square rod, &c.

The *superficial* unit has generally the same name as the *linear* unit, which forms the side of the square. Thus,

the side of a square inch is a linear inch;

- " of a square foot is a linear foot;
- " of a square yard is a linear yard, &c.

There are some superficial units which have no corresponding linear units of the same name, as, for example, an acre.

The following table contains the square measures in comtnon use:

Table of Square Measures.

PROBLEM I.

(81.) To find the area of a parallelogram.

RULE I.

Multiply the base by the altitude.

For the demonstration of this rule, see Geometry, Prop. 5 B. IV.

Ex. 1. What is the area of a parallelogram whose base is 17.5 rods, and the altitude 13 rods?

Ans., 227.5 square rods.

- Ex. 2. What is the area of a square whose side is 315.7 Ans., 99666.49 square feet. feet?
- Ex. 3. What is the area of a rectangular board whose length is 15.25 feet, and breadth 15 inches?

Ans., 19.0625 square feet.

- Ex. 4. How many square yards are there in the four sides of a room which is 18 feet long, 15 feet broad, and 9 feet high? Ans., 66 square yards.
- (82.) If the sides and angles of a parallelogram are given, the perpendicular height may be found by Trigonometry. For DE is one side of a right-angled triangle, of which AD is the hypothenuse. Hence,

R : AD :: sin. A : DE;

from which

$$DE = \frac{AD \times \sin_{\bullet} A}{R}.$$

Therefore, the area=AB×DE= $\frac{AB\times AD\times \sin A}{D}$

Hence we derive

Rule II.

Multiply together two adjacent sides, and the sine of the included angle.

Ex. 1. What is the area of a parallelogram having an angle of 58°, and the including sides 36 and 25.5 feet?

Ans. The area= $36\times25.5\times.84805$ (natural sine of 58°)= **778.508** square feet.

The computation will generally be most conveniently performed by logarithms.

Ex. 2. What is the area of a rhombus, each of whose sides is 21 feet 3 inches, and each of the acute angles 53° 20'?

Ans., 362.209 feet.

Ex. 3. How many acres are contained in a parallelogram one of whose angles is 30°, and the including sides are 25.35 and 10.4 chains? Ans., 13 acres, 29.12 rods

PROBLEM II.

(83.) To find the area of a triangle.

RULE I.

Multiply the base by half the altitude.

For demonstration, see Geometry, Prop. 6, B. IV:

Ex. 1. How many square yards are contained in a triangle whose base is 49 feet, and altitude $25\frac{1}{4}$ feet?

Ans., 68.736.

Ex. 2. What is the area of a triangle whose base is 45 feet, and altitude 27.5 feet?

Ans., 618.75 square feet.

(84.) When two sides and the included angle are given, we may use

RULE II.

Multiply half the product of two sides by the sine of the included angle.

The reason of this rule is obvious, from Art. 82, since a triangle is half of a parallelogram, having the same base and attitude.

Ex. 1. What is the area of a triangle of which two sides are 45 and 32 feet, and the included angle 46° 30′?

Ans. The area= $45 \times 16 \times .725374$ (natural sine of 46° 30')= 522.269 feet.

Ex. 2. What is the area of a triangle of which two sides are 127 and 96 feet, and the included angle 67° 15'?

Ans.

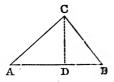
(85.) When the three sides are known, we may use

Rule III.

From half the sum of the three sides subtract each side severally; multiply together the half sum and the three remainders, and extract the square root of the product.

Demonstration.

Let a, b, c denote the sides of the triangle ABC; then, by Geometry, Prop. 12, B. IV., we have BC²=AB²+AC²-2AB×AD, or $a^2=b^2+c^2-2c\times AD$; whence,



$$AD = \frac{b^2 + c^2 - a^2}{2c}.$$
But
$$CD^2 = AC^2 - AD^2;$$
hence
$$CD^2 = b^2 - \frac{(b^2 + c^2 - a^2)^2}{4c^2} = \frac{4b^2c^2 - (b^2 + c^2 - a^2)^4}{4c^2},$$
or
$$CD = \frac{\sqrt{4b^2c^2 - (b^2 + c^2 - a^2)^2}}{2c}.$$
But the $area = \frac{AB \times CD}{2} = \frac{1}{4}\sqrt{4b^2c^2 - (b^2 + c^2 - a^2)^2}.$

The quantity under the radical sign being the difference of two squares, may be resolved into the factors $2bc + (b^2 + c^2 - a^2)$ and $2bc - (b^2 + c^2 - a^2)$; and these, in the same manner, may be resolved into $(b+c+a) \times (b+c-a)$, and $(a+b-c) \times (a-b+c)$.

Hence, if we put S equal to $\frac{a+b+c}{2}$, we shall have

the area =
$$\sqrt{S(S-a)(S-b)(S-c)}$$
.

Ex. 1. What is the area of a triangle whose sides are 125, 173, and 216 feet?

Here S=257, S-b=84, S-a=132. S-c=41.

Hence the $area = \sqrt{257 \times 132 \times 84 \times 41} = 10809$ square feet. Ex. 2. How many acres are contained in a triangle whose sides are 49, 50.25, and 25.69 chains?

Ans., 61 acres, 1 rood, 39.68 perches.

Ex. 3. What is the area of a triangle whose sides are 234, 289, and 345 feet?

Ans.

(86.) In an equilateral triangle, one of whose sides is a, the expression for the area becomes

$$\sqrt{\frac{3}{2}a \times \frac{1}{2}a \times \frac{1}{2}a \times \frac{1}{2}a}$$

$$= \frac{a^2 \sqrt{3}}{4};$$

that is, the area of an equilateral triangle is equal to on fourth the square of one of its sides multiplied by the square root of 3.

Ex. What is the area of a triangle whose sides are each 37 feet?

Ans., 592.79 feet

PROBLEM III.

(87.) To find the area of a trapezoid.

RULE.

Multiply half the sum of the parallel sides into their perpendicular distance.

For demonstration, see Geometry, Prop. 7, B. IV.

Ex. 1. What is the area of a trapezoid whose parallel sides are 156 and 124, and the perpendicular distance between them 57 feet?

Ans., 7980 feet.

Ex. 2. How many square yards in a trapezoid whose parallel sides are 678 and 987 feet, and altitude 524 feet?

Ans.

PROBLEM IV.

(88.) To find the area of an irregular polygon.

Rule.

Draw diagonals dividing the polygon into triangles, and find the sum of the areas of these triangles.

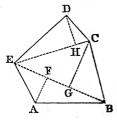
Ex. 1. What is the area of a quadrilateral, one of whose diagonals is 126 feet, and the two perpendiculars let fall upon it from the opposite angles are 74 and 28 feet?

Ans., 6426 feet.

Ex. 2. In the polygon ABCDE, there are given EC=205, EB=242, AF=65, CG=114, and DH=110, to find the area.

Ans.

' (89.) If the diagonals of a quadrilateral are given, the area may be found by the following



RULE.

Multiply half the product of the diagonals by the sine of the angle at their intersection.

Demonstration.

The sines of the four angles at E are all equal to each other

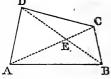
since the adjacent angles AED, DEC are the supplements of each other (Art. 27). But, according to the Rule, Art. 84, the area of

the triangle $ABE = \frac{1}{2}AE \times BE \times sine E$;

" $AED = \frac{1}{2}AE \times DE \times sine E$;

" $BEC = \frac{1}{2}BE \times EC \times sine E;$

" $DEC = \frac{1}{2}DE \times EC \times sine E.$



Therefore,

the area of ABCD= $\frac{1}{2}$ (AE+EC)×(BE+ED)×sine E = $\frac{1}{2}$ AC×BD×sine E.

- Ex. 1. If the diagonals of a quadrilateral are 34 and 56 rods, and if they intersect at an angle of 67°, what is the area?

 Ans., 876.32.
- Ex. 2. If the diagonals of a quadrilateral are 75 and 49, and the angle of intersection is 42°, what is the area?

Ans.

PROBLEM V.

(90.) To find the area of a regular polygon.

Rule I.

Multiply half the perimeter by the perpendicular let fall from the center on one of the sides.

For demonstration, see Geometry, Prop. 7, B. VI.

Ex. 1. What is the area of a regular pentagon whose side is 25, and the perpendicular from the center 17.205 feet?

Ans., 1075.31 feet.

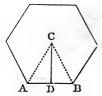
Ex. 2. What is the area of a regular octagon whose side is 53, and the perpendicular 63.977?

Ans.

(91.) When the perpendicular is not given, it may be computed from the perimeter and number of sides. If we divide

360 degrees by the number of sides of the polygon, the quotient will be the angle ACB at the center, subtended by one of the sides. The perpendicular CD bisects the side AB, and the angle ACB. Then, in the triangle ACD, we have (Art. 42),

R: AD: cot. ACD: CD; that is,



Radius is to half of one of the sides of the polygon, as the intangent of the opposite angle is to the perpendicular from the center.

Ex. 3. Find the area of a regular hexagon whose side is 32 inches.

The angle ACD is $\frac{1}{12}$ of $360^{\circ}=30^{\circ}$. Then

- R: 16:: cot. $30^{\circ}: 27.7128 = \text{CD}$, the perpendicular; and the area= $27.7128 \times 16 \times 6 = 2660.4288$.
- Ex. 4. Find the area of a regular decagon whose side is 46 feet.

 Ans., 16280.946.
- (92.) In this manner was computed the following table of the areas of regular polygons, in which the side of each polygon is supposed to be a unit.

TABLE OF REGULAR POLYGONS.

Names.	Sides.	Arcas.
Triangle,	3	0.4330127.
Square,	4	1.0000000.
Pentagon,	. 5	1.7204774.
Hexagon,	6	2.5980762.
Heptagon,	7	3.6339124
Octagon,	8	4.8284271
Nonagon,	9	6.1818242.
Decagon,	10	7.6942088.
Undecagon,	11	9.3656399.
Dodecagon,	12	11.1961524.
_		

By the aid of this table may be computed the area of any other regular polygon having not more than twelve sides. For, since the areas of similar polygons are as the *squares* of their homologous sides, we derive

Rule II.

Multiply the square of one of the sides of the polygon by the area of a similar polygon whose side is unity.

- Ex. 5. What is the area of a regular nonagon whose side is 63?

 Ans., 24535.66.
- Ex. 6. What is the area of a regular dodecagon whose side is 54 feet?

 Ans., 32647.98 feet.

PROBLEM VI

(93.) To find the circumference of a circle from its diameter

RULE

Multiply the diameter by 3.14159.

For the demonstration of this rule, see Geometry, Prop. 13, Cor. 2, B. VI.

When the diameter of the circle is small, and no great accuracy is required, it may be sufficient to employ the value of π to only 4 or 5 decimal places. But if the diameter is large, and accuracy is required, it will be necessary to employ a corresponding number of decimal places of π . The value of π to ten decimal places is 3.14159,26536,

and its logarithm is 0.497150.

Ex. 1. What is the circumference of a circle whose diameter is 125 feet?

Ans., 392.7 feet.

Ex. 2. If the diameter of the earth is 7912 miles, what is its circumference?

Ans., 24856.28 miles.

Ex. 3. If the diameter of the earth's orbit is 189,761,000 miles, what is its circumference?

Ans., 596,151,764 miles.

To obtain this answer, the value of π must be taken to at least eight decimal places.

PROBLEM VII.

(94.) To find the diameter of a circle from its circum ference.

RULE I.

Divide the circumference by 3.14159.

This rule is an obvious consequence from the preceding To divide by a number is the same as to multiply by its reciprocal; and, since multiplication is more easily performed than division, it is generally most convenient to multiply by the reciprocal of π , which is 0.3183099. Hence we have

RULE II.

Multiply the circumference by 0.31831.

Ex. 1. What is the diameter of a circle whose circumference is 875 feet?

Ans., 278.52 feet.

Ex. 2. If the circumference of the moon is 6786 miles, what is its diameter?

Ans., 2160 miles.

Ex. 3. If the circumference of the moon's orbit is 1,492,987 miles, what is its diameter?

Ans., 475,233 miles

PROBLEM VIII.

(95.) To find the length of an arc of a circle.

RULE I.

As 360 is to the number of degrees in the arc, so is the curcumference of the circle to the length of the arc.

This rule follows from Prop. 14, B. III., in Geometry, where it is proved that angles at the center of a circle have the same ratio with the intercepted arcs.

Ex. 1. What is the length of an arc of 22°, in a circle whose diameter is 125 feet?

The circumference of the circle is found to be 392.7 feet.

Then 360: 22::392.7:23.998 feet.

Ex. 2. If the circumference of the earth is 24,856.28 miles what is the length of one degree?

Ans., 69.045 miles.

Rule II.

(96.) Multiply the diameter of the circle by the number of degrees in the arc, and this product by 0.0087266.

Since the circumference of a circle whose diameter is unity is 3.14159, if we divide this number by 360, we shall obtain the length of an arc of one degree, viz., 0.0087266. If we multiply this decimal by the number of degrees in any arc, we shall obtain the length of that arc in a circle whose diameter is unity; and this product, multiplied by the diameter of any other circle, will give the length of an arc of the given number of degrees in that circle.

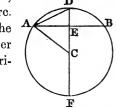
Ex. 3. What is the length of an arc of 25°, in a circle whose radius is 44 rods?

Ans., 19.198 rods.

Ex. 4. What is the length of an arc of 11° 15', in a circle whose diameter is 1234 feet?

Ans., 121.147 feet.

(97.) If the number of degrees in an arc is not given, it may be computed from the radius of the circle, and either the chord or height of the arc. Thus, let AB be the chord, and DE the height of the arc ADB, and C the center of the circle. Then, in the right-angled triangle ACE,



AC: R:: \{ AE: \sin. ACE, CE: \cos. ACE,

either of which proportions will give the number of degrees in half the arc.

If only the chord and height of the arc are given, the diameter of the circle may be found. For, by Geometry, Prop. 22, Cor., B. IV.,

DE : AE :: AE : EF.

Ex. 5. What is the length of an arc whose chord is 6 feet, in a circle whose radius is 9 feet?

Ans., 6.117 feet.

PROBLEM IX.

(98.) To find the area of a circle.

Rule I.

Multiply the circumference by half the radius. For demonstration, see Geometry, Prop. 12, B. VI.

Rule II.

Multiply the square of the radius by 3.14159.

See Geometry, Prop 13, Cor. 3, B. VI.

Ex. 1. What is the area of a circle whose diameter is 18 feet?

Ans., 254.469 feet.

Ex 2. What is the area of a circle whose circumference is 74 feet?

Ans., 435.766 feet.

Ex. 3. What is the area of a circle whose radius is 125 yards?

Ans., 49087.38 yards.

PROBLEM X.

(99.) To find the area of a sector of a circle.

RULE I

Multiply the arc of the sector by half its radius. See Geometry, Prop. 12, Cor., B. VI.

RULE II.

As 360 is to the number of degrees in the arc, so is the area of the circle to the area of the sector.

This follows from Geometry, Prop. 14, Cor. 2, B. III.

Ex. 1. What is the area of a sector whose arc is 22°, in a circle whose diameter is 125 feet?

The length of the arc is found to be 23.998.

Hence the area of the sector is 749.937.

Ex. 2. What is the area of a sector whose arc is 25°, in a circle whose radius is 44 rods?

Ans., 422.367 rods.

Ex. 3. What is the area of a sector less than a semicircle. whose chord is 6 feet, in a circle whose radius is 9 feet?

Ans., 27.522 feet

PROBLEM XI.

(100.) To find the area of a segment of a circle.

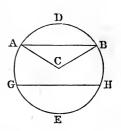
RULE.

Find the area of the sector which has the same arc, and also the area of the triangle formed by the chord of the segment and the radii of the sector.

Then take the sum of these areas if the segment is greater than a semicircle, but take their difference if it is less

It is obvious that the segment AEB is equal to the sum of the sector ACBE and the triangle ACB, and that the segment ADB is equal to the difference between the sector ACBD and the triangle ACB.

Ex. 1. What is the area of a segment whose arc contains 280°, in a circle whose diameter is 50?



The whole circle = 1963.495The sector = 1527.163The triangle = 307.752The segment = 1834.915, Ans.

Ex. 2. What is the area of a segment whose chord is 20 feet, and height 2 feet?

Ans., 26.8788 feet.

Ex. 3. What is the area of a segment whose arc is 25°, in a circle whose radius is 44 rods?

Ans.

- (101.) The area of the zone ABHG, included between two parallel chords, is equal to the difference between the segments GDH and ADB.
- Ex. 4. What is the area of a zone, one side of which is 96, and the other side 60, and the distance between them 26?

 Ans., 2136.7527.

The radius of the circle in this example will be found to be 50.

PROBLEM XII.

(102.) To find the area of a ring included between the cir cumferences of two concentric circles.

Rule.

Take the difference between the areas of the two circles; or. Subtract the square of the less radius from the square of the greater, and multiply their difference by 3.14159.

For, according to Geometry, Prop. 13, Cor. 3, B. VI., the area of the greater circle is equal to πR^2 , and the area of the smaller, πr^2 .

Their difference, or the area of the ring, is π (R²-r²).

Ex. 1. The diameters of two concentric circles are 60 and 50. What is the area of the ring included between their circumferences?

Ans., 863.938.

Ex. 2. The diameters of two concentric circles are 320 and 280 What is the area of the ring included between their circumferences?

Ans., 18849.55

PROBLEM XIII.

(103.) To find the area of an ellipse.

RULE.

Multiply the product of the semi-axes by 3.14159.

For demonstration, see Geometry, Ellipse, Prop. 21.

Ex. 1. What is the area of an ellipse whose major axis in 70 feet, and minor axis 60 feet?

Ans., 3298.67 feet.

Ex. 2. What is the area of an ellipse whose axes are 340 and 310?

Ans., 82780.896

PROBLEM XIV.

(104.) To find the area of a parabola.

Rule.

Multiply the base by two thirds of the height.

For demonstration, see Geometry, Parabola, Prop. 12.

Ex. 1. What is the area of a parabola whose base is 18 feet, and height 5 feet?

Ans., 60 feet.

Ex. 2. What is the area of a parabola whose base is 525 feet, and height 350 feet?

Ans., 122500 feet

MENSURATION OF SOLIDS.

(105.) The common measuring unit of solids is a *cube*, whose faces are squares of the same name; as, a cubic inch, a cubic foot, &c. This measuring unit is not, however, of

necessity a cube whose faces are squares of the same name. Thus a bushel may have the form of a cube, but its faces can only be expressed by means of some unit of a different denomination. The following is

The Table of Solid Measure.

1728 cubic inches = 1 cubic foot.

27 cubic feet = 1 cubic yard.

 $4492\frac{1}{8}$ cubic feet = 1 cubic rod.

231 cubic inches = 1 gallon (liquid measure).

268.8 cubic inches = 1 gallon (dry measure).

2150.4 cubic inches = 1 bushel.

PROBLEM I.

(106.) To find the surface of a right prism.

Rule.

Multiply the perimeter of the base by the altitude for the convex surface. To this add the areas of the two ends when the entire surface is required.

See Geometry, Prop. 1, B. VIII.

Ex. 1. What is the entire surface of a parallelopiped whose altitude is 20 feet, breadth 4 feet, and depth 2 feet?

Ans., 256 square feet.

Ex. 2. What is the entire surface of a pentagonal prism whose altitude is 25 feet 6 inches, and each side of its base 3 feet 9 inches?

Ans., 526.513 square feet.

Ex. 3. What is the entire surface of an octagonal prism whose altitude is 12 feet 9 inches, and each side of its base 2 feet 5 inches?

Ans., 302.898 square funt.

PROBLEM II.

(107.) To find the solidity of a prism.

RULE.

Multiply the area of the base by the altitude. See Geometry, Prop. 11. B. VIII.

Ex. 1. What is the solidity of a parallelopiped whose altitude is 30 feet, breadth 6 feet, and depth 4 feet?

Ans., 720 cubic feet.

- Ex. 2. What is the solidity of a square prism whose altitude is 8 feet 10 inches, and each side of its base 2 feet 3 inches?

 Ans., $44\frac{23}{33}$ cubic feet.
- Ex. 3 What is the solidity of a pentagonal prism whose attitude is 20 feet 6 inches, and its side 2 feet 7 inches?

 Ans., 235.376 cubic feet.

PROBLEM III.

(108.) To find the surface of a regular pyramid.

RULE.

• Multiply the perimeter of the base by half the slant height for the convex surface. To this add the area of the base when the entire surface is required.

See Geometry, Prop. 14, B. VIII.

- Ex. 1. What is the entire surface of a triangular pyramid whose slant height is 25 feet, and each side of its base 5 feet?

 Ans., 198.325 square feet.
- Ex. 2. What is the entire surface of a square pyramid whose slant height is 30 feet, and each side of the base 4 feet?

 Ans., 256 square feet.
- Ex. 3. What is the entire surface of a pentagonal pyramid whose slant height is 20 feet, and each side of the base 3 feet?

Ans., 165.484 square feet.

PROBLEM IV.

(109.) To find the solidity of a pyramid.

RULE.

Multiply the area of the base by one third of the altitude. See Geometry, Prop. 17, B. VIII.

Ex. 1. What is the solidity of a triangular pyramid whose altitude is 25 feet, and each side of its base 6 feet?

Ans., 129.904 cubic feet

Ex. 2. What is the solidity of a square pyramid whose slant height is 22 feet, and each side of its base 10 feet?

Ans., 714.143 cubic feet.

Ex. 3. What is the solidity of a pentagonal pyramid whose altitude is 20 feet, and each side of its base 3 feet?

Ans., 103.228 cubic feet.

PROBLEM V.

(110.) To find the surface of a frustum of a regular pyramid.

Rule.

Multiply half the slant height by the sum of the perimeters of the two bases for the convex surface. To this add the areas of the two bases when the entire surface is required.

See Geometry, Prop. 14, Cor. 1, B. VIII.

Ex. 1. What is the entire surface of a frustum of a square pyramid whose slant height is 15 feet, each side of the greater base being 4 feet 6 inches, and each side of the less base 2 feet 10 inches?

Ans., 248.278 square feet.

Ex. 2. What is the entire surface of a frustum of an octagonal pyramid whose slant height is 14 feet, and the sides of the ends 3 feet 9 inches, and 2 feet 3 inches?

Ans., 428.344 square feet.

PROBLEM VI.

(111.) To find the solidity of a frustum of a pyramid.

Rule.

Add together the areas of the two bases, and a mean proportional between them, and multiply the sum by one third of the altitude.

See Geometry, Prop. 18, B. VIII.

When the pyramid is regular, it is generally most convenient to find the area of its base by Rule II., Art. 92. If we put a to represent one side of the lower base, and b one side of the upper base, and the tabular number from Art. 92 by

T, the area of the lower base will be a^2T ; that of the upper base will be b^2T ; and the mean proportional will be abT. Hence, if we represent the height of the frustum by h, its solidity will be

$$(a^2+b^2+ab)\frac{hT}{3}$$
.

Ex. 1. What is the solidity of a frustum of an hexagonal pyramid whose altitude is 15 feet, each side of the greater end being 3 feet, and that of the less end 2 feet?

Ans., 246.817 cubic feet.

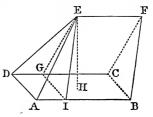
Ex. 2. What is the solidity of a frustum of an octagonal pyramid whose altitude is 9 feet, each side of the greater end being 30 inches, and that of the less end 20 inches?

Ans., 191.125 cubic feet.

Definition.

(112.) A wedge is a solid bounded by five planes, viz., a rec-

tangular base, ABCD, two trapezoids, ABFE, DCFE, meeting in an edge, and two triangular ends, ADE, BCF. The altitude of the wedge is the perpendicular drawn from any point in the edge to the plane of the base, as EH.



PROBLEM VII.

(113.) To find the solidity of a wedge.

Rule.

Add the length of the edge to twice the length of the base, and multiply the sum by one sixth of the product of the height of the wedge and the breadth of the base.

Demonstration.

Put L=AB, the length of the base;

" l=EF, the length of the edge;

" b=BC, the breadth of the base;

" h=EH, the altitude of the wedge.

Now, if the length of the base is equal to that of the edge,

it is evident that the wedge is half of a prism of the same base and height. If the length of the base is greater than that of the edge, let a plane, EGI, be drawn parallel to BCF. The wedge will be divided into two parts, viz., the pyramid E-AIGD, and the triangular prism BCF-G.

The solidity of the former is equal to $\frac{1}{3}bh(L-l)$, and that of the latter is $\frac{1}{2}bhl$. Their sum is

 $\frac{1}{2}bhl + \frac{1}{3}bh(L-l) = \frac{1}{6}bh3l + \frac{1}{6}bh2L - \frac{1}{6}bh2l = \frac{1}{6}bh(2L+l).$

If the length of the base is less than that of the edge, the wedge will be equal to the difference between the prism and pyramid, and we shall have

 $\frac{1}{2}bhl - \frac{1}{3}bh(l - L),$

which is equal to

 $\frac{1}{2}bhl + \frac{1}{3}bh(\mathbf{L} - l),$

the same result as before.

Ex. 1. What is the solidity of a wedge whose base is 30 inches long and 5 inches broad, its altitude 12 inches, and the length of the edge 2 feet?

Ans., 840 cubic inches.

Ex. 2. What is the solidity of a wedge whose base is 40 inches long and 7 inches broad, its altitude 18 inches, and the length of the edge 30 inches?

Ans., 2310 cubic inches.

Definition.

(114.) A rectangular prismoid is a solid bounded by six planes, of which the two bases are rectangles having their corresponding sides parallel, and the four upright sides of the solid are trapezoids.

PROBLEM VIII.

To find the solidity of a rectangular prismoid.

RULE.

Add together the areas of the two bases, and four times the area of a parallel section equally distant from the bases, and nultiply the sum by one sixth of the altitude.

Demonstration.

Put L and B=length and breadth of one base;

Put l and b = length and breadth of the other base;

" M " m = length and breadth of middle sec.;

" h = the altitude of the prismoid.

It is evident that if a plane be made to pass through the opposite edges of the upper and lower bases, the prismoid will be divided into two wedges, whose bases are the bases of the



prismoid, and whose edges are L and l. The solidity of these wedges, and, consequently, that of the prismoid, is

$$\frac{1}{6}Bh(2L+l)+\frac{1}{6}bh(2l+L)=\frac{1}{6}h(2BL+Bl+2bl+bL).$$

But, since M is equally distant from L and l, we have

$$2M=L+l$$
, and $2m=B+b$;

hence

$$4Mm = (L+l) (B+b) = BL + Bl + bL + bl.$$

Substituting 4Mm for its value in the preceding expression, we obtain for the solidity of the prismoid

$$\frac{1}{6}h(BL+bl+4Mm)$$
.

Ex. 1. What are the contents of a log of wood, in the form of a rectangular prismoid, the length and breadth of one end peing 16 inches and 12 inches, and of the other 7 inches and 4 inches, the length of the log being 24 feet?

Ans., $16\frac{1}{3}$ cubic feet.

Ex. 2. What is the solidity of a log of hewn timber, whose and are 18 inches by 15, and 14 inches by $11\frac{1}{2}$, its length being 18 feet?

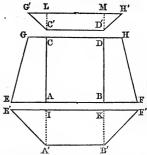
Ans., $26\frac{3}{4}\frac{1}{8}$ cubic feet.

PROBLEM IX.

To compute the excavation or embankment for a rail-way. (115.) By the preceding rule may be computed the amount of excavation or embankment required in constructing a rail-road or canal. If we divide the line of the road into portions to small that each may be regarded as a straight line, and suppose an equal number of transverse sections to be made, the excavation or embankment between two sections may be regarded as a prismoid, and its contents found by the preceding rule.

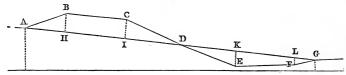
Let ABCD represent the lower surface of the supposed excavation, which we will assume to be parallel to the horizon; and let EFGH represent the upper surface of the excavation projected on a horizontal plane. Also, let E'A'B'F', G'C'D'H

represent the vertical sections at the extremities. If we suppose vertical planes to pass through the lines AC, BD, the middle part of the excavation, or that contained between these vertical planes, will be a rectangular prismoid, of which A'B'KI will be one base, and C'D'ML the other base. Its solidity will therefore be given by Art. 114. The



parts upon each side of the middle prismoid are also halves of rectangular prismoids; or, if the two parts are equal, they may be regarded as constituting a second prismoid, one of whose bases is the sum of the triangles A'E'I, B'F'K; and the other base is the sum of the triangles C'G'L, D'H'M. Therefore the volume of the entire solid is equal to the product of one sixth of its length, by the sum of the areas of the sections at the two extremities, and four times the area of a parallel and equidistant section.

Ex. 1. Let ABCDEFG represent the profile of a tract of



land selected for the line of a rail-way; and suppose it is required, by cutting and embankment, to reduce it from its present hilly surface to one uniform slope from the point A to the point G.

The distance AH is 561 feet; the distance DK is 820 feet;

" " HI is 858 feet; " " KL is 825 feet;

" " ID is 825 feet; " " LG is 320 feet.

The perpendicular BH is 18 feet; the perpendicular KE is 19 feet;

" " CI is 20 feet; " " LF is 8 feet
The annexed figure repre-

sents a cross section, showing the form of the excavation.

The base of the cutting is to



be 50 feet wide, the slope $1\frac{1}{2}$ horizontal to 1 perpendicular; that is, where the depth ad is 10 feet, the width of the slope cd at the surface will be 15 feet.

Calculation of the portion ABH.

Since BH is 18 feet, the length of cd in the cross section will be 27 feet, and cf, the breadth at the top of the section, will be 104 feet. We accordingly find, by Art. 87, the area of the trapezoid forming the cross section at BH equal to

$$\frac{104+50}{2}$$
 × 18=1386 feet.

For the middle section, the height is \Im feet, cd is 13.5 feet, and cf is 77 feet. The area of the cross section is therefore equal to

$$\frac{77+50}{2}$$
 × 9=571.5.

The solid ABH will therefore be equal to

$$(1386+(4\times571.5))\frac{561}{6}=343332$$
 cubic feet, or

12716 cubic yards.

Calculation of the portion BCIH.

Since CI is 20 feet, the length of cd is 30 feet, and cf is 11.0 feet. The area of the section at CI is therefore equal to

$$\frac{110+50}{2}$$
 × 20=1600.

For the middle section, the height is 19 feet, cd is 28.5 feet, and cf is 107 feet. The area of the cross section is therefore equal to

$$\frac{107+50}{2}$$
 × 19 = 1491.5.

The solid BCIH will therefore be equal to

$$(1386+1600+(4\times1491.5))\frac{858}{6}=1280136$$
 cubic feet, or 47412.4 cubic yards.

Calculation of the portion CID.

The height of the middle section is 10 feet; therefore cf is 80 feet, and the area of the cross section is

$$\frac{80+50}{2}$$
 × 10=650.

The solid CID will therefore be equal to

$$(1600+4\times650)\frac{825}{6}=577500$$
 cubic feet, or

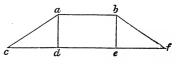
21388.9 cubic yards.

The entire amount of excavation therefore is,

$$BCIH = 47412.4$$

The following is a cross section, showing the firm of the embankment.

The top of the embankment is to be 50 feet wide, the slope 2 to 1; that is, where the height ad is 10 feet, the base cd is to be 20 feet.



Calculation of the portion DKE.

Since EK is 19 feet, the length of cd is 38 feet, and cf is 126 feet. The area of the cross section at EK is therefore equal to

$$\frac{126+50}{2}$$
 × 19=1672.

For the middle section, the height is 9.5 feet; cd is therefore 19 feet, and cf is 88 feet. The area of the cross section is therefore

$$\frac{88+50}{2} \times 9.5 = 655.5$$

The solid DKE is therefore equal to

$$(1672 + (4 \times 655.5) \frac{820}{6} = 586846.7$$
 cubic feet, or

21735.1 cubic yards.

Calculation of the portion KEFL.

Since LF is 8 feet, cd is 16 feet, and cf is 82 feet. The area of the section at LF is therefore equal to

$$\frac{82+50}{2} \times 8 = 528.$$

The height of the middle section is 13.5 feet; therefore cd is 27 feet, and cf is 104 feet. The area of the cross section is therefore equal to

 $\frac{104+50}{2}$ × 13.5=1039.5.

The solid KEFL will therefore be equal to

$$(1672+528+4\times1039.5)\frac{825}{6}$$
=874225 cubic feet, or 32378.7 cubic yards.

Calculation of the portion LFG.

The height of the middle section is 4 feet; therefore cf is 66 reet, and the area of the cross section is equal to

$$\frac{66+50}{2}$$
 × 4=232.

The solid LFG will therefore be equal to

$$(528+4\times232)\frac{330}{6}$$
 = 80080 cubic feet, or

2965.9 cubic yards.

The entire amount of embankment therefore is

DKE=21735.1 cubic yards.

Total embankment, 57079.7

* Ex. 2. Compute the amount of excavation of the hill ABCD from the following data:

The distance AH is 325 feet; the perpendicular BH is 12 feet;

" " HI is 672 feet; " " CI is 13 feet.

" " ID is 534 feet.

The base of the cutting to be 50 feet wide, and the slope 1½ norizontal to 1 perpendicular.

Ans., 33969 cubic yards.

PROBLEM X.

(116.) To find the surface of a regular polyedron.

Rule.

Multiply the area of one of the faces by the number of

faces; or, Multiply the square of one of the edges by the surface of a similar solid whose edge is unity.

Since all the faces of a regular polyedron are equal, it is evident that the area of one of them, multiplied by their number, will give the entire surface. Also, regular solids of the same name are similar, and similar polygons are as the squares of their homologous sides (*Geom.*, Prop. 26, B. IV.). The following table shows the surface and solidity of regular polyedrons whose edge is unity. The surface is obtained by multiplying the area of one of the faces, as given in Art. 92, by the number of faces. Thus the area of an equilateral triangle, whose side is 1, is 0.4330127. Hence the surface of a regular tetraedron

 $=.4330127 \times 4 = 1.7320508$,

and so on for the other solids.

A Table of the regular Polyedrons whose Edges are unity

Names.	No. of Faces.	_ Surface.	Solidity.
Tetraedron,	4	1.7320508	0.1178513.
Hexaedron,	6	6.0000000	1.0000000.
Octaedron,	8	3.4641016	0.4714045
Dodecaedron,	12	20.6457288	7.6631189.
Icosaedron,	20	8.6602540	2.1816950.

Ex. 1. What is the surface of a regular octaedron whose edges are each 8 feet?

Ans., 221.7025 feet.

Ex. 2. What is the surface of a regular dodecaedron whose edge is 12 feet?

Ans., 2972.985 feet.

PROBLEM XI.

(117.) To find the solidity of a regular polyedron.

RULE.

Multiply the surface by one third of the perpendicular let full from the center on one of the faces; or, Multiply the subset of one of the edges by the solidity of a similar polyedron, whose edge is unity.

Since the faces of a regular polyedron are similar and equal,

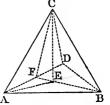
and the solid angles are all equal to each other, it is evident that the faces are all equally distant from a point in the solid called the center. If planes be made to pass through the center and the several edges of the solid, they will divide it into as many equal pyramids as it has faces. The base of each pyramid will be one of the faces of the polyedron; and since their altitude is the perpendicular from the center upon one of the faces, the solidity of the polyedron must be equal to the areas of all the faces, multiplied by one third of this perpendicular.

Also, similar pyramids are to each other as the cubes of their homologous edges (*Geom.*, Prop. 17, Cor. 3, B. VIII.). And since two regular polyedrons of the same name may be divided into the same number of similar pyramids, they must be to each other as the cubes of their edges.

(118.) The solidity of a tetraedron whose edge is unity, may be computed in the following manner:

Let C-ABD be a tetraedron. From one angle, C, let fall

a perpendicular, CE, on the opposite face; draw EF perpendicular to AD; and join CF, AE. Then AEF is a right-angled triangle, in which EF, being the sine of 30°, is one half of AE or BE; and therefore FE is one third of BF or CF. Hence the cosine of the angle CFE is equal to $\frac{1}{3}$; that is the angle of inclination of the faces of the



is, the angle of inclination of the faces of the polyedron is 70° , 31' 44''. Also, in the triangle CAF, CF is the sine of 60° , which is 0.866025. Hence, in the right-angled triangle CEF, knowing one side and the angles, we can compute CE, which is found to be 0.8164966. Whence, knowing the base ABD (Art. 92), we obtain the solidity of the tetraedron = 0.1178513.

In a somewhat similar manner may the solidities of the other regular polyedrons, given in Art. 116, be obtained.

Ex. 1. What is the solidity of a regular tetraedron whose edges are each 24 inches?

Ans., 0.9428 feet.

Ex. 2. What is the solidity of a regular icosaedron whose edges are each 20 feet?

Ans., 17453.56 feet.

THE THREE ROUND BODIES.

PROBLEM I.

(119.) To find the surface of a cylinder.

RULE.

Multiply the circumference of the base by the altitude for the convex surface. To this add the areas of the two ends when the entire surface is required.

See Geometry, Prop. 1, B. X.

Ex. 1. What is the convex surface of a cylinder whose altitude is 23 feet, and the diameter of its base 3 feet?

Ans., 216.77 square feet.

Ex. 2. What is the entire surface of a cylinder whose altitude is 18 feet, and the diameter of its base 5 feet?

Ans.

PROBLEM II.

(120.) To find the solidity of a cylinder.

RULE.

Multiply the area of the base by the altitude.

See Geometry, Prop. 2, B. X.

Ex. 1. What is the solidity of a cylinder whose altitude is 18 feet 4 inches, and the diameter of its base 2 feet 10 inches?

Ans., 115.5917 cubic feet.

Ex. 2. What is the solidity of a cylinder whose altitude is 12 feet 11 inches, and the circumference of its base 5 feet 3 inches?

Ans., 28.3308 cubic feet.

Problem III.

(121.) To find the surface of a cone.

Rule.

Multiply the circumference of the base by half the side for the convex surface; to which add the area of the base when the entire surface is required.

See Geometry, Prop. 3, B. X.

Ex. 1. What is the entire surface of a cone whose side is 10 feet and the diameter of its base 2 feet 3 inches?

Ans., 39.319 square feet.

Ex. 2. What is the entire surface of a cone whose side is 15 feet, and the circumference of its base 8 feet?

Ans., 65.093 square feet.

PROBLEM IV:

(122.) To find the solidity of a cone.

RULE.

Multiply the area of the base by one third of the altitude. See Geometry, Prop. 5, B. X.

Ex. 1. What is the solidity of a cone whose altitude is 12 feet, and the diameter of its base $2\frac{1}{2}$ feet?

Ans., 19.635 cubic feet.

Ex. 2. What is the solidity of a cone whose altitude is 25 feet, and the circumference of its base 6 feet 9 inches?

Ans.

PROBLEM V.

(123.) To find the surface of a frustum of a cone.

Rule.

Multiply half the side by the sum of the circumferences of the two bases for the convex surface; to this add the areas of the two bases when the entire surface is required.

See Geometry, Prop. 4, B. X.

Ex. 1. What is the entire surface of a frustum of a cone, the diameters of whose bases are 9 feet and 5 feet, and whose side is 16 feet 9 inches?

Ans., 451.6036 square feet.

Ex. 2. What is the convex surface of a frustum of a cone whose side is 10 feet, and the circumferences of its bases 6 feet and 4 feet?

Ans., 50 square feet.

PROBLEM VI.

(124.) To find the solidity of a frustum of a cone.

RULE

Add together the areas of the two bases, and a mean proportional between them, and multiply the sum by one third of the altitude.

See Geometry, Prop. 6, B. X.

If we put R and r for the radii of the two bases, then πR^2 will represent the area of one base, πr^2 the area of the other, and $\pi R r$ the mean proportional between them. Hence, if we represent the height of the frustum by h, its solidity will be

$$\frac{\pi h}{3}(\mathbf{R}^2+r^2+\mathbf{R}r).$$

Ex. 1. What is the solidity of a frustum of a cone whose altitude is 20 feet, the diameter of the greater end 5 feet, and that of the less end 2 feet 6 inches?

Ans., 229.074 cubic feet

Ex. 2. The length of a mast is 60 feet, its diameter at the greater end is 20 inches, and at the less end 12 inches: what is its solidity?

Ans., 85.521 cubic feet

PROBLEM VII.

t (125.) To find the surface of a sphere.

Rule.

Multiply the diameter by the circumference of a great circle; or, Multiply the square of the diameter by 3.14159

See Geometry, Prop. 7, B. X.

Ex. 1. Required the surface of the earth, its diameter being 7912 miles.

Ans., 196,662,896 square miles.

Ex. 2. Required the surface of the moon, its circumference being 6786 miles.

Ans.

PROBLEM VIII.

(126.) To find the solidity of a sphere.

RULE.

* Multiply the surface by one third of the radius; or, Multiply the cube of the diameter by $\frac{1}{6}\pi$; that is, by 0.5236.

See Geometry, Prop. 8, B. X.

Where great accuracy is required, the value of $\frac{1}{6}\pi$ must be

taken to more than four decimal places. Its value, correct to ten decimal places, is .52359,87756.

Ex. 1. What is the solidity of the earth, if it be a sphere 7912 miles in diameter?

Ans., 259,332,805,350 cubic miles.

Ex. 2. If the diameter of the moon be 2160 miles, what is its solidity?

Ans.

PROBLEM IX.

(127.) To find the surface of a spherical zone.

Rule.

Multiply the altitude of the zone by the circumference of a great circle of the sphere.

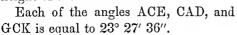
See Geometry, Prop. 7, Cor. 1, B. X.

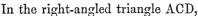
Ex. 1. If the diameter of the earth be 7912 miles, what is the surface of the torrid zone, extending 23° 27′ 36″ on each side of the equator?

Ans., 78,293,218 square miles

Let PEP'Q represent a meridian of the earth; EQ the

equator; P, P' the poles; AB one of the tropics, and GH one of the polar circles. Then PK will represent the height of one of the frigid zones, KD the height of one of the temperate zones, and CD half the height of the torrid zone.





 $R:AC::\sin_{\bullet}CAD:CD$

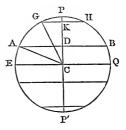
Also, in the ight-angled triangle CGK,

R: CG:: cos. GCK: CK,

Then PK=PC-KC.

Where great accuracy is required, the sine and cosine of 23° 27′ 36″ must be taken to more than six decimal places. The following values are correct to ten decimal places:

Natural sine of 23° 27′ 36″=.39810,87431. " cosine of 23° 27′ 36″=.91733,82302.



Ex. 2. If the polar circle extends 23° 27′ 36″ from the pole find the convex surface of either frigid zone.

Ans., 8,128,252 square miles.

Ex. 3. On the same suppositions, find the surface of each of the temperate zones.

Ans., 51,056,587 square miles.

PROBLEM X.

(128.) To find the solidity of a spherical segment with one base.

RULE.

Multiply half the height of the segment by the area of the base, and the cube of the height by .5236, and add the two products.

See Geometry, Prop. 9, B. X.

Ex. 1. What is the solidity of either frigid zone, supposing the earth to be 7912 miles in diameter, the polar circles extending 23° 27′ 36″ from the poles?

Ans., 1,292,390,176 cubic miles.

- (129.) The solidity of a spherical segment of two bases is the difference between two spherical segments, each having a single base.
- Ex. 2. On the same supposition as in Ex. 1, find the solidity of either temperate zone.

Ans., 55,032,766,543 cubic miles

Ex. 3. Find the solidity of the torrid zone.

Ans., 146,682,491,911 cubic miles

PROBLEM XI.

(130.) To find the area of a spherical triangle.

RULE.

Compute the surface of the quadrantal triangle, or one eighth of the surface of the sphere. From the sum of the three angles subtract two right angles; divide the remainder by 90, and multiply the quotient by the quadrantal triangle See Geometry, Prop. 20, B. IX.

Ex. 1. What is the area of a triangle on a sphere whose diameter is 10 feet, if the angles are 55°, 60°, and 85°?

Ans., 8.7266 square feet.

Ex. 2. If the angles of a spherical triangle measured on the surface of the earth are 78° 4′ 10″, 59° 50′ 54″, and 42° 5′ 37″, what is the area of the triangle, supposing the earth a sphere, of which the diameter is 7912 miles?

Ans., 3110.794 square miles.

If the excess of the angles above two right angles is expressed in seconds, we must divide it by 90 degrees also expressed in seconds; that is, by 324,000.

PROBLEM XII.

(131.) To find the area of a spherical polygon.

Rule.

Compute the surface of the quadrantal triangle. From the sum of all the angles subtract the product of two right angles by the number of sides less two; divide the remainder by 90, and multiply the quotient by the quadrantal triangle.

See Geometry, Prop. 21, B. IX.

Ex. 1. What is the area of a spherical polygon of 5 sides on a sphere whose diameter is 10 feet, supposing the sum of the angles to be 640 degrees?

Ans., 43.633 square feet 62° 33′ 13″;

Ex. 2. The angles of a spherical polygon, measured on the surface of the earth, are

135° 8′ 26″; 149° 16′ 9″; 111° 45′ 8″; 105° 59′ 7″; 155° 19′ 12″.

Required the area of the polygon.

Ans., 5690.477 square miles

BOOK IV.

SURVEYING

(132.) The term Surveying includes the measurement of heights and distances, the determination of the area of portions of the earth's surface, and their delineation upon paper.

Since the earth is spherical, its surface is not a plane surtace, and if large portions of the earth are to be measured, the curvature must be taken into account; but in ordinary surveying, the portions of the earth are supposed to be so small that the curvature may be neglected. The parts surveyed are therefore regarded as plane figures.

(133.) If a plummet be freely suspended by a line, and allowed to come to a state of rest, this line is called a *vertical tine*.

Every plane passing through a vertical line is a vertica. plane.

A line perpendicular to a vertical line is a horizontal line.

A plane perpendicular to a vertical line is a horizontal plane.

A vertical angle is one the plane of whose sides is vertical. A horizontal angle is one the plane of whose sides is horizontal.

An angle of elevation is a vertical angle having one side horizontal and the other an ascending

line, as the angle BAD.

An angle of depression is a vertical angle having one side horizontal and the other a descending line, as the angle CDA.

(134.) When distances are to be found A B by trigonometrical computation, it is necessary to measure at least one line upon the ground, and also as many angles as may be necessary to render three parts of every triangle known

In the measurement of lines, the unit commonly employed by surveyors is a chain four rods or sixty-six feet in length, called *Gunter's Chain*, from the name of the inventor. This chain is divided into 100 links. Sometimes a half chain is used, containing 50 links.

Hence, 1 chain= 100 links = 66 feet; 1 rod = 25 links = $16\frac{1}{2}$ feet; 1 link = 7.92 inches= $\frac{2}{3}$ of a foot nearly.

(135.) To measure a horizontal line.

To mark the termination of the chain in measuring, ten iron pins should be provided, about a foot in length.

Let the person who is to go foremost in carrying the chain, and who is called the leader, take one end of the chain and the ten pins; and let another person take the other end of the chain, and hold it at the beginning of the line to be measured. When the leader has advanced until the chain is stretched tight, he must set down one pin at the end of the chain, the other person taking care that the chain is in the direction of the line to be measured. Then measure a second chain in the same manner, and so on until all the marking pins are exhausted. A record should then be made that ten chains have been measured, after which the marking pins should be returned to the leader, and the measurement continued as before until the whole line has been passed over.

It is generally agreed to refer all surfaces to a horizontal plane. Hence, when an inclined surface, like the side of a hill, is to be measured, the chain should be maintained in a horizontal position. For this purpose, in ascending a hill, the hind end of the chain should be raised from the ground until it is on a level with the fore end, and should be held vertically over the termination of the preceding chain. In descending a hill, the fore end of the chain should be raised in the same manner.

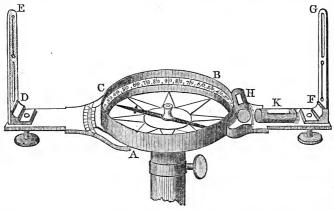
INSTRUMENTS FOR MEASURING ANGLES.

In measuring angles, some instrument is used which contains a portion of a graduated circle divided into degrees and minutes These instruments may be adapted to measuring

either horizontal or vertical angles. The instrument most frequently employed for measuring horizontal angles is called

THE SURVEYOR'S COMPASS.

(136.) The principal parts of this instrument are a compassbox, a magnetic needle, two sights, and a stand for its support. The compass-box, ABC, is circular, generally about six inches in diameter, and at its center is a small pin on which the magnetic needle is balanced. The circumference of the box is divided into degrees, and sometimes to half degrees; and the degrees are numbered from the extremities of a diameter both ways to 90°. The sights, DE, FG, are placed at right angles



to the plane of the graduated circle, and in each of these there is a large and small aperture for convenience of observation. The instrument, when used, is mounted on a tripod, or a single staff pointed with iron at the bottom, so that it may be firmly placed in the ground.

Sometimes two spirit levels, H and K, are attached, to indicate when the plane of the graduated circle is brought into a horizontal position.

(137.) When the magnetic needle is supported so as to turn freely, and is allowed to come to a state of rest, the direction it assumes is called the *magnetic meridian*, one end of the needle indicating the north point and the other the south.

A horizontal line perpendicular to a meridian is an east and west line

All the meridians passing through a survey of moderate extent, are considered as straight lines parallel to each other.

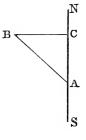
The bearing or course of a line is the angle which it makes with a meridian passing through one end; and it is reckoned from the north or south point of the horizon, toward the east or west.

Thus, if NS represent a meridian, and the angle NAB is 40°.

then the bearing of AB from the point A is 40° to the west of north, and is written N. 40° W., and read north forty degrees west.

The reverse bearing of a line is the bearing taken from the other end of the line.

The forward bearing and reverse bearing of a line are equal angles, but lie between directly opposite points. Thus, if the bearing of AB from A is N. 40° W., the bearing of the same line from B is S. 40° E.

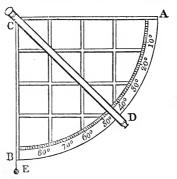


(138.) For measuring vertical angles, the instrument commonly used is

A QUADRANT.

It consists of a quarter of a circle, usually made of brass,

and its limb, AB, is divided into degrees and minutes, numbered from A up to 90°. It is furnished either with a pair of plain sights or with a telescope, CD, which is to be directed toward the object observed. A plumb line, CE, is suspended from the center of the quadrant, and indicates when the radius CB is brought into a vertical position.



To measure the angle of elevation, for example, of the top of a tower, point the telescope, CD, toward the tower, keeping the radius, CB, in a vertical position by means of the plumb line, CE. Move the telescope until the given object is seen in the middle of the field of view. The center of the field is indicated by two wires placed in the focus of the object-glass of

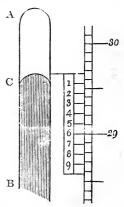
the telescope, one wire being vertical and the other horizontal. When the horizontal wire is made to coincide with the summit of the tower, the angle of elevation is shown upon the arc AB by means of an index which moves with the telescope.

As the arc is not commonly divided into parts smaller than half degrees, when great accuracy is required, some contrivance is needed for obtaining smaller fractions of a degree. This is usually effected by a vernier.

(139.) A Vernier is a scale of small extent, graduated in such a manner that, being moved by the side of a fixed scale, we are enabled to measure minute portions of this scale. The length of this movable scale is equal to a certain number of parts of that to be subdivided, but it is divided into parts one more or one less than those of the primary scale taken for the length of the vernier. Thus, if we wish to measure hundredths of an inch, as in the case of a barometer, we first divide an inch into ten equal parts. We then construct a vernier equal in length to 11 of these divisions, but divide it into 10 equal parts, by which means each division on the vernier is $\frac{1}{10}$ th longer than a division of the primary scale.

Thus, let AB be the upper end of a barometer tube, the mer-

cury standing at the point C; the scale is divided into inches and tenths of an inch, and the middle piece, numbered from 1 to 9, is the vernier that slides up and down, having 10 of its divisions equal to 11 divisions of the scale, that is, to $\frac{1}{10}$ ths of an inch. Therefore, each division of the vernier is $\frac{1}{100}$ ths of an inch; or one division of the vernier exceeds one division of the scale by $\frac{1}{100}$ th of an inch. Now, as the sixth division of the vernier (in the figure) coincides with a division of the scale, the fifth division of the ver-



nier will stand $\frac{1}{1000}$ th of an inch above the nearest division of the scale; the fourth division $\frac{2}{1000}$ ths of an inch, and the top of the vernier will be $\frac{6}{1000}$ ths of an inch above the next lower division of the scale; *i. e.*, the top of the vernier coincides with 29 66 inches upon the scale. In practice, therefore, we ob-

serve what division of the vernier coincides with a division of the scale; this will show the hundredths of an inch to be added to the tenths next below the vernier at the top.

A similar contrivance is applied to graduated circles, to obtain the value of an arc with greater accuracy. If a circle is graduated to half degrees, or 30', and we wish to measure single minutes by the vernier, we take an arc equal to 31 divisions upon the limb, and divide it into 30 equal parts. Then each division of the vernier will be equal to $\frac{3}{6}$ ths of a degree, while each division of the scale is $\frac{3}{6}$ ths of a degree. That is, each space on the vernier exceeds one on the limb by 1'.

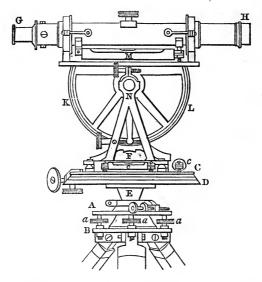
In order, therefore, to read an angle for any position of the vernier, we pass along the vernier until a line is found coinciding with a line of the limb. The number of this line from the zero point indicates the minutes which are to be added to the degrees and half degrees taken from the graduated circle. Sometimes a vernier is attached to the common surveyor's compass.

(140.) An instrument in common use for measuring both horizontal and vertical angles is

THE THEODOLITE.

The theodolite has two circular brass plates, C and D (see fig. next page), the former of which is called the *vernier plate*, and the latter the *graduated limb*. Both have a horizontal motion about the vertical axis, E. This axis consists of two parts, one external, and the other internal; the former secured to the graduated limb, D, and the latter to the vernier plate, C, so that the vernier plate turns freely upon the lower. The edge of the lower plate is divided into degrees and half degrees, and this is subdivided by a vernier attached to the upper plate into single minutes. The degrees are numbered from 0 to 360.

The parallel plates, A and B, are held together by a ball which rests in a socket. Four screws, three of which, a, a, a, are shown in the figure, turn in sockets fixed to the lower plate, while their heads press against the under side of the upper plate, by which means the instrument is leveled for observation. The whole rests upon a tripod, which is firmly attached to the body of the instrument.



To the vernier plate, two spirit-levels, c, c, are attached at right angles to each other, to determine when the graduated limb is horizontal. A compass, also, is placed at F. Two frames, one of which is seen at N, support the pivots of the horizontal axis of the vertical semicircle KL, on which the telescope, GH, is placed. One side of the vertical arc is divided into degrees and half degrees, and it is divided into single minutes by the aid of its vernier. The graduation commences at the middle of the arc, and reads both ways to 90°. Under and parallel to the telescope is a spirit-level, M, to show when the telescope is brought to a horizontal position. To enable us to direct the telescope upon an object with precision, two lines called wires are fixed at right angles to each other in the focus of the telescope.

To measure a Horizontal Angle with the Theodolite.

(141.) Place the instrument exactly over the station from which the angle is to be measured; then level the instrument by means of the screws, a, a, bringing the telescope over each pair alternately until the two spirit-levels on the vernier plate retain their position, while the instrument is turned entirely round upon its axis. Direct the telescope to one of the objects

to be observed, moving it until the cross-wires and object coincide. Now read off the degrees upon the graduated limb, and the minutes indicated by the vernier. Next, release the upper plate (leaving the graduated limb undisturbed), and move it round until the telescope is directed to the second object, and make the cross-wires bisect this object, as was done by the first. Again, read off the vernier; the difference between this and the former reading will be the angle required.

The magnetic bearing of an object is determined by simply reading the angle pointed out by the compass-needle when the object is bisected.

To measure an Angle of Elevation with the Theodolite.

(142.) Direct the telescope toward the given object so that it may be bisected by the horizontal wire, and then read off the arc upon the vertical semicircle. After observing the object with the telescope in its natural position, it is well to revolve the telescope in its supports until the level comes uppermost, and repeat the observation. The mean of the two measures may be taken as the angle of elevation.

By the aid of the instruments now described, we may determine the distance of an inaccessible object, and its height above the surface of the earth.

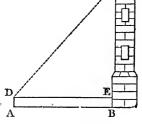
HEIGHTS AND DISTANCES.

PROBLEM I.

(143.) To determine the height of a vertical object situatea on a horizontal plane.

Measure from the object to any convenient distance in a straight line, and then take the angle of elevation subtended by the object.

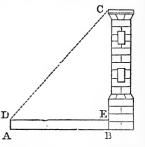
If we measure the distance DE, and the angle of elevation CDE, there will be given, in the right-angled triangle CDE, the base and the angles, to find the perpendicular CE (Art. 46). To this we must add the height of the instrument, to obtain the entire height of the object alove the plane AB.



Ex. 1. Having measured AB equal to 100 feet from the

bottom of a tower on a horizontal plane, I found the angle of elevation, CDE, of the top to be 47° 30′, the center of the quadrant being five feet above the ground. What is the height of the tower?

R: tang. CDE:: DE: CE=109.13. To which add five feet, and we obtain the height of the tower, 114.13 feet.



Ex. 2. From the edge of a ditch 18 feet wide, surrounding a fort, the angle of elevation of the wall was found to be 62° 40′. Required the height of the wall, and the length of a ladder necessary to reach from my station to the top of it.

Ans. The height is 34.82 feet. Length of ladder, 39.20 feet.

PROBLEM II.

(144.) To find the distance of a vertical object whose height is known.

Measure the angle of elevation, and we shall have given the angles and perpendicular of a right-angled triangle to find the base (Art. 46).

Ex. 1. The angle of elevation of the top of a tower whose

height was known to be 143 feet, was found to be 35°. What was its distance?

Here we have given the angles of the triangle ABC, and the side CB, to find AB.

Ans., 204.22 feet.

If the observer were stationed at the A B top of the tower BC, he might find the length of the base AB by measuring the angle of depression DCA, which is equal to BAC.

Ex. 2. From the top of a ship's mast, which was 80 feet above the water, the angle of depression of another ship's hull was found to be 20°. What was its distance?

Ans., 219.80 feet

* PROBLEM III.

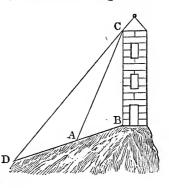
(145.) To find the height of a vertical object standing on an inclined plane.

Measure the distance from the object to any convenient station, and observe the angles which the base-line makes with lines drawn from its two ends to the top of the object.

If we measure the base-line AB, and the two angles ABC,

BAC, then, in the triangle ABC, we shall have given one side and the angles to find BC.

Ex. 1. Wanting to know the height of a tower standing on an inclined plane, BD, I measured from the bottom of the tower a distance, AB, equal to 165 feet; also the angle ABC, equal to 107° 18′, and the angle BAC, equal to 33° 35′. Required the height of the object.



sin. ACB: AB:: sin. BAC: BC=144.66 feet.

The height, BC, may also be found by measuring the distances BA, AD, and taking the angles BAC, BDC. The difference between the angles BAC and BDC will be the angle ACD. There will then be given, in the triangle DAC, one side and all the angles to find AC; after which we shall have, in the triangle ABC, two sides and the included angle to find BC.

Ex. 2. A tower standing on the top of a declivity, I measured 75 feet from its base, and then took the angle BAC, 47° 50′; going on in the same direction 40 feet further, I took the angle BDC, 38° 30′. What was the height of the tower?

Ans., 117.21 feet.

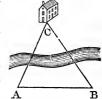
PROBLEM IV.

(146.) To find the distance of an inaccessible object.

Measure a horizontal base-line, and also the angles between this line and lines drawn from each station to the object. Let C • the object inaccessible from A and B. Then, if the distance between the stations A and B be measured, as also the

angles at A and B, there will be given, in the triangle ABC, the side AB and the angles, to find AC and BC, the distances of the object from the two stations.

Ex. 1. Being on the side of a river, and wanting to know the distance to a house which stood on the other side, I measured A



400 yards in a right line by the side of the river, and found that the two angles at the ends of this line, formed by the other end and the house, were 73° 15′ and 68° 2′. What was the distance between each station and the house?

The angle C is found to be 38° 43'. Then

$$sin. C : AB :: \begin{cases} sin. A : BC=612.38; \\ sin. B : AC=593.09. \end{cases}$$

Ex. 2. Two ships of war, wishing to ascertain their distance from a fort, sail from each other a distance of half a mile, when they find that the angles formed between a line from one to the other, and from each to the fort, are 85° 15′ and 83° 45′. What are the respective distances from the fort?

Ans., 4584.52 and 4596.10 yards.

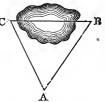
PROBLEM V.

(147.) To find the distance between two objects separated by an impassable barrier.

Measure the distance from any convenient station to each of the objects, and the angle included between those lines.

If we wish to know the distance between the places C and

B, both of which are accessible, but separated from each other by water, we may measure the lines AC and AB, and also the angle A. We shall then have given two sides of a triangle and the included angle to find the third side.



Ex. 1. The passage between the two A objects C and B being obstructed, I measured from A to C 735 rods, and from A to B 840 rods; also, the angle A, equal to 55° 40′. What is the distance of the places C and B?

Ans., 741.21 rods

Ex. 2. In order to find the distance between two objects, C A B, which could not be directly measured, I measured on C to A 652 yards, and from B to A 756 yards; also, the angle A equal to 142° 25'. What is the distance between the objects C and B?

Ans.

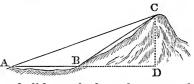
PROBLEM VI.

(148.) To find the height of an inaccessible object above a horizontal plane.

First Method.—Take two stations in a vertical plane passing through the top of the object; measure the distance between the stations and the angle of elevation at each.

If we measure the base AB, and the angles DAC, DBC,

then, since CBA is the supplement of DBC, we shall have, in the triangle ABC, one side and all the angles to find BC. Then, in the right-angled triangle DBC,



right-angled triangle DBC, we shall have the hypothenuse and the angles to find DC.

Ex. 1. What is the perpendicular height of a hill whose angle of elevation, taken at the bottom of it, was 46°; and 100 yards farther off, on a level with the bottom of it, the angle was 31°?

Ans., 143.14 yards.

Ex. 2. The angle of elevation of a spire I found to be 58°, and going 100 yards directly from it, found the angle to be only 32°. What is the height of the spire, supposing the instrument to have been five feet above the ground at each observation?

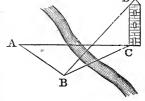
Ans., 104.18 yards.

(149.) Second Method.—Measure any convenient base-line, also the angles between this base and lines drawn from each of its extremities to the foot of the object, and the angle of elevation at one of the stations.

Let DC be the given object. If we measure the horizontal base-line AB, and the angles CAB, CBA, we can compute the distance BC. Also, if we observe the angle of elevation CBD.

we shall have given, in the right-angled triangle BCD, the base and angles to find the perpendicular.

Ex. 1. Being on one side of a river, and wanting to know the height of a spire on the other side, I measured 500 yards, AB, along the side of the river, and found the angle ABC=74° 14′, and BAC=49° 23′; also, the an-



gle of elevation CBD=11° 15′. Required the height of the spire.

Ans., 271.97 feet.

Ex. 2. To find the height of an inaccessible eastle, I measured a line of 73 yards, and at each end of it took the angle of position of the object and the other end, and found the one to be 90°, and the other 61° 45′; also, the elevation of the eastle from the latter station, 10° 35′. Required the height of the eastle.

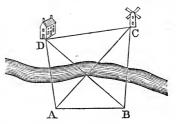
Ans., 86.45 feet

PROBLEM VII.

(150.) To find the distance between two inaccessible objects Measure any convenient base-line, and the angles between this base and lines drawn from each of its extremities to each of the objects.

Let C and D be the two inaccessible objects. If we meas-

ure a base-line, AB, and the angles DAB, DBA, CAB, CBA, then, in the triangle DAB, we shall have given the side AB and all the angles to find BD; also, in the triangle ABC, we shall have one side and all the angles to find BC; and then, in



the triangle BCD, we shall have two sides, BD, BC, with the included angle, to find DC.

Ex. 1. Wanting to know the distance between a house and a mill, which were separated from me by a river, I measured a base-line, AB, 300 yards, and found the angle CAB=58° 20′, CAD=37°, ABD=53° 30′, DBC=45° 15′. What is the distance of the house from the mill?

Ans., 479.80 yards.

Ex. 2. Wanting to know the distance between two inaccessi ble objects, C and D, I measured a base-line, AB, 28.76 rods, and found the angle CAB=33°, CAD=66°, DBA=59° 45′, and DBC=76°. What is the distance from C to D?

Ans., 97.696 rods.

THE DETERMINATION OF AREAS.

(151.) The area or content of a tract of land is the horizontal surface included within its boundaries.

When the surface of the ground is broken and uneven, it is very difficult to ascertain exactly its actual surface. Hence it has been agreed to refer every surface to a horizontal plane; and for this reason, in measuring the boundary lines, it is necessary to reduce them all to horizontal lines.

The measuring unit of surfaces chiefly employed by surveyors is the *acre*, or ten square chains.

One quarter of an acre is called a rood.

Since a chain is four rods in length, a square chain contains sixteen square rods; and an acre, or ten square chains, contains 160 square rods. Square rods are called *perches*. The area of a field is usually expressed in acres, roods, and perches, designated by the letters A., R., P.

When the lengths of the bounding lines of a field are given in chains and links, the area is obtained in square chains and square links. Now, since a link is $\frac{1}{100}$ of a chain, a square link will be $\frac{1}{100} \times \frac{1}{100}$ of a square chain; that is, $\frac{1}{1000} = \frac{1}{1000}$ of a chain. Hence we have the following

TABLE.

1 square chain=10,000 square links.

1 acre=10 square chains=100,000 square links.

1 acre=4 roods=160 perches.

If, then, the linear dimensions are links, the area will be expressed in square links, and may be reduced to square chains by cutting off *four* places of decimals; if *five* places be cut off, the remaining figures will be *acres*. If the decimal part of an acre be multiplied by 4, it will give the roods, and the resulting decimal, multiplied by 40, will give the perches.

(152.) The difference of latitude, or the northing or southing of a line, is the distance that one end is further north of south than the other end.

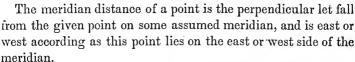
Thus, if NS be a meridian passing through the end A of the line AB, and BC be perpendicular to NS, then is

AC the difference of latitude, or northing of AB.

The departure, or the easting or westing of a .ine, is the distance that one end is further east or west than the other end.

Thus BC is the departure or westing of the line AB.

It is evident that the distance, difference of lattude, and departure form a right-angled triangle, of which the distance is the hypothenuse.



The meridian distance of a line is the distance of the middle point of that line from some assumed meridian.

(153.) When a piece of ground is to be surveyed, we begin at one corner of the field, and go entirely around the field, measuring the length of each of the sides with a chain, and their bearings with a compass.

Plotting a Survey.

When a field has been surveyed, it is easy to draw a plan of it on paper. For this purpose, draw a line to represent the meridian passing through the first station; then lay off an angle equal to the angle which the first side of the field makes with the meridian, and take the length of the side from a scale of equal parts. Through the extremity of this side draw a second meridian parallel to the first, and proceed in the same manner with the remaining sides. This method will be easily understood from an example.

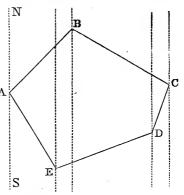
EXAMPLE 1.

Draw a plan of a field from the following courses and distances, as given in the field-book.

Stations.	Bearings.	Distances.
1	N. 45° E.	9.30 chains.
2	S. 60° E.	11.85 "
3	S. 20° W.	5.30 "
4	s. 70° W.	10.90 "
5	N. 31° W.	9.40 "

Draw NS to represent a meridian line; in NS take any convenient point, as A, for the first station, and lay off an angle,

NAB, equal to 45°, the bearing from A to B, which will give the direction from A to B. Then, from the scale of equal parts, make AB equal to 9.30, the length of the first side; this will give the station B. Through B draw a second meridian parallel to NS; lay off an angle of 60°, and make the line BC equal to 11.85. Proceed in the same



manner with the other sides. If the survey is correct, and the plotting accurately performed, the end of the last side, EA, will fall on A, the place of beginning. This plot is made on a scale of 10 chains to an inch.

(154.) To avoid the inconvenience of drawing a meridian through each angle of the field, the sides may be laid down from the angles which they make with each other, instead of the angles which they make with the meridian. Reverse one of the bearings, if necessary, so that both bearings may run from the same angular point; then the angle which any two contiguous sides make with each other may be determined from the following

Rules.

- 1. If both courses are north or south, and both east or west, subtract the less from the greater.
- 2. If both are north or south, but one east and the other west, add them together.

- 3. If one is north and the other south, but both east or west, subtract their sum from 180°.
- 4. If one is north and the other south, one east and the other west, subtract their difference from 180°.

 \mathbf{B}

Thus the angle CAB is equal to NAB-NAC.

The angle CAD is equal to NAC -NAD.

The angle DAF is equal to 180° -(NAD+SAF).

The angle CAF is equal to 180° –(SAF—NAC).

In the preceding example we accordingly find the angle

 $CDE=130^{\circ}$.

the angle
ABC=105°. DEA=101°.
BCD=100°. EAB=104°.

With these angles the field may be plotted without drawing parallels.

Example 2.

The following field notes are given to protract the survey:

Stations.	Bearings.	Distances.
1	N. 50° 30′ E.	16.50 chains.
2	S. 68° 15′ E.	14.20 "
3	S. 9° 45′ E.	8.45 "
4	S. 21° 0′ W.	6.84 "
5	S. 73° 30′ W.	12.31 "
6	N. 78° 15′ W.	9.76 "
7	N. 15° 30′ W.	11.55 "

THE TRAVERSE TABLE.

(155.) The accompanying traverse table shows the difference of latitude and the departure to four decimal places, for distances from 1 to 10, and for bearings from 0° to 90°, at intervals of 15′. If the bearing is less than 45°, the angle will be found on the left margin of one of the pages of the table, and the distance at the top or bottom of the page; the difference

of latitude will be found in the column headed Lat. at the top of the page, and the departure in the column headed Dep. If the bearing is more than 45° , the angle will be found on the right margin, and the difference of latitude will be found in the column marked Lat. at the bottom of the page, and the departure in the other column. The latitudes and departures for different distances with the same bearing are proportional to the distances. Therefore the distances may be reckoned as tens, hundreds, or thousands, if the place of the decimal point in each departure and difference of latitude be changed accordingly.

Ex. 1. To find the latitude and departure for the course 45° and the distance 93.

Under distance 9 on page 141, and opposite 45°, will be found latitude 6.3640 and departure 6.3640. Hence, for distance 90, the latitude is 63.640, and adding the latitude for the distance 3, viz., 2.121, we find the latitude for distance 93 to be 65.761.

Ex. 2. To find the latitude and departure for the course 60° and the distance 11.85.

The	latitud	le for	10	is	5.0000.	Departu	re :	for	10	is	8.6603.
66	"	"	1	is	.5000.			"	1	is	.8660.
					.4000.			"	.8	is	.6928.
"	"	"	.05	is	.0250.	"		"	.05	is	.0433.
Lat	titude :	for $\overline{11}$	L.85	is	5.9250.	Depart.	for	$\overline{11}$.85	is	10.2624.

Ex. 3. To find the latitude and departure for the course 20° and the distance 5.30.

Ans. Latitude 4.98, and departure 1.81.

The traverse table may be used not only for obtaining departure and difference of latitude, but for finding by inspection the sides and angles of any right-angled triangle; for the latitude and departure form the two legs of a right-angled triangle, of which the distance is the hypothenuse, and the course is one of the acute angles.

In this manner we find the latitude and departure for each side of the field given in Example 1, page 105, to be as in the following table:

		Dis-	Lati	tude.	Depa	rture.	Cor.	Cor.		Balar	nced.	
	Courses.	tances.	N.	s.	E.	W.	Lat.	Dep.	N.	S.	E.	W.
T	N. 45° E.	9.30	6.58		6.58			+.01	6.58		6.59	
2	S. 60° E.	11.85		5.92	10.26		+.01	-,01		5.93	10.27	
3	S. 20° W.	5.30		4.98		1.81		<u>-</u> .01		4.98		1.80
4	S. 70° W.	10.90		3.73		10.24		.01		3.73		10.23
5	N. 31° W.	9.40	.8.06			4.84		01	8.06			4.83
Γ	Perimeter	46.75	14.64	14.63	16.84	16.89			14.64	14.64	16.86	16.86

(156.) When a field has been correctly surveyed, and the latitudes and departures accurately calculated, the sum of the northings should be equal to the sum of the southings, and the sum of the eastings equal to the sum of the westings. If the northings do not agree with the southings, and the eastings with the westings, there must be an error either in the survey or in the calculation. In the preceding example, the northings exceed the southings by one link, and the westings exceed the eastings by five links. Small errors of this kind are unavoidable; but when the error does not exceed one link to a distance of three or four chains, it is customary to distribute the error among the sides by the following proportion:

As the perimeter of the field, Is to the length of one of the sides, So is the error in latitude or departure, To the correction corresponding to that side.

This correction, when applied to a column in which the sum of the numbers is too small, is to be *added*; but if the sum of the numbers is too great, it is to be *subtracted*.

We thus obtain the corrections in columns 8 and 9 of the preceding table; and applying these corrections, we obtain the balanced latitudes and departures, in which the sums of the northings and southings are equal, and also those of the eastings and westings.

As the computations are generally carried to but two decimal places, the corrections of the latitudes and departures are only required to the nearest link, and these corrections may often be found by mere inspection without stating a formal proportion. Thus, in the preceding example, since the departures require a correction of five links, and the field has five sides which are not very unequal, it is obvious that we must make a correction of one link on each side.

It is the opinion of some surveyors that when the error in latitude or departure exceeds one link for every five chains of the perimeter, the field should be resurveyed; but most surveyors do not attain to this degree of accuracy. however, should never exceed one link to a distance of two or three chains.

(157.) To find the area of the field.

Let ABCDE be the field to be measured. Through A, the most western station, draw the meridian NS, and upon it let fall the perpendiculars BF, CG, DH, EI.

Then the area of the required field is equal to FBCDEI-(ABF+AEI).

But FBCDEI is equal to the sum of the three trapezoids FBCG, GCDH, HDEI.

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Also, if the sum of the parallel sides FB, GC be multiplied by FG, it will give twice

the area of FBCG (Art. 87). The sum of the sides GC, DH, multiplied by GH, gives twice the area of GCDH; and the sum of HD, IE, multiplied by HI, gives twice the area of HDEI.

Now BF is the departure of the first side, GC is the sum of the departures of the first and second sides, HD is the algebraic sum of the three preceding departures, IE is the algebraic sum of the four preceding departures. Then the sum of the parallel sides of the trapezoids is obtained by adding together the preceding meridian distances two by two; and if these sums are multiplied by FG, GH, &c., which are the corresponding latitudes, it will give the double areas of the trapezoids.

(158.) It is most convenient to reduce all these operations to a tabular form, according to the following

RULE.

Having arranged the balanced latitudes and departures in

their appropriate columns, draw a meridian through the most eastern or western station of the survey, and, calling this the first station, form a column of double meridian distances.

The double meridian distance of the first side is equal to its departure; and the double meridian distance of any side is equal to the double meridian distance of the preceding side, plus its departure, plus the departure of the side itself.

Multiply each double meridian distance by its corresponding northing or southing, and place the product in the column of north or south areas. The difference between the sum of the north areas and the sum of the south areas will be double the area of the field.

It must be borne in mind that by the term *plus* in this rule is to be understood the algebraic sum. Hence, when the double meridian distance and the departure are both east or both west, they must be added together; but if one be east and the other west, the one must be subtracted from the other.

The double meridian distance of the last side should always be equal to the departure for that side. This coincidence affords a check against any mistake in forming the column of double meridian distances.

The preceding example will then be completed as follows:

	N.	s.	E.	W.	D.M.D.	N. Areas.	S. Areas.
1	6.58		6.59		6.59	43.3622	
2		5.93	10.27		23.45		139.0585
3		4.98		1.80	31.92		158.9616
4		3.73		10.23	19.89		74.1897
5	8.06			4.83	4.83	38.9298	
						82.2920	372.2098

Twice the figure FBCDEI is 372.2098 square chains.

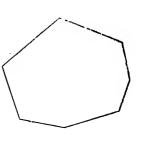
Twice the figure FBAEI is 82.2920 '

The difference is 289.9178 "

Therefore the area of the field is 144.9589 square chains, or 14.49589 acres, which is equal to 14 acres, 1 rood, 39 perches.

Ex. 2. It is required to find the contents of a tract of land of which the following are the field notes:

Sta- tions.		Bear	ings.		Dist	ances.
1	N.	50°	30′	E.	16.50	chains.
2	S.	68°	15'	E.	14.20	"
3	S.	9°	45'	E.	8.45	4
4	S.	21°	0'	W.	6.84	"
5	S.	73°	30'	W.	12.31	"
6	N.	78°	15'	W.	9.76	66
7	N.	17°	0′	W.	11.64	"



Calculation.

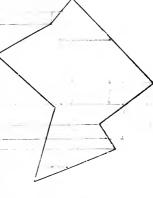
П		n: .	Dif.	Lat.	Depa		_		Bala	nced.		D.M.		
_	Courses.	Dist.	N.	S.	E.	w.	Cor.	N.	S.	E.	w.	D.	N. Areas.	S. Areas.
		16.50	10.50		12.73		.03	10.47		12.70			132.9690	
		14.20			13.19		.03		5.29	13.16		38.56		203,9824
	S. 9º 45' E.	8.45			1.43		.01		8.34			53.14		443.1876
	S. 210 0' W.			6.39		2.45			6.40			52.10		333.4400
	S. 73° 30′ W.			3.50		11.80			3.52			37.82		133.1264
	N. 78° 15′ W.				1	9.56						16.42		
3	N. 170 OW.	11.64	11.13			3.40	.02	11.11			3.42	3.42	37.9962	
		79.70	23.62	23.48	27.35	27.21		23.55	23.55	27.28	27.28		203.3126	1113.7364
			Erro	r.14	Erro	r .14								203.3126

2)910.4238

Ans., 45 A., 2 R., 3 P. . . 455.2119

Ex. 3. Required the area of a tract of land of which the following are the field notes:

Sta- tions.	Bearings.	Distances.
1	N. 58° 45′ E.	19.84 chains.
2	N. 39° 30′ E.	10.45 "
3	S. 45° 15′ E.	37.26 "
4	S. 52° 30 W.	21 .53 "
5	S. 34° 0′ E.	9.12 "
6	S. 66° 15′ W.	27.69 "
7	N. 12° 45′ E.	24.31 "
8	N. 48° 15′ W.	24.60 "



Ans., 130 A., 2 R., 23 P.

Ex. 4. Required the area of a piece of land from the following field notes:

Stations.	Bearings.	Distances.
1	N. 5° 15′ E.	15.17 chains.
2	N. 45° 45′ E.	16.83 "
$\overline{)}$ 3	N. 32° 0′ W.	14.26 "
4	N. 88° 30′ E.	19.54 "
5	S. 28° 15′ E.	17.92 "
6	S. 40° 45′ W.	9.71 "
7	S. 31° 30′ E.	22.65 "
8	S. 14° 0′ W.	18.39 "
9	S. 82° 45′ W.	24.80 "
10	N. 23° 15′ W.	26.31 "

Ans., 173 A., 0 R., 23 P.

Ex 5. Required the area of a field from the following notes

_		· · · · · · · · · · · · · · · · · · ·
Stations.	Bearings.	Distances.
1	N. 32° 15′ E.	28.74 chains.
2	N. 17° 45′ E.	21.59 "
3	S. 81° 30′ E.	13.38 "
4	S. 9° 45′ W.	11.92 "
5	S. 43° 0′ E.	19.65 "
6	N. 25° 30′ E.	17.26 "
7	S. 78° 15′ E.	18.87 "
8	S. 5° 45′ W.	31.41 "
9	S. 37° 30′ W.	26.13 "
10	N. 69° 0′ W.	23.86 "
11	S. 74° 15′ W.	20.91 "
12	N. 27° 30′ W.	23.20 "

Ans., 304 A., 2 R., 9 P.

Ex. 6. Required the area of a field from the following not so:

Stations.	Bearings.	Distances.
1	N. 36° 15′ E.	24.73 chains.
2	N. 7° 45′ E.	11.58 "
3	N. 79° 30′ E.	15.39 "
4	S. 86° 45′ E.	20.56 "
5	S. 12° 15′ W.	18.14 "
6	S. 25° 0′ E.	21.92 "
7	S. 58° 30′ W.	29.27 "
8	N. 34° 0′ W.	19.81 "
9	N. 81° 15′ W.	21.24 "

Ans., 179 A., 1 R., 6 P

(159) The field notes from which the area is to be computed may be imperfect. There may be obstacles which prevent the measuring of one side, or the notes may be defaced so as to render some of the numbers illegible. If the bearings and lengths of all the sides of a field except one are given, the remaining side may easily be found by calculation. For the difference between the sum of the northings and the sum of the southings of the given sides will be the northing or southing of the remaining side; and the difference between the sum of the eastings and the sum of the westings of the given sides will be the easting or westing of the remaining side. Having, then, the difference of latitude and departure of the required side, its length and direction are easily found by Trigonometry (Art. 47).

Ex. Given the bearings and lengths of the sides of a tract of land as follows:

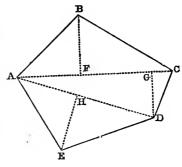
Stations.	Bearings.	Distances.
1	N. 18° 15′ E.	8.93 chains.
2	N. 79° 45′ E.	15.64 "
3	S. 25° 0′ E.	14.27 "
4	Unknown.	Unknown.
5	N. 87° 30′ W.	18.52 chains.
6	N. 41° 15′ W.	12.18 "

Required the bearing and distance of the fourth side.

Ans., S. 15° 33′ E., distance 8.62 chains.

(160.) There is another method of finding the area of a field which may be practiced when great accuracy is not required It consists in first drawing a plan of the field, as in Art. 153

then dividing the field into triangles by diagonal lines, and measuring the bases and perpendiculars of the triangles upon the same scale of equal parts by which the plot was drawn. Thus, if we take Ex. 1, and draw the diagonals AC, AD, the field will be divided into three triangles, whose area easily found when we know



the diagonals AC, AD, and the perpendiculars BF, DG, EH. The diagonal AC is found by measurement upon the scale of equal parts to be 16.87; the diagonal AD is 15.67; the perpendicular BF is 6.30; DG is 4.92; and EH is 6.42. Hence

the triangle ABC= $16.87 \times 3.15 = 53.14$ " " ADC= $16.87 \times 2.46 = 41.50$ " " ADE= $15.67 \times 3.21 = 50.30$

the figure ABCDE == 144.94 sq. chains.

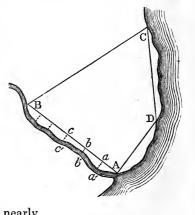
This method of finding the area of a field is very expeditious, and when the plot is carefully drawn, may afford results sufficiently precise for many purposes.

(161.) To survey an irregular boundary by means of offsets.

When the boundaries of a field are very irregular, like a river or lake shore, it is generally best to run a straight line, coming as near as is convenient to the true boundary, and measure the perpendicular distances of the prominent points of the boundary from this line.

Let ABCD be a piece of land to be surveyed; the land being bounded on the east by a lake, and on the west by a creek

We select stations A, B, C, D, so as to form a polygon which shall embrace most of the proposed field, and find its area. We then measure perpendiculars aa', bb', cc', &c., as also the distances Aa, ab, bc, &c. Then, considering the spaces Aaa', abb'a', &c., as triangles or trapezoids, their area may be computed; and, adding these areas to the figure ABCD, we shall obtain the area of the proposed field nearly.



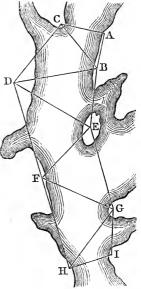
(162.) To determine the bearing and distance from one point to another by means of a series of triangles.

When it is required to find the distance between two points remote from each other, we form a series of triangles such that

the first and second triangles may have one side in common; the second and third, also, one side in common; the third and fourth, &c. We then measure one side of the first triangle for a base line, and all the angles in each of the triangles. These data are sufficient to determine the length of the sides of each triangle; for in the first triangle we have one side and the angles to find the other sides. When these are found, we shall have one side and all the angles of a second triangle to find the other sides. In the same manner we may calculate the dimensions of the third triangle, the fourth, and so on. We shall illustrate this method by an example taken from the Coast Survey of the United States.

The object here is to make a survey of Chesapeake Bay and

its vicinity; to determine with the utmost precision the position of the most prominent points of the country, to which subordinate points may be referred, and thus a perfect map of the country be obtained. Accordingly, a level spot of ground was selected on the eastern side of the bay, on Kent Island, where a base line, AB, of more than five miles in length, was measured with every precaution. A station, C, was also selected upon the other side of the bay, near Annapolis, so situated that it was visible from A and B. The three angles of the triangle ABC were then measured with a large theodolite, after which the length of BC may be com-



puted. A fourth station, D, is now taken on the western shore of the bay, visible from C and B, and all the angles of the triangle BCD are measured, when the line BD can be computed. A fifth station, E, is now taken on an island near the eastern shore, visible both from B and D, and all the angles of the triangle BDE are measured, when DE can be computed. Also, all the angles of the triangle DEF are measured, and EF is computed. Then all the angles of the triangle EFG are measured.

ured, and FG is computed. So, also, all the angles of the triangle FGH are measured, and GH is computed; and thus a chain of triangles may be extended along the entire coast of the United States. To test the accuracy of the work, it is common to measure a side in one of the triangles remote from the first base, and compare its measured length with that deduced by computation from the entire series of triangles. This line is called a base of verification. Such a base has been measured on Long Island; and, indeed, several bases have been measured on different points of the coast. These are all connected by a triangulation, and thus the length of a side in any triangle may be deduced from more than one base line, and the agreement of these results is a test of the accuracy of Thus the length of one of the sides of a trithe entire work. angle which was twelve miles, as deduced from the Kent Island base, differed only twenty inches from that derived from the Long Island base, distant two hundred miles.

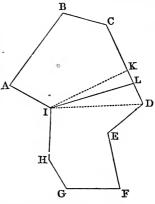
The superiority of this method of surveying arises from the circumstance that it is necessary to measure but a small number of base lines along a coast of a thousand or more miles in extent; and for these the most favorable ground may be selected any where in the vicinity of the system of triangles. All the other quantities measured are angles; and the precision of these measurements is not at all impaired by the inequalities of the surface of the ground. Indeed, mountainous countries afford peculiar facilities for a trigonometrical survey, since they present heights of ground visible to a great distance, and thus permit the formation of triangles of very large dimensions.

(163.) To divide an irregular piece of land into any two given parts.

We first run a line, by estimation, as near as may be to the required division line, and compute the area thus cut off. It this is found too large or too small, we add or subtract a triangle, or some other figure, as the case may require. Suppose it is required to divide the field ABCDEFGHI into two equal parts, by a line IL, running from the corner I to the opposite side CD. We first draw a line from I to D, and compute the area of the part DEFGHI; and, knowing the area

of the entire field, we learn the area which must be contained

in the triangle DIL, in order that IL may divide the field into two equal parts. Having the bearings and distances of the sides DE, EF, &c., we can compute the bearing and distance of DI. Thus the angle IDK is known; and, having the hypothenuse ID, we can compute the length of the perpendicular IK let fall on CD. Now the base of a triangle must be equal to its area divided by half the altitude. Hence, if we divide the



area of the triangle DIL by half of IK, it will give DL.

In a similar manner we might proceed if it was required to divide a tract of land into any two given parts.

Variation of the Needle.

(164.) The line indicated by a magnetic needle, when freely supported and allowed to come to a state of rest, is called the *magnetic meridian*. This does not generally coincide with the *astronomical meridian*, which is a true north and south line.

The angle which the magnetic meridian makes with the true meridian is called the *variation of the needle*, and is said to be east or west, according as the north end of the needle points east or west of the north pole of the earth.

The variation of the needle is different in different parts of the earth. In some parts of the United States it is 10° west, and in others 10° east, while at other places the variation has every intermediate value. Even at the same place, the variation does not remain constant for any length of time. Hence it is necessary frequently to determine the amount of the variation, which is easily done when we know the position of the true meridian. The latter can only be determined by astronomical observations. The best method is by observations of the pole star. If this star were exactly at the pole, it would always be on the meridian; but, being at a distance of about

a degree and a half from the pole, it revolves about the pole in a small circle in a little less than 24 hours. In about six hours from its passing the meridian above the pole, it attains its greatest distance west of the meridian; in about six hours more it is on the meridian beneath the pole; and in about six hours more it attains its greatest distance east of the meridian. If the star can be observed at the instant when it is on the meridian, either above or below the pole, a true north and south line may be obtained.

(165.) The following table shows the time of the pole star's passing the meridian above the pole for every fifth day of the year:

January 6 20 P.M. 6 0 P.M. 5 41 P.M. 5 52 P.M. February 4 18 " 3 58 " 3 39 " 3 19 " March 2 28 " 2 8 " 1 49 " 1 29 "	5 1 P.M. 3 0 "	h. m. 4 42 P.M.
June 8 26 8 7 7 47 7 27 1 July 6 28 6 9 5 49 5 29 4 August 4 27 4 7 3 47 3 27 3 27 September 2 25 2 5 1 45 1 26 1 26 October 0 26 0 7 1 1 43 P.M. 11 24 P.M. 11 1 24 P.M. 1	1 9 " 1 8 A.M. 9 9 " 7 8 " 5 10 " 3 8 " 1 6 " 1 4 P.M.	2 40 " 0 50 " 10 48 A.M. 8 50 " 6 48 " 4 50 " 2 48 " 0 46 " 10 44 P.M. 8 42 " 6 44 "

If the pole star passes the meridian in the daytime, it can not be observed without a good telescope; but 11th 58th after the dates in the above table, the star will be on the meridian below the pole, and during the whole year, except in summer, the pole star may be seen with the naked eye on the meridian either above or below the pole. These observations are best made with a theodolite, but they may be made with a common compass. At 5th 59th after the dates in the above table, the star will have attained its greatest distance west of the meridian; and 5th 59th before these dates, it will be at its greatest distance east of the meridian. In summer, therefore. we may observe the greatest eastern elongation of the pole star, at which time the star is 1° 55' east of the true meridian for all places in the neighborhood of New York. Making this allowance, a true meridian is easily obtained; after which, the variation of the needle is determined by placing a compass upon this line, turning the sights in the same direction, and noting the angle shown by the needle.

The following table shows the angle which the plane of the

meridian makes with a vertical plane passing through the pole star, when at its greatest eastern or western elongation, for any latitude from 30° to 44°.

```
Lat. 30° | Lat. 32° | Lat. 34° | Lat. 36° | Lat. 38° | Lat. 40° | Lat. 42° | Lat. 44° | 1° 41′ | 1° 43′ | 1° 45′ | 1° 48′ | 1° 51′ | 1° 54′ | 1° 58′ | 2° 2′
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(166.) The variation of the needle, in 1840, for several parts of the United States, was as follows:

```
Burlington, Vt. . . 9° 27′ W. Buffalo, N. Y. . . 1° 37′ W. Boston, Mass. . . 9° 12′ W. Cleveland, Ohio . 0° 19′ E. Albany, N. Y. . . 6° 58′ W. Detroit, Mich. . . 1° 56′ E. New Haven, Ct. . 6° 13′ W. Charleston, S. C. . 2° 44′ E. New York City . 5° 34′ W. Cincinnati, Ohio . 4° 46′ E. Philadelphia . . . 4° 8′ W. Mobile, Ala. . . . 7° 5′ E. Washington City . 1° 20′ W. St. Louis, Mo. . . 8° 37′ E.
```

Since 1840, the variation in New England has increased about five minutes annually; in New York and Pennsylvania it has increased from three to four minutes annually. In the Western States it decreases at about the same rate, and in the Southern States it decreases about two minutes annually.

LEVELING.

(167.) Leveling is the art of determining the difference of level between two or more places.

The surface of an expanse of tranquil water, or any surface parallel to it, is called a *level surface*. Points situated in a level surface are said to be on the *same level*, and a line traced on such a surface is called a *line of true level*.

On account of the globular figure of the earth, a level surface is not a plane surface. It is nearly spherical; and in the common operations of leveling it is regarded as perfectly so. Hence every point of a level surface is regarded as at the same distance from the center of the earth; and the difference of level of two places is the difference between their distances from the center.

A line of apparent level is a straight line tangent to the surface of the earth.

Thus, if AB represent the surface of the ocean, the two places A and B are said to be on the same level; but if AD

be drawn tangent to the arc AB at A, then AD is a line of apparent level.

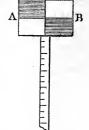
This is the line which is indicated by a leveling instrument placed at A. The theodolite may be employed for tracing horizontal lines; but if nothing further were required, there would be no occasion for graduated circles, and several parts of the theodolite might



be dispensed with. A leveling instrument, therefore, usually consists of a large spirit level attached to a telescope, mounted upon a stand in a manner similar to the theodolite.

(168.) The surveyor should also be provided with a pair of

leveling staves. A leveling staff consists of a rectangular bar of wood six feet in length, divided to inches and sometimes tenths of an inch, and having a groove running its entire length. A smaller staff of the same length, called a *slide*, also divided into inches, is inserted in this groove, and moves freely along it.



At the upper end of the slide is a rectangular board called a vane, AB, about six inches

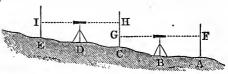
wide. The vane is divided into four equal parts by two lines, one horizontal and the other vertical. Two opposite parts of the vane are painted white, and the other two black, in order that they may be distinguished at a great distance.

To find the difference of level between any two points.

(169.) Set up the leveling staves perpendicular to the horizon, and at equal distances from the leveling instrument Having adjusted the level by means of the proper screws, turn the telescope to one of the staves, and direct an assistant to slide up the vane until the line AB coincides with the center of the telescope, and note the height of this line from the ground. Turn the telescope to the other staff, and repeat the same operation. Level in the same manner from the second station to the third, from the third to the fourth, &c. Then the difference between the sum of the heights at the back stations and at the forward stations will be equal to the difference of level between the first station and the last.

If we wish to level from A to E, we set up the staves at a

convenient distance, AC, and midway between them place the level B. Observe where the line of lev-



el, FG, cuts the rods, and note the heights AF, CG. Their difference is the difference of level between the first and second stations. Take up the level and place it at D, midway between the rods C and E, and observe where the line of level, HI, cuts the rods, and note the heights CH, EI.

Then FA-CG=the ascent from A to C, and CH-EI=the ascent from C to E.

Therefore (FA+CH)-(CG+EI)=the entire ascent from A to E; and in the same manner we may find the difference of level for any distance; that is, the difference between the sum of the heights at the back stations and at the forward stations is equal to the difference of level between the first station and the last.

(170.) The following is a copy of the field notes for running a level from A to E:

Back s	ights.	•		Fore	sights.
	Inches.				Inches.
0	4			3	2
5	10			5	7
4	2			4	3
5	6			1	2
4	11			3	2
4	7			1	3
6	1			2	0
Sum 31	5		Jan	$1\overline{20}$	7

The back sights being greater in amount than the forward sights, it is evident that E is higher than A by 10 feet 10 inches.

The heights indicated by the leveling staves are sometimes read off by the assistant, but it is better for the observer to read off the quantities himself through the telescope of his leveling instrument. This may easily be done provided the graduation of the staff is perfectly distinct; and in that case it

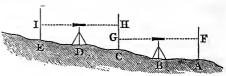
Hence

and

is only necessary to rely upon the assistant to hold the staff perpendicularly. To enable him to do this, a small plummet is suspended in a groove cut in the side of the staff.

(171.) It must be observed that the lines GF, HI are lines

of apparent level, and not of true level; nevertheless, we shall obtain the true difference of level between



A and E by this method if the leveling instrument is placed midway between the leveling staves, because the points G and F will in that case be at equal distances from the earth's center. If the level is not placed midway between the staves, then we must apply a correction for the difference between the true and apparent level.

(172.) To find the difference between the true and apparent level.

Let C be the center of the earth, AB a portion of its surface.

and AD a tangent to the earth's surface at A; then BD is the difference between the true and apparent level for the distance AD.

Now, by Geom., Prop. 11, B. IV.,

$$CD^{2}=AC^{2}+AD^{2}.$$

$$CD = \sqrt{AC^{2}+AD^{2}},$$

$$BD = \sqrt{AC^{2}+AD^{2}}-BC.$$

If we put R=BC, the radius of the earth, d=AD,

and h=BD, the difference between the true and apparent level, we shall have

$$h = \sqrt{\mathbf{R}^2 + d^2} - \mathbf{R}$$
;

that is, to find the difference between the true and apparent level for any distance, add the square of the distance to the square of the earth's radius, extract the square root of the sum, and subtract the radius of the earth.

If BD represent a mountain, or other elevated object, then AD will represent the distance at which it can be seen in consequence of the curvature of the earth.

- Ex. 1. If the diameter of the earth be 7912 miles, and if Mount Ætna can be seen at sea 126 miles, what is its height?

 Ans., 2 miles.
- Ex. 2. If a straight line from the summit of Chimborazo touch the surface of the ocean at the distance of 179 miles, what is the height of the mountain?

 Ans., 4.05 miles.

From the preceding formula we obtain

$$R^{2}+d^{3}=(R+h)^{2}$$

= $R^{2}+2Rh+h^{2}$,
 $d^{2}=2Rh+h^{2}$.

that is,

But in the common operations of leveling, h is very small in comparison with the radius of the earth, and h^2 is very small in comparison with 2Rh. If we neglect the term h^2 , we have

$$d^{2}=2Rh;$$
 $h=\frac{d^{2}}{2R};$

whence

that is, the difference between the true and apparent level is nearly equal to the square of the distance divided by the diameter of the earth.

Ex. 1. What is the difference between the true and apparent level for one mile, supposing the diameter of the earth to be 7912 miles?

Ans., 8.008 inches, or 8 inches nearly.

Ex. 2. What is the difference between the true and apparent level for half a mile?

Ans., 2 inches.

In the equation $h=\frac{d^2}{2R}$, since 2R is a constant quantity, h varies as d^2 ; that is, the difference between the true and apparent level varies as the square of the distance.

Hence, the difference for 1 mile being 8 inches, $_{\text{Ft. In}}$ the difference for 2 miles is $8 \times 2^2 = 32$ inches = 2 8.

"
$$6$$
 " $8 \times 6^2 = 288$ " $= 24$ 0, &c.

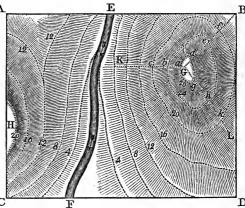
Topographical Maps.

(173.) It is sometimes required to determine and represent upon a map the undulations and inequalities in the surface of

a tract of land. Such a map should give a complete view of the ground, so as to afford the means for an appropriate location of buildings or extensive works. For this purpose, we suppose the surface of the ground to be intersected by a num ber of horizontal planes, at equal distances from each other The lines in which these planes meet the surface of the ground, being transferred to paper, will indicate the variations in the inclination of the ground; for it is obvious that the curves will be nearer together or further apart, according as the ascent is steep or gentle.

Thus, let ABCD be a tract of broken ground, divided by a stream, EF, the ascent being rapid on each bank, the ground

swelling to a hill A at G, and also at H. It is required to represent these inequalities upon paper, so as to give an exact idea of the face of the ground. The lowest point of the ground is at F. Suppose the tract to be intersected C



by a horizontal plane four feet above F, and let this plane intersect the surface of the ground in the undulating lines marked 4, one on each side of the stream. Suppose a second horizontal plane to be drawn eight feet above F, and let it intersect the surface of the ground in the lines marked 8. Let other horizontal planes be drawn at a distance of 12, 16, 20, 24, &c., feet above the point F. The projection of these lines of level upon paper shows at a glance the outline of the tract. We perceive that on the right bank of the stream the ground rises more rapidly on the upper than on the lower portion of the map, as is shown by the lines of level being nearer to one another. On the right bank of the stream the ascent is unin terrupted until we reach G, which is the summit of the hill. Beyond G the ground descends again toward B. On the left

pank of the stream the ground rises to H; but toward A the level line of 12 feet divides into two branches, and between them the ground is nearly level.

(174.) The surveys requisite for the construction of such a map may be made with a theodolite or common level.

The object is to trace a series of level lines upon the surface of the ground. For this purpose we may select any point on the surface of a hill, place the level there, and run a level line around the hill, measuring the distances, and also the angles, at every change of direction. We may then select a second point at any convenient distance above or below the former, and trace a second level line around the hill, and so on for as many curves as may be thought necessary. Such a method, however, would not always be most convenient in practice.

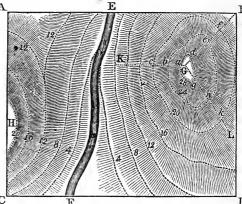
(175.) The following method may sometimes be preferable: Set up the level on the summit of the hill at G, and fix the vane on the leveling staff at an elevation of four feet in addition to the height of the telescope above the ground. Then direct an assistant to carry the leveling staff, holding it in a vertical position, toward K, till he arrives at a point, as a, where the vane appears to coincide with the cross wires of the telescope. This will determine one point of the curve line four feet below G. The assistant may then proceed to the line GB, and afterward to GL, moving backward or forward in each of those directions till he finds points, as d and g, at which the vane coincides with the cross wires of the telescope. The horizontal distance between G and a, G and d, G and g, must then be measured.

If the leveling staff is sufficiently long, the vane may be fixed on it at the height of eight feet, in addition to the height of the telescope at G; and the assistant, placing himself in the directions GK, GB, GL, must move till the vane appears to coincide with the cross wires as before. The horizontal distances ab, de, gh, must then be measured, and stakes driven into the ground at b, e, and h.

The level must now be removed to b; and the vane being fixed on the staff at a height equal to four feet, together with the height of the instrument from the ground at b, the assistant must proceed in the direction bK, and stop at c where

the vane coincides with the cross wires; then the horizontal

distance of c from A b must be measured. In a like manner, the operations may be continued from b or c as far as necessary toward K; then, commencing at e, and afterward at h, they may be continued in the same C



way toward B and L respectively. The angles which the directions GK, GB, GL make with the magnetic meridian being found with the compass, these directions may be represented on paper. Then the measured distances Ga, ab, &c.; Gd, de, &c.; Gg, gh, &c., being set off on those lines of direction, curves drawn through a, d, g; b, e, h; c, f, k, &c., will show the contour of the hill.

The map is shaded so as to indicate the hills and slopes by drawing fine lines, as in the figure, perpendicular to the horizontal curves.

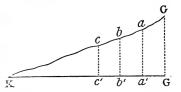
(176.) Another method, which may often be more convenient than either of the preceding, is as follows: From the summit of the hill measure any line, as GK, and at convenient points of this line let stakes be driven, and their distances from G be carefully measured. Then determine the difference of level of all these points; and if the assumed points do not fall upon the horizontal curves which are required to be delineated, we may, by supposing the slope to be uniform from one stake to another, compute by a proportion the points where the horizontal curves for intervals of four feet intersect the line GK. The same may be done for the lines GB and GL, and for other lines, if they should be thought necessary.

(177.) If the surface of the ground is gently undulating, it may be more convenient to run across the tract a number of lines parallel to one another. Drive stakes at each extremity

of these lines, and also at all the points along them where there is any material change in the inclination of the ground, and find the difference of level between all these stakes, and their distances from each other. Then, if we wish to draw upon a map the level lines at intervals of 4, 6, or 10 feet, we may compute in the manner already explained the points where the horizontal curves intersect each of the parallel lines. The curve lines are then to be drawn through these points, according to the judgment of the surveyor.

(178.) If it is required to draw a profile of the ground, $i \sim$

example, from G to K, draw a straight line, G'K, to represent a horizontal line to which the heights are referred, and set off G'a', G'b', G'c', &c., equal to the distances of the stations from the heginning of the line.



from the beginning of the line. At the points G', a', b', &c., erect perpendiculars, G'G, a'a, &c., and make them equal to the heights of the respective stations. Through the tops of these perpendiculars draw the curved line GK, and it will be the profile of the hill in the direction of the line GK.

On setting out Rail-way Curves.

(179.) It is of course desirable that the line of a rail-way should be perfectly straight and horizontal. This, however, is seldom possible for any great distance; and when it becomes necessary to change the direction of the line, it should be done gradually by a curve. The curve almost universally employed for this purpose is the arc of a circle, and such an arc may be traced upon the ground by either of the following methods.

First Method.—When the center of the circle can be seen from every part of the curve.

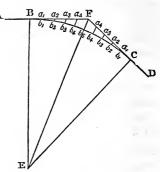
Let AB, CD be two straight portions of a road which it is desired to connect by an arc of a circle. Set up a theodolite at B and another at C, and from each point range a line at right angles to the lines AB and CD respectively; and at the intersection of these lines, E, which will be the center of the circle, erect a signal which can be seen from any point between B and C. Produce the lines AB and CD until they meet in F. and

on these lines drive stakes at equal distances, a_1 , a_2 , a_3 , com-

mencing from the points B and If r represents the radius of the circle, and d the distance between the points a_1, a_2, a_3 &c., then (Art. 172),

$$\sqrt{r^2+d^2}-r$$

will be the distance which must be set off from the first point a_1 , in the direction a_1 E, to obtain a point of the circular arc. In like manner,



$$\sqrt{r^2+(2d)^2}-r$$

will be the distance to be set off from the point a_2 , in the direction $a_2 E$; and, generally,

$$\sqrt{r^2+(nd)^2}-r$$

will be the distance to be set off at the nth points from B and C. For example, let r be one mile, or 5280 feet, and d equal to 100 feet; then,

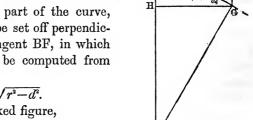
$$\sqrt{5280^2+100^2}-5280=.94$$
 feet,

will be the distance a_1b_1 . In a similar manner, we find at

 a_2 , or 200 feet from B, the offset will be 3.79 feet

$$a_3$$
, or 300 " " 8.52 " a_4 , or 400 " " 15.13 " a_5 , or 500 " " 23.62 "

(180.) Second Method. - When the center of the circle can not be seen from every part of the curve, the offsets may be set off perpendicularly to the tangent BF, in which case they must be computed from the formula



$$r-\sqrt{r^2-d^2}$$
.

For, in the annexed figure,

$$EH = \sqrt{GE^2 - GH^2};$$

that is, EH = $\sqrt{r^2-d^2}$.

And
$$a_s G = BH = BE - HE = r - \sqrt{r^2 - d^2}$$
.

If r=5280 feet, we shall find the offsets at intervals of 100 feet to be $a_1b_1 = .95$ feet.

 $a_1b_1 = .95 \text{ feet.}$ $a_2b_2 = 3.79 \text{ } ...$ $a_3b_3 = 8.53 \text{ } ...$ $a_4b_4 = 15.17 \text{ } ...$ $a_5b_5 = 23.73 \text{ } ...$

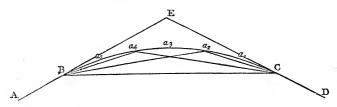
For small distances, the offsets will be given with sufficient accuracy by the formula

 $\frac{d^2}{2r}$

see Art. 172.

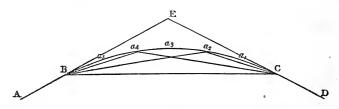
It is very common for surveyors, after they have found the first point, b_1 , of the curve, to join the points B, b_1 , and produce the line Bb_1 to the distance d, and from the end of this line set off an offset to determine the point b_2 ; then, producing the line b_1b_2 , set off a third offset to determine the point b_3 , and so on. The objection to this method is, that any error committed in setting out one of the points of the curve will occasion an error in every succeeding one. Whenever this method, therefore, is employed, it should be checked by determining the position of every fourth or fifth point by independent computation and measurement.

(181.) Third Method.—Where the radius of the curve is small, place a theodolite at B, and point its telescope toward



C Place another theodolite at C, and point its telescope toward E, the point of intersection of the lines AB, CD produced. Then, if the former be moved through any number of degrees toward a_1 , and the latter the same number of degrees toward a_1 , the point a_1 will be a point of the curve, for the angle Ba_1C will be equal to BCD (Geom., Prop. 16, B. III.). In the same manner, a_2 , a_3 , &c., any number of points of the curve, may be determined. It will be most convenient to move the

theodolites each time through an even number of degrees, for example, an arc of two degrees, and a stake must be driven at each of the points of intersection a_1 , a_2 , a_3 , &c. The accuracy of this method is independent of any undulations in the surface of the ground, so that in a hilly country this method may be preferable to any other.



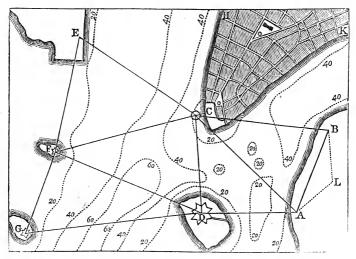
When the position of one end of the curve is not absolutely determined, the engineer may proceed more rapidly. Suppose it is required to trace an arc of a circle having a curvature of two degrees for a hundred feet.

Place a theodolite at C, the point where the curve commences, and lay off from the line CE, toward B, an angle of two degrees, and in the direction of the axis of the instrument set off a distance of 100 feet, which will give the first point a, of Next lay off from CE an angle of four degrees, and from a, set off a distance of 100 feet, and the point where this line cuts the axis of the instrument produced will be the second point a_3 . In the same manner, lay off from CE an angle of six degrees, and from a_2 set off a distance of 100 feet, and the point where it cuts the axis of the instrument produced will be the third point a_3 . All the points a_1 , a_2 , a_3 , etc., thus determined lie in the circumference of a circle (Geom., Prop. 15, B. III.). Circles thus drawn are generally made with a curvature of one or two degrees, or some convenient fraction of a degree, for every hundred feet. This method is very ex tensively practiced in the United States.

Surveying Harbors.

(182.) In surveying a harbor, it is necessary to determine the position of the most conspicuous objects, to trace the outline of the shore, and discover the depth of water in the neighborhood of the channel. A smooth, level piece of ground is chosen, on which a base line of considerable length is measured, and station staves are fixed at its extremities. We also erect station staves on all the prominent points to be surveyed, forming a series of triangles covering the entire surface of the harbor. The angles of these triangles are now measured with a theodolite, and their sides computed. After the principal p ints have been determined, subordinate points may be ascert ined by the compass or plane table.

Let the following figure be a map of a harbor to be survey-



ed. We select the most favorable position for a base line, which is found to be on the right of the harbor, from A to B. We also erect station flags at the points C, D, E, F, and G. Having earefully measured the base line AB, we measure the three angles of the triangle ABC, which enables us to compute the remaining sides. We then measure the three angles of the triangle ACD, and by means of the side AC, just computed, we are enabled to compute AD and CD. We then measure the three angles of the triangle CDF, and by means of the side CD, just found, we are enabled to compute CF and DF. Proceeding in the same manner with the triangles CEF, DFG, we are enabled, after measuring the angles, to compute the sides.

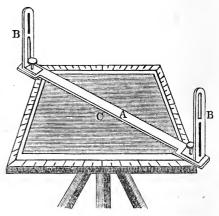
(183.) Having determined the main points of the harbor, we nay proceed to a more detailed survey by means of the chain

and compass. If it is required to trace the shore, HCK, we commence at H, and observe the bearings with the compass, and measure the distances with the chain. Where the shore is undulating, it is most convenient to run a straight line for a considerable distance, and at frequent intervals measure offsets to the shore.

When a great many objects are to be represented upon a map, the most convenient instrument is

The Plane Table.

(184.) The plane table is a board about sixteen inches square, designed to receive a sheet of drawing paper, and has two plates of brass upon opposite sides, confined by screws, for stretching and retaining the paper upon the board. The margin of the board is divided to 360 degrees from a center C, in the middle of the board, and these are



subdivided as minutely as the size of the table will admit. On one side of the board there is usually a diagonal scale of equal parts. A compass box is sometimes attached, which renders the plane table capable of answering the purpose of a surveyor's compass.

The ruler, A, is made of brass, as long as the diagonal of the table, and about two inches broad. A perpendicular sight-vane, B, B, is fixed to each extremity of the ruler, and the eye looking through one of them, the vertical thread in the other is made to bisect any required distant object.

To the under side of the table, a center is attached with a ball and socket, or parallel plate screws, like those of the theodolite, by which it can be placed upon a staff-head; and the table may be made horizontal by means of a detached spirit level

(185.) To prepare the table for use, it must be covered with arawing paper. Then set up the instrument at one of the stations, for example, B (see fig. on p. 131), and fix a needle in the table at the point on the paper representing that station, and place the edge of the ruler against the needle. rect the sights to the station A, and by the side of the ruler draw a line upon the paper to represent the direction of AB. Then, with a pair of dividers, take from the scale a certain number of equal parts to represent the base, and lay off this distance on the base line. Having drawn the base line, move the ruler around the needle, direct the sights to any object, as L, and keeping it there, draw a line along the edge of the ru-Then direct the sights in the same manner to any other objects which are required to be sketched, drawing lines in their respective directions, taking care that the table remains steady during the operation.

Now remove the instrument to the other extremity of the base A, and place the point of the paper corresponding to that extremity directly over it. Place the edge of the ruler on the base line, and turn the table about till the sights are directed to the station B. Then placing the edge of the ruler against the needle, direct the sights in succession to all the objects observed from the other station, drawing lines from the point A in their several directions. The intersections of these lines with those drawn from the point B will determine the positions of the several objects on the map.

In this manner the plane table may be employed for filling in the details of a map; setting it up at the most remarkable spots, and sketching by the eye what is not necessary should be more particularly determined, the paper will gradually become a representation of the country to be surveyed.

To determine the Depth of Water.

(186.) Let signals be established on the principal shoals and along the edges of the channel, by erecting poles or anchoring buoys, and let their bearings be observed from two stations of the survey. Then in each triangle there will be known one side and the angles, from which the other sides may be computed, and their positions thus become known. Then ascer

tain the precise depth of water at each of the buoys, and proceed in this manner to determine as many points as may be thought necessary.

If an observer is stationed with a theodolite at each extremity of the base line, we may dispense with the erection of permanent marks upon the water. One observer in a boat may make a sounding for the depth of water, giving a signal at the same instant to two observers at the extremities of the base line. The direction of the boat being observed at that instant from two stations, the precise place of the boat can be computed. In this way soundings may be made with great expedition.

There is also another method, still more expeditious, which may afford results sufficiently precise in some cases. Let a boat be rowed uniformly across the harbor from one station to another, for example, from D to G (see fig. on p. 131), and let a series of soundings be made as rapidly as possible, and the instant of each sounding be recorded. Then, knowing the entire length of the line DG, and the time of rowing over it, we may find by proportion the approximate position of the boat at each sounding.

If the soundings are made in tide waters, the times of high water should be observed, and the time of each sounding be recorded, so that the depth of water at high or low tide may be computed. In the maps of the United States Coast Survey, the soundings are all reduced to low-water mark, and the number of feet which the tide rises or falls is noted upon the map

(187.) The results of the soundings may be delineated upon a map in the same manner as the observations of level on page 124. We draw lines joining all those points where the depth of water is the same, for example, 20 feet. Such a line is seen to be an undulating line running in the direction from E to G. We draw another line connecting all those points where the depth of water is 40 feet. This line runs somewhat to the east of the former line, but nearly parallel with it. We draw other lines for depths of 60 feet, &c. The lines being thus drawn, a mere glance at the map will show nearly the depth of water at any point of the harbor.

BOOK V.

NAVIGATION.

(138.) NAVIGATION is the art of conducting a ship at sea from one port to another.

There are two methods of determining the situation of a vessel at sea. The one consists in finding by astronomical observations her latitude and longitude; the other consists in measuring the ship's course, and her progress every day from the time of her leaving port, from which her place may be computed by trigonometry. The latter method is the one to be now considered.

(189.) The figure of the earth is nearly that of a sphere, and in navigation it is considered perfectly spherical. The earth's axis is the diameter around which it revolves once a day. The extremities of this axis are the terrestrial poles; one is called the north pole, and the other the south pole.

The equator is a great circle perpendicular to the earth's axis.

Meridians are great circles passing through the poles of the earth. Every place on the earth's surface has its own meridian.

(190.) The longitude of any place is the arc of the equator intercepted between the meridian of that place and some assumed meridian to which all others are referred. In most countries of Europe, that has been taken as the standard meridian which passes through their principal observatory. The English reckon longitude from the Observatory of Greenwich; and in the United States, we have usually adhered to the English custom, though we believe the time has come when longitude should be reckoned from the Observatory of Washington.

Longitude is usually reckoned east and west of the first meridian, from 0° to 180°.

The difference of longitude of two places is the arc of the equator included between their meridians. It is equal to the

difference of their longitudes if they are on the same side of the first meridian, and to the sum of their longitudes if on opposite sides.

(191.) The *latitude* of a place is the arc of the meridian passing through the place, which is comprehended between that place and the equator.

Latitude is reckoned north and south of the equator, from 0° to 90°.

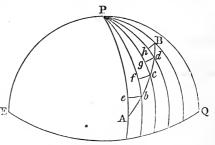
Parallels of latitude are the circumferences of small circles parallel to the equator.

The difference of latitude of two places is the arc of a meridian included between the parallels of latitude passing through those places. It is equal to the difference of their latitudes if they are on the same side of the equator, and to the sum of their latitudes if on opposite sides.

The *distance* is the length of the line which a vessel describes in a given time.

The departure of two places is the distance of either place from the meridian of the other. If the two places are on the same parallel, the departure is the distance between the places. Otherwise, we divide the distance AB into portions

Ab, bc, cd, &c., so small that the curvature of the earth may be neglected. Through these points we draw the meridians Pb, Pc, &c., and the parallels be, cf, &c. Then the departure for Ab is eb, for bc it is fc; and



the whole departure from A to B is eb+fc+gd+hB; that is, the sum of the departures corresponding to the small portions into which the distance is divided.

Distance, departure, and difference of latitude are measured in nautical miles, one of which is the 60th part of a degree at the equator. A nautical mile is nearly one sixth greater than an English statute mile.

The course of a ship is the angle which the ship's path makes with the meridian. A ship is said to continue on the same

course when she cuts every meridian which she crosses at the same angle. The path thus described is not a straight line, but a curve called a *rhumb-line*.

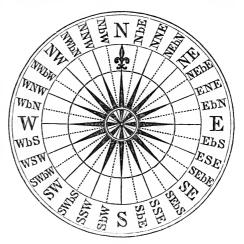
The course of a ship is given by the mariner's compass.

(192.) The mariner's compass consists of a circular piece of paper, called a card, attached to a magnetic needle, which is balanced on a pin so as to move freely in any direction. Directly over the needle, a line is drawn on the card, one end of which is marked N, and the other S. The circumference is divided into thirty-two equal parts called rhumbs or points, each point being subdivided into four equal parts called quarter points.

The points of the compass are designated as follows, begin-

ning at north and going east: north, north by east, north-northeast, northeast by north, northeast, and so on, as shown in the annexed figure.

The interval between two adjacent points is 11° 15′, which is the eighth part of a quadrant. On the inside of the compass-box a black line is drawn perpen-

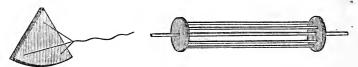


dicular to the horizon, and the compass should be so placed that a line drawn from this mark through the center of the card may be parallel to the keel of the ship. The part of the card which coincides with this mark will then show the point of the compass to which the keel is directed. The compass is suspended in its box in such a manner as to maintain a horizontal position, notwithstanding the motion of the ship.

The following table shows the number of degrees and minutes corresponding to each point of the compass:

North.					Pts.	South.			
N. by E.	N. by W.	1	11°	15'	1	S. by E.	S. by W.		
N.N.E.	N.N.W.	2	22°	30'	2	S.S.E.	S.S.W.		
N.E. by N.	N.W. by N.	3	33°	45'	3	S.E. by S.	S.W. by S.		
N.E.	N.W.	4	45°	0'	4	S.E.	s.w.		
N.E. by E.	N.W. by W.	5	56°	15^{\prime}	5	S.E. by E.	S.W. by W.		
E.N.E.	W.N.W.	6	67°	30′	6	E.S.E.	W.S.W.		
E. by N.	W. by N.	7	78°	45'	7	E. by S.	W. by S.		
East.	West.	8	90°	0′	8	East.	West.		

(193.) The ship's rate of sailing is measured by a *log-line*. The log-line is a cord about 300 yards long, which is wound



round a reel, one end being attached to a piece of thin board called a log. This board is in the form of a sector of a circle, the arc of which is loaded with lead sufficient to give the board a vertical position when thrown upon the water. This is designed to prevent the log from being drawn along after the vessel while the line is running off the reel.

The time is measured by a sand-glass, through which the sand passes in half a minute, or the 120th part of an hour.

The log-line is divided into equal parts called knots, each of which is 50 feet, or the 120th part of a nautical mile. Now, since a knot has the same ratio to a nautical mile that half a minute has to an hour, it follows, that if the motion of a ship is uniform, she sails as many miles in an hour

as she does knots in half a minute. If, then, seven knots are observed to run off in half a minute, the ship is sailing at the rate of seven miles an hour.

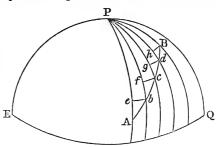
PLANE SAILING.

(194.) Plane sailing is the method of calculating a ship's place at sea by means of the properties of a plane triangle. The particulars which are given or required are four, viz., the

distance, course, difference of latitude, and departure. Of these, any two being given, the others may be found.

Let the figure EPQ represent a portion of the earth's sur-

face, P the pole, and EQ the equator. Let AB be a rhumb-line, or the track described by a ship in sailing from A to B on a uniform course. Let the whole distance be divided into portions Ab, bc, &c., so small



that the curvature of the earth may be neglected. Through the points of division draw the meridians Pb, Pc, &c., and the parallels eb, fc, &c. Then, since the course is every where the same, each of the angles eAb, fbc, &c., is equal to the course. The distances Ae, bf, &c., are the differences of latitude of A and b, b and c, &c. Also, eb, fc, &c., are the departures for the same distances. Hence the difference of latitude from A to B is equal to

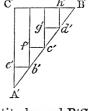
Ae+bf+cg+dh, and the departure is equal to eb+fc+gd+hB.

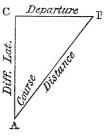
Construct the triangle A'B'C' so that A'b'e' shall be equal to Abe, b'c'f' shall be equal to bcf, c'd'g' equal to cdg, and d'B'h' equal to dBh. Then A'B' represents the distance sail-

ed, B'A'C' the course, A'C' the difference of latitude, and B'C the departure; that is, the distance, dif-

the departure; that is, the distance, difference of latitude, and departure are correctly represented by the hypothenuse and sides of a right-angled triangle, of which the angle opposite to the departure is the course. Of these four quantities, any two being given, the others may be found.

Plane sailing does not assume the earth's surface to be a plane, and does not involve any error even in great distances.





EXAMPLES.

1. A ship sails from Vera Cruz N.E. by N. 74 miles. Required her departure and difference of latitude

According to the principles of right-angled triangles, Art. 44.

Radius : distance :: sin. course : departure.

:: cos. course : diff. latituae

The course is three points, or 33° 45'; hence we obtain

Departure =41.11 miles.

Diff. latitude=61.53 miles.

2. A ship sails from Sandy Hook, latitude 40° 28′ N., upon a course E.S.E., till she makes a departure of 500 miles. What distance has she sailed, and at what latitude has she arrived?

By Trigonometry, Art. 44,

Sin. course : departure :: radius : distance,

:: cos. course : diff. latitude

Ans. Distance =541.20 miles.

Diff. latitude=207.11 miles, or 3° 27.

Hence the latitude at which she has arrived is 37° 1′ N.

3. The bearing of Sandy Hook from Bermuda is N. 42° 56′ W., and the difference of latitude 486 miles. Required the distance and departure.

By Trigonometry, Art. 46,

Radius: diff. latitude::tang. course: departure,

 $:: sec.\ course: distance.$

Ans. Distance =663.8 miles.

Departure=452.1 miles.

4. A ship sails from Bermuda, latitude 32° 22′ N., a distance of 666 miles, upon a course between north and east, until she finds her departure 444 miles. What course has she sailed, and what is her latitude?

By Trigonometry, Art. 44,

 $Distance: radius:: departure: sin.\ course,$

 $Radius: distance:: cos.\ course: diff.\ latitude.$

Ans. Latitude= 40° 38′ N.

Course = N. 41° 49′ E

5. The distance from Vera Cruz, latitude 19° 12′ N., to Pensacola, latitude 30° 19′ N., is 820 miles. Required the bearing and departure.

By Trigonometry, Art. 45,

Distance: radius:: diff. l'atitude: cos. course, Radius: distance:: sin. course: departure.

Ans. Bearing =N. 35° 34′ E.

Departure=476.95 miles

6. A ship sails from Sandy Hook upon a course between south and east to the parallel of 35°, when her departure was 300 miles. Required her course and distance.

By Trigonometry, Art. 47,

Diff. latitude: radius:: departure: tang. course, Radius: diff. latitude:: sec. course: distance.

Ans. Course S. 42° 27' E.

Distance 444.5 miles

TRAVERSE SAILING.

(195.) A traverse is the irregular path of a ship when sailing on different courses.

The object of traverse sailing is to reduce a traverse to a single course, when the distances sailed are so small that the curvature of the earth may be neglected. When a ship sails on different courses, the difference of latitude is equal to the difference between the sum of the northings and the sum of the southings; and, neglecting the earth's curvature, the departure is equal to the difference between the sum of the eastings and the sum of the westings. If, then, the difference of latitude and the departure for each course be taken from the traverse table, and arranged in appropriate columns, the difference of latitude for the whole time may be obtained exactly, and the departure nearly, by addition and subtraction; and the corresponding distance and course may be determined as in plane sailing.

EXAMPLES.

- 1. A ship sails on the following successive tracks:
 - 1. N.E. 23 miles.
 - 2. E.S.E. 45 "
 - . 3. E. by N. 34 "
 - 4. North 29 "
 - 5. N. by W. 31 "
 - 6. N.N.E. 17 "

Find the course and distance for the whole traverse.

We form a table as below, entering the courses from the table of rhumbs, page 138, and then enter the latitudes and departures taken from the traverse table.

Traverse Table.

No.	Course.	Distance.	N.	S.	E.	w.
1	N. 45° E.	23	16.26		16.26	
2	S. 67° 30′ E.	45		17.22	41.57	
3	N. 78° 45′ E.	34	6.63		33.35	1
4	North.	29	29.00			
5	N. 11° 15′ W.	31	30.40			6.05
6	N. 22° 30′ E.	17	15.71		6.51	
Su	ım of columns .		98.00	17.22	97.69	6.05

Sum of columns . . . 98.00 17.22 97.69 6.05

Diff. latitude=80.78 N. Dep.=91.64 E.

Hence the course is found by plane sailing N. 48° 36′ E., and the distance =122.2 miles.

The proportions are

Diff. latitude: radius:: departure: tang. course, Radius: diff. latitude:: sec. course: distance.

- 2. A ship leaving Sandy Hook makes the following courses and distances:
 - 1. S.E. 25 miles.
 - 2. E.S.E. 32 "
 - 3. East 17 "
 - 4. E. by S. 51 "
 - 5. South 45 "
 - 6. S. by E. 63 "

Required her latitude, the distance made, and the direct course.

Ans. Latitude=38° 1′ N.
Distance=193.7 miles.
Course =S. 40° 47′ E.

- 3. A ship from Pensacola, latitude 30° 19′, sails on the following successive courses:
 - 1 South 48 miles.
 - 2. S.S.W. 23 "
 - 3. S.W. 32 "

- 4 S.W. by S. 76 miles.
- 5. West 17 "
- 6. W.S.W. 54 "

Required her latitude, direct course, and distance.

Ans. Latitude= 27° 23′ N.

Course =S. 38° 39′ W.

Distance = 225.0 miles.

- 4. A ship from Bermuda, latitude 32° 22′, sails on the following successive courses:
 - 1. N.E. 66 miles.
 - 2. N.N.E. 14 "
 - 3. N.E. by E. 45 "
 - 4. East 21 "
 - 5. E. by N. 32 "

Required her latitude, direct course, and distance.

Ans. Latitude 33° 53′ N

Course = N. 57° 22′ E

Distance=168.4 miles.

- (196.) When the water through which a ship is moving has a progressive motion, the ship's progress is affected in the same manner as if she had sailed in still water, with an additional course and distance equal to the direction and motion of the current.
- Ex. 5. If a ship sail 125 miles N.N.E. in a current which sets W. by N. 32 miles in the same time, required her true course and distance.

Form a traverse table containing the course sailed by the ship and the progress of the current, and find the difference of latitude and departure. The resulting course and distance is found as in the preceding examples.

Traverse Table.

Courses.	Distance.	N.	E.	w.		
N. 22° 30′ E	125	115.49	47.84			
N. 78° 45′ W.	32	6.24		31.39		
	·	101.00				

Diff. latitude . . . $=121.73 ext{ } 47.84 ext{ } 31.39$

31.39

Departure . . . =16.45 E.

Hence the course is found by plane sailing N. 7° 42' E., and the distance=122.8 miles.

Ex. 6. A ship sails S. by E. for two hours at the rate of 9 miles an hour; then S. by W. for five hours at the rate of 8 miles an hour; and during the whole time a current sets W. by N. at the rate of two and a half miles an hour. Required the direct course and distance.

> Ans. The course is S. 21° 51′ W. Distance 57.6 miles.

PARALLEL SAILING.

(197.) Parallel sailing is when a ship sails exactly east or west, and therefore remains constantly on the same parallel of latitude. In this case the departure is equal to the distance sailed, and the difference of longitude may be found by the following

THEOREM.

The cosine of the latitude of the parallel is to radius, as the distance run is to the difference of longitude.

Let P be the pole of the earth, C the center, AB a portion of the equator, and DE any parallel of latitude; then will CA be the radius of the equator, and FD the radius of the parallel. Let DE be the distance sailed by the ship F on the parallel of latitude, then the difference of longitude will be measured by AB, the C

arc intercepted on the equator by the merid-

ians passing through D and E.

Since AB and DE correspond to the equal angles ACB, DFE, they are similar arcs, and are to each other as their Hence radii.

FD: CA:: arc DE: arc AB.

But FD is the sine of PD, or the cosine of AD, that is, the cosine of the latitude, and CA is the radius of the sphere; hence

Cosine of latitude: R:: distance: diff. longitude.

Cor. Like portions of different parallels of latitude are to each other as the cosines of the latitudes.

The length of a degree of longitude in different parallels may be computed by this theorem. A degree of longitude at the equator being 60 nautical miles, a degree in latitude 40° may be found by the proportion

R: cosine 40° :: 60: 45.96, the required length.

The following table is computed in the same manner.

(198.) Table showing the length of a degree of longitude for each degree of latitude.

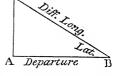
,		U									
Lat.	Miles.										
1	59.99	16	57.68	31	51.43	46	41.68	61	29.09	76	14.52
2	59.96	17	57.38	32	50.88	47	40.92	62	28.17	77	13.50
3	59.92	18	57.06	33	50.32	48	40.15	63	27.24	78	12.47
4	59.85	19	56.73	34	49.74	49	39.36	64	26.30	79	11.45
5	59.77	20	56.38	35	49.15	50	38.57	65	25.36	80	10.42
6	59.67		56.01				37.76				
7							36.94		23.44		
8	59.42	23	55.23	38	47.28	53	36.11	68	22.48	83	7.31
9	59.26	24	54.81	39	46.63	54	35.27	69	21.50	1	
10	59.09	25	54.38	40	45.96	55	34.41	70	20.52		5.23
11	58.90	26	53.93	41	45.28	56	33.55	71	19.53	86	4.19
12	58.69	27	53.46	42	44.59	57	32.68	72	18.54	87	3.14
13	58.46	28	52.98	43	43.88	58	31.80	73	17.54	88	2.09
							30.90				1.05
15	57.96	30	51.96	45	42.43	60	30.00	75	15.53	90	0.00

Let ABC represent a right-angled triangle; then, by Trigonometry, Art. 41,

cos. B : R :: AB : BC.

But, by the preceding Theorem, we have cos. lat.: R:: depart.: diff. long.,

trom which we see that if one leg of a right-angled triangle represent the dis-



tance run on any parallel, and the adjacent acute angle be made equal to the degrees of latitude of that parallel, then the hypothenuse will represent the difference of longitude.

EXAMPLES.

1. A ship sails from Sandy Hook, latitude 40° 28' N., longitude 74° 1' W., 618 miles due east. Required her present longitude.

Cos. 40° 28′: R:: 618: 812′.3=13° 32′, the difference of longitude.

This, subtracted from 74° 1′, leaves 60° 29′ W., the longitude required.

2. A ship in latitude 40° sails due east through nine degrees of longitude. Required the distance run.

Ans. 413.66 miles.

- 3. A ship having sailed on a parallel of latitude 261 miles, finds her difference of longitude 6° 15′. What is her latitude?

 Ans. Latitude 45° 54′.
- 4. Two ships in latitude 52° N., distant from each other 95 miles, sail directly south until their distance is 150 miles. What latitude do they arrive at?

Ans. Latitude 13° 34'

 \mathbf{E}

MIDDLE LATITUDE SAILING.

(199.) By the method just explained may be found the longitude which a ship makes while sailing on a parallel of latitude. When the course is oblique, the departure may be found by plane sailing, but a difficulty is found in converting this departure into difference of longitude.

If a ship sail from A to B, the departure is equal to eb+fc

+gd+hB, which is less than AC, but greater than DB. Navigators have assumed that the departure was equal to the distance between the meridians PA, PB, measured on a parallel EF, equidistant from A and B, called the *middle latitude*.

The middle latitude is equal to half the sum of the two extreme latitudes, if both

are north or both south; but to half their difference, if one is north and the other south.

The principle assumed in middle latitude sailing is not per feetly correct. For long distances the error is considerable, but the method is rendered perfectly accurate by applying to the middle latitude a correction which is given in the accompanying tables, page 149.

(200.) It has been shown that when a ship sails upon an oblique course, the distance, departure, and difference of latitude may be represented by the sides of a right-angled trian

gle. The difference of longitude is derived from the departure, in the same manner as in parallel sailing, the ship being supposed to sail on the middle latitude parallel. Hence, if we

combine the triangle ABC for plane sailing with the triangle BCD for parallel sailing, we shall obtain a triangle ABD, by which all the cases of middle latitude sailing may be solved.

In the triangle BCD,

Cos. CBD : BC :: R : BD ;

that is, cosine of middle latitude is to the departure, as radius is to the difference of longitude.

In the triangle ABD, since the angle D is A the complement of CBD, which represents the middle latitude, we have

Sin.
$$D : AB :: sin. A : BD$$
;

that is, cosine of middle latitude is to the distance, as the sine of the course is to the difference of longitude.

In the triangle ABC, we have the proportion

AC: BC:: R: tang. A.

But we have before had the proportion

Cos. CBD : BC :: R : BD.

The means being the same in these two proportions, we have Cos. CBD: AC:: tang. A: BD;

that is, cosine of middle latitude is to the difference of latitude, as the tangent of the course is to the difference of longitude.

The middle latitude should always be corrected according to the table on page 149. The given middle latitude is to be looked for either in the first or last vertical column, opposite to which, and under the given difference of latitude, is inserted the proper correction in minutes, which must be added to the middle latitude to obtain the latitude in which the meridian listance is exactly equal to the departure. Thus, if the midle latitude is 41°, and the difference of latitude 14°, the correction will be found to be 25′, which, added to the middle latitude, gives the corrected middle latitude 41° 25′.

EXAMPLES.

1. Find the bearing and distance of Liverpool, latitude 53° 22' N., longitude 2° 52' W., from New York, latitude 40° 42' N., longitude 74° 1′ W.

Here are given two latitudes and longitudes to find the course and distance.

The difference of latitude is $1. 12^{\circ} 40' = 760'$ The difference of longitude is 71° 9'=4269'. The middle latitude is To which add the correction from p. 149 The corrected middle latitude is . . . 47° 24′. Then, according to the third of the preceding theorems, Diff. lat.: cos. mid. lat.:: diff. long.: tang. course=N.75° 16' E

To find the distance by plane sailing,

Cos. course: diff. latitude:: R: distance=2988.4 miles.

2. A ship sailed from Bermuda, latitude 32° 22' N., longitude 64° 38' W., a distance of 500 miles, upon a course W.N W Required her latitude and longitude at that time.

By plane sailing,

R: distance:: cos. course: diff. latitude=191.3. Therefore the required latitude is 35° 33′; the middle latitude 33° 58′: and the corrected middle latitude 33° 59 Then we have

Cos. mid. lat.: distance:: sin. course: diff. long.=557'.1. Therefore the longitude required is 73° 55'.

3. A ship sails southeasterly from Sandy Hook, latitude 40° 28′ N., longitude 74° 1′ W., a distance of 395 miles, when her latitude is 34° 40' N. Required her course and longitude Ans. Course S. 28° 14' E.

Longitude 70° 5′ W.

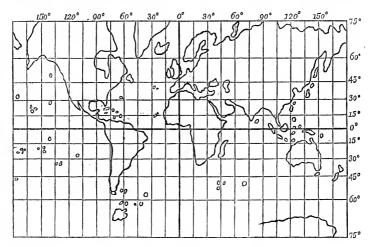
4. A ship sails from Brest, latitude 48° 23' N., longitude 4° 29' W., upon a course W.S.W., till her departure is 556 miles. Required the distance sailed and the place of the ship.

Ans. Distance 601.8 miles.

Latitude 44° 33′ N. Longitude 17° 57' W.

MERCATOR'S SAILING

(201.) Mercator's sailing is a method of computing difference of longitude on the principles of Mercator's chart. On this chart, the meridians, instead of converging toward the poles as they do on the globe, are drawn *parallel* to each other, by which means the distance of the meridians is every where



made too great except at the equator. To compensate for this, in order that the outline of countries may not be too much distorted, the degrees of latitude are proportionally enlarged, so that the distance between the parallels of latitude increases from the equator to the poles. In latitude 60° the distance of the meridians is twice as great, compared with a degree at the equator, as it is upon a globe, and a degree of latitude is here represented twice as great as near the equator The diameter of an island in latitude 60° is represented twice as great as if it was on the equator, and its area four times In latitude 70° 32′ the distance of the meridians is three times too great, in latitude 75° 31' four times too great and so on, by which means the relative dimensions of countries in high latitudes is exceedingly distorted. On this account it is not common to extend the chart beyond latitude 75°.

(202.) The distance of any parallel upon Mercator's chart from the equator has been computed, and is exhibited in the

accompanying tables, pages 142-8, which is called a Table of *Meridional Parts*. This table may be computed in the following manner:

According to Art. 197, cosine of latitude is to radius, as the departure is to the difference of longitude; that is, as a part of a parallyl of latitude is to a like part of the equator, or any meridian.

```
But by Art. 28, cosine: R:: R: secant; hence
```

But on Mercator's chart the distance between the meridians is the same in all latitudes; that is, a minute on a parallel of latitude is equal to a minute at the equator, or a geographical mile. Hence the length of one minute, on any part of a meridian, is equal to the secant of the latitude. Thus,

The first minute of the meridian = the secant of 1'; second " = "
$$2'$$
, third " = " $3'$, &c.,

The table of meridional parts is formed by adding together the minutes thus found. Thus,

```
Mer. parts of 1'=sec. 1';

Mer. parts of 2'=sec. 1'+sec. 2';

Mer. parts of 3'=sec. 1'+sec. 2'+sec. 3';

Mer. parts of 4'=sec. 1'+sec. 2'+sec. 3'+sec. 4',

&c., &c., &c.
```

Since the secants of small arcs are nearly equal to radius or unity, if the meridional parts are only given to one tenth of a mile, we shall have

The meridional parts of
$$1'=1.0$$
 mile;
" " $2'=2.0$ " " $3'=3.0$ " " $4'=4.0$ " &c.,

as shown in the table on page 142.

At 2° 33′ the sum of the small fractions omitted becomes greater than half of one tenth, and the meridional parts of 2° 33′ is 153.1; that is, the meridional parts exceed by one tenth of a mile the minutes of latitude. At 3° 40′ the excess is two tenths of a mile; at 4° 21′ the excess is three tenths;

and as the latitude increases, the meridional parts increase more rapidly, as is seen from the table.

An arc of Mercator's meridian contained between two parallels of latitude is called meridional difference of latitude. It is found by subtracting the meridional parts of the less latitude from the meridional parts of the greater, if both are north or south, or by adding them together if one is north and the other south. Thus,

The lat. of New York is 40° 42′; meridional parts=2677.8, 'New Orleans 29° 57′; " 1884.9.

The true diff. of lat. is $10^{\circ} 45'$; mer. diff. lat. is 792.9

If one latitude and the meridional difference of latitude be given, the true difference of latitude may be found by reversing this process. Thus,

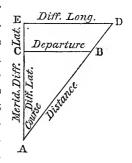
The meridional parts for New Orleans . . . =1884.9.

Meridional difference of latitude between New } = 792.0

York and New Orleans

Therefore the meridional parts for New York =2677.8, and the corresponding latitude from the table is 40° 42′.

(203.) If we take the figure ABC for plane sailing, as on page 139, and produce AC to E, making AE equal to the meridional difference of latitude, then will DE represent the difference of longitude corresponding to the departure BC. For we have seen (Art. 202) that the departure is to the difference of longitude as radius is to the secant of latitude, which is also the ratio of the true



difference of latitude to the meridional difference of latitude.

Now, from the similarity of the triangles ABC, ADE, we have

AC : AE :: BC : DE;

that is, the true difference of latitude is to the meridional difference of latitude, as the departure is to the difference of longitude.

Also, in the triangle ADE, we have

R: tan. A: AE: DE;

that is, radius is to the tangent of the course, as the meridional difference of latitude is to the difference of longitude.

EXAMPLES.

1. Find the bearing and distance from Sandy Hook, latitude 40° 28′ N., longitude 74° 1′ W., to Havre, latitude 49° 29′ N., longitude 0° 6′ E.

The true difference of latitude is 9° 1'= 541'; meridional difference of latitude = 767.1; difference of longitude is 74° 7'= 4447.

Hence, to find the course by the preceding proportion,

Mer. diff. lat.: diff. long.:: R: tan. course=N. 80° 13′ E.

To find the distance by plane sailing,

Cos. course: true diff. lat.:: R: distance=3183.8 miles.

2. Find the bearing and distance from Nantucket Shoals, in latitude 41° 4′ N., longitude 69° 55′ W., to Cape Clear, in latitude 51° 26′ N., longitude 9° 29′ W.

Ans. Course N. 76° E. Distance 2572.9 miles.

3. A ship sails from Sandy Hook a distance of 600 miles upon a course S. by E. Required the place of the ship.

The difference of latitude may be found by plane sailing, the difference of longitude by Mercator's sailing.

Ans. Latitude 30° 39′.5 N. Longitude 71° 36′.7 W.

4. A ship sails from St. Augustine, latitude 29° 52′ N., longitude 81° 25′ W., upon a course N.E. by E., until her latitude is found to be 34° 40′ N. What is then her longitude, and what distance has she run?

Ans. Longitude=72° 55′ W. Distance =518.4 miles.

5. A ship sails from Bermuda upon a course N.W. by W until her longitude is found to be 69° 30′ W. What is then her latitude, and what distance has she run?

Ans. Latitude 35° 4′ N. Distance 291.6 miles

6. A ship sailing from Madeira, latitude 32° 38′ N , longitude 16° ξ 5′ W., steers westerly until her latitude is 40° 2′ N.,

and her departure 2425 miles. Required her course, distance and longitude.

Ans. Course N. 79° 37′ W Distance 2465.3 miles. Longitude 67° 9′.3 W.

7. Find the bearing and distance from Sandy Hook, latitude 10° 28′ N., longitude 74° 1′ W., to the Cape of Good Hope latitude 34° 22′ S., longitude 18° 30′ E.

Ans. Course Distance

CHARTS.

(204.) The charts commonly used in navigation are plane charts, or Mercator's chart. In the construction of the former, the portion of the earth's surface which is represented is supposed to be a plane. The meridians are drawn parallel to each other, and the lines of latitude at equal distances. The distance between the parallels should be to the distance between the meridians, as radius to the cosine of the middle latitude of the chart. A chart of moderate extent constructed in this manner will be tolerably correct. The distance of the meridians in the middle of the chart will be exact, but on each side it will be either too great or too small.

When large portions of the earth's surface are to be represented, the error of the plane chart becomes excessive. To obviate this inconvenience Mercator's chart has been constructed. Upon this chart the meridians are represented by parallel lines, and the distance between the parallels of latitude is proportioned to the meridianal difference of latitude, as represented on page 149.

We have seen that the meridional difference of latitude is to the difference of longitude as radius is to the tangent of the course. Hence, while the course remains unchanged, the ratio of the meridional difference of latitude to the difference of longitude is constant; and, therefore, every rhumb line will be represented on Mercator's chart by a straight line. This property renders Mercator's chart peculiarly convenient to navigators

The preceding sketch affords a very incomplete view of the present state of the science of navigation. The most accurate method of ascertaining the situation of a vessel at sea is by means of astronomical observations. For these, however, the student must be referred to some treatise on Astronomy.

BOOK VI.

SPHERICAL TRIGONOMETRY.

(205.) Spherical trigonometry teaches how to determine the several parts of a spherical triangle from having certain parts given.

A spherical triangle is a portion of the surface of a sphere, bounded by three arcs of great circles, each of which is less than a semicircumference.

RIGHT-ANGLED SPHERICAL TRIANGLES.

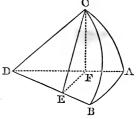
THEOREM I.

(206.) In any right-angled spherical triangle, the sine of the hypothenuse is to radius, as the sine of either side is to the sine of the opposite angle.

Let ABC be a spherical triangle, right-angled at A; then

will the sine of the hypothenuse BC be to radius, as the sine of the side AC is to the sine of the angle ABC.

Let D be the center of the sphere; join AD, BD, CD, and draw CE perpendicular to DB, which will, therefore, be the sine of the hypothenuse BC. From the point E draw the



straight line EF, in the plane ABD, perpendicular to BD, and join CF. Then, because DB is perpendicular to the two lines CE, EF, it is perpendicular to the plane CEF; and, consequently, the plane CEF is perpendicular to the plane ABD (Geom., Prop. 6, B. VII.). But the plane CAD is also perpendicular to the plane ABD; therefore their line of common section, CF, is perpendicular to the plane ABD; hence CFD, CFE are right angles, and CF is the sine of the arc AC.

Now, in the right-angled plane triangle CFE,

CE: radius:: CF: sine CEF

But since CE and FE are both at right angles to DB, the angle CEF is equal to the inclination of the planes CBD, ABD; that is, to the spherical angle ABC. Therefore,

sine BC: R:: sine AC: sine ABC.

(207.) Cor. 1. In any right-angled spherical triangle, the sines of the sides are as the sines of the opposite angles.

For, by the preceding theorem,

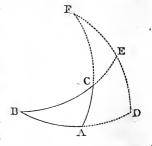
sine BC: R:: sine AC: sine ABC, sine BC: R:: sine AB: sine ACB;

and sine BC: R:: sine AB: sine ACB; therefore, sine AC: sine AB:: sine ABC: sine ACB.

Cor. 2. In any right-angled spherical triangle, the cosine of either of the sides is to radius, as the cosine of the hypothenuse is to the cosine of the other side.

Let ABC be a spherical triangle, right-angled at A. De-

scribe the circle DE, of which B is the pole, and let it meet the three sides of the triangle ABC produced in D, E, and F. Then, because BD and BE are quadrants, the arc DF is perpendicular to BD. And since BAC is a right angle, the arc AF is perpendicular to BD. Hence the point F, where the arcs FD, FA intersect



each other, is the pole of the arc BD (Geom., Prop. 5, Cor. 2, B. IX.), and the arcs FA, FD are quadrants.

Now, in the triangle CEF, right-angled at the point E, according to the preceding theorem, we have

sine CF: R:: sine CE: sine CFE.

But CF is the complement of AC, CE is the complement of BC, and the angle CFE is measured by the arc AD, which is the complement of AB. Therefore, in the triangle ABC, we have

 \cos AC : R :: \cos BC : \cos AB.

Cor. 3. In any right-angled spherical triangle, the cosine of either of the sides is to radius, as the cosine of the angle opposite to that side is to the sine of the other angle.

For, in the triangle CEF, we have

sine CF: R:: sine EF: sine ECF.

But sine CF is equal to cos. CA. EF is the complement of

ED, which measures the angle ABC, that is, sine EF is equal to cos. ABC, and sine ECF is the same as sine ACB; therefore.

cos. AC: R:: cos. ABC: sine ACB

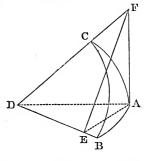
THEOREM II.

(208.) In any right-angled spherical triangle, the sine of either of the sides about the right angle is to the cotangent of the adjacent angle, as the tangent of the remaining side is to radius.

Let ABC be a spherical triangle, right-angled at A; then

will the sine of the side AB be to the cotangent of the angle ABC, as the tangent of the side AC is to radius.

Let D be the center of the sphere; join AD, BD, CD; draw AE perpendicular to BD, which will, therefore, be the sine of the arc AB. Also, from D the point E in the plane BDC, draw the straight line EF perpendicular to BD, meeting DC produced in F, and



join AF. Then will AF be perpendicular to the plane ABD because, as was shown in the preceding theorem, it is the common section of the two planes ADF, AEF, each perpendicular to the plane ADB. Therefore FAD, FAE are right angles and AF is the tangent of the arc AC.

Now, in the triangle AEF, right-angled at A, we have AE: radius:: AF: tang. AEF.

But AE is the sine of the arc AB, AF is the tangent of the arc AC, and the angle AEF is equal to the inclination of the planes CBD, ABD, or to the spherical angle ABC; hence

sine AB: R:: tang. AC: tang. ABC.

And because, Art. 28,

R : cot. ABC :: tang. ABC : R;

therefore, sine AB: cot. ABC:: tang. AC: R.

(209.) Cor. 1. In any right-angled spherical triangle, the cosine of the hypothenuse is to the cotangent of either of the oblique angles, as the cotangent of the other oblique angles is to radius

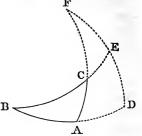
Let ABC be a spherical triangle, right-angled at A. De-

scribe the circle DEF, of which B is the pole, and construct the complemental triangle CEF, as in Cor. 2, Theorem I.

Then, in the triangle CEF, according to the preceding theorem, we have

sine CE : cot. ECF :: tan. EF : R.

But CE is the complement of BC,



EF is the complement of ED, the measure of the angle ABC; and the angle ECF is equal to ACB, being its vertical angle; hence

cos. BC: cot. ACB:: cot. ABC: R.

Cor. 2. In any right-angled spherical triangle, the cosine of either of the oblique angles is to the tangent of the adjacent side, as the cotangent of the hypothenuse is to radius.

For, in the complemental triangle CEF, according to the

preceding theorem, we have

sine EF: cot. CFE:: tan. CE: R;

hence, in the triangle ABC,

cos. ABC: tan. AB:: cot. BC: R.

Napier's Rule of the Circular Parts.

(210.) The two preceding theorems, with their corollaries, are sufficient for the solution of all cases of right-angled spherical triangles, and a rule was invented by Napier by means of which these principles are easily retained in mind.

If, in a right-angled spherical triangle, we set aside the right angle, and consider only the five remaining parts of the triangle, viz., the three sides and the two oblique angles, then the two sides which contain the right angle, and the complements of the other three, viz., of the two angles and the hypothenuse. are called the *circular parts*.

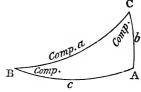
Thus, in the triangle ABC, right-angled at A, the circular parts are AB, AC, with the complements of B, BC, and C.

When, of the five circular parts, any one is taken for the middle part, then, of the remaining four, the two which are immediately adjacent to it on the right and left are called the

adjacent parts; and the other two, each of which is separated from the middle by an adjacent part,

are called opposite parts.

In every question proposed for solution, three of the circular parts are concerned, two of which are given, and one required; and of these three, B the middle part must be such that



the other two may be equidistant from it; that is, may be either both adjacent or both opposite parts. The value of the part required may then be found by the following

RULE OF NAPIER.

(211.) The product of the radius and the sine of the middle part, is equal to the product of the tangents of the adjacent parts, or to the product of the cosines of the opposite parts.

It will assist the learner in remembering this rule to remark, that the first syllable of each of the words tangent and adjacent contains the same vowel a, and the first syllable of the words cosine and opposite contains the same vowel o.

It is obvious that the cosine of the complement of an angle is the sine of that angle, and the tangent of a complement is a cotangent, and vice versa.

In the triangle ABC, if we take the side b as the middle part, then the side c and the complement of the angle C are the adjacent parts, and the complements of the angle B and of the hypothenuse a are the opposite parts. Then, according to Napier's rule, R sin. b=tan. c cot. C, which corresponds with Theorem II.

Also, by Napier's rule,

R sin. $b=\sin a \sin B$,

which corresponds with Theorem I.

Making each of the circular parts in succession the middle part, we obtain the ten following equations:

R sin. $b = \sin a \sin B = \tan c \cot C$.

R sin. $c = \sin a \sin C = \tan b \cot B$.

R cos. B=cos. b sin. C=cot. a tan. c.

R cos. $a = \cos b \cos c = \cot B \cot C$.

R cos. $C = \cos c \sin B = \cot a \tan b$.

(212.) In order to determine whether the quantity sought is less or greater than 90°, the algebraic sign of each term should be preserved whenever one of them is negative. If the quantity sought is determined by means of its cosine, tangent, or cotangent, the algebraic sign of the result will show whether this quantity is less or greater than 90°; for the cosines, tangents, and cotangents are positive in the first quadrant, and negative in the second. But since the sines are positive in both the first and second quadrants, when a quantity is determined by means of its sine, this rule will leave it ambiguous whether the quantity is less or greater than 90°. The ambiguity may, however, generally be removed by the following rule.

In every right-angled spherical triangle, an oblique angle and its opposite side are always of the same species; that is, both are greater, or both less than 90°.

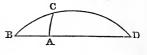
This follows from the equation

R sin. $b = \tan c \cot C$;

where, since sine b is always positive, tane c must always have the same sign as cot. C; that is, the side c and the opposite angle C both belong to the same quadrant.

(213.) When the given parts are a side and its opposite angle, the problem admits of two solutions; for two right-angled spherical triangles may always be found, having a side and its opposite angle the same in both, but of which the remaining sides and the remaining angle of the one are the supplements of the remaining sides and the remaining angle of the other. Thus, let BCD, BAD be the halves of two great circles, and

let the arc CA be drawn perpendicular to BD; then ABC, ADC are two right-angled triangles, having the side B AC common, and the opposite angle



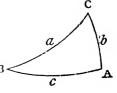
B equal to the angle D; but the side DC is the supplement of BC, AD is the supplement of AB, and the angle ACD is the supplement of ACB.

EXAMPLES.

1. In the right-angled spherical triangle ABC, there are given $a=63^{\circ}$ 56' and $b=40^{\circ}$. Required the other side c, and the angles B and C.

It find the side c.

Here the circular parts concerned are the two legs and the complement of the hypotheruse; and it is evident that if the complement of a be made the middle part, b and c will be opposite parts; hence, by Napier's rule,



R cos. $a = \cos b \cos c$;

or, reducing this equation to a proportion,

 $\cos b : \mathbf{R} :: \cos a : \cos c = 54^{\circ} 59' 49''.$

To find the angle B.

Here b is the *middle part*, and the complements of B and a are opposite parts; hence

R sin. $b = \cos$. (comp. a)×cos. (comp. B)=sin. a sin. B, or sin. a: R:: sin. b: sin. B=45° 41′ 25″. B is known to be an acute angle, because its opposite side is less than 90°.

To find the angle C.

Here the complement of C is the $middle\ part$; also b and the complement of a are $adjacent\ parts$; hence

R cos. C=cot. a tan. b,

or R: tan. $b := \cot a : \cos C = 65^{\circ} 45' 57''$.

Ex. 2. In a right-angled triangle ABC, there are given the hypothenuse $a=91^{\circ}$ 42′, and the angle B=95° 6′. Required the remaining parts.

To find the angle C.

Make the complement of the hypothenuse the middle part; then R cos. $a=\cot$. B cot. C.

Whence

C=71° 36′ 47″.

To find the side c.

Make the complement of the angle B the middle part; and we have $R \cos B = \cot a \tan c$.

Whence

 $c=71^{\circ} 32' 14'$.

To find the side b.

Make the side b the middle part; then

R sin. $b=\sin a \sin B$. $b=95^{\circ} 22' 30''$.

Whence

b is known to be greater than a quadrant, because its opposite angle is obtuse.

Ex. 3. In the right-angled triangle ABC, the side b is 26° 4′, and its opposite angle B 36°. Required the remaining parts.

Ans. $\begin{cases} a = 48^{\circ} \ 22' \ 52'', \text{ or } 131^{\circ} \ 37' \ 8'' \\ c = 42^{\circ} \ 19' \ 17'', \text{ or } 137^{\circ} \ 40' \ 43''. \\ C = 64^{\circ} \ 14' \ 26'', \text{ or } 115^{\circ} \ 45' \ 34''. \end{cases}$

This example, it will be seen, admits of two solutions, conformably to Art. 213.

Ex. 4. In the right-angled spherical triangle ABC, there are given the side c, 54° 30′, and its adjacent angle B, 44° 50′. Required the remaining parts.

Ans. $\begin{cases} C = 65^{\circ} \ 49' \ 53''. \\ a = 63^{\circ} \ 10' \ 4''. \\ b = 38^{\circ} \ 59' \ 11'' \end{cases}$

Why is not the result ambiguous in this case?

Ex. 5. In the right-angled spherical triangle ABC, the side b is 55° 28′, and the side c 63° 15′. Required the remaining parts.

Ans. $\begin{cases} a = 75^{\circ} \ 13' \ 2''. \\ B = 58^{\circ} \ 25' \ 47 \\ C = 67^{\circ} \ 27' \ 1'. \end{cases}$

Ex. 6. In the right-angled spherical triangle ABC, there are given the angle $B=69^{\circ}$ 20', and the angle $C=58^{\circ}$ 16'. Required the remaining parts.

Ans.
$$\begin{cases} a = 76^{\circ} 30' 37''. \\ b = 65^{\circ} 28' 58''. \\ c = 55^{\circ} 47' 46''. \end{cases}$$

(214.) A triangle, in which one of the sides is equal to a quadrant, may be solved upon the same principles as right-angled triangles, for its polar triangle will contain a right angle. See *Geom.*, Prop. 9, B. IX.

Ex. 7. In the spherical triangle ABC, the side BC=90°, the angle C=42° 10′, and the angle A=115° 20′. Required the remaining parts.

Taking the supplements of the given parts, we shall have

in the polar triangle the hypothenuse $a'=180^{\circ}-115^{\circ}$ $20'=64^{\circ}$ 40', and one of the sides, $c'=180^{\circ}-42^{\circ}$ $10'=137^{\circ}$ 50', from which, by Napier's rule, we find

Hence, taking the supplements of these arcs, we find the parts of the required triangle are

Ex. 8. In the spherical triangle ABC, the side $AC=90^{\circ}$, the angle $C=69^{\circ}$ 13' 46", and the angle $A=72^{\circ}$ 12' 4". Required the remaining parts.

Ans.
$$\begin{cases} AB = 70^{\circ} & 8' \ 39''. \\ BC = 73^{\circ} \ 17' \ 29''. \\ B = 96^{\circ} \ 13' \ 23 \end{cases}$$

OBLIQUE-ANGLED SPHERICAL TRIANGLES.

THEOREM III.

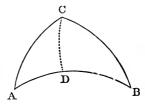
(215.) In any spherical triangle, the sines of the sides are proportional to the sines of the opposite angles.

In the case of right-angled spherical triangles, this proposi-

tion has already been demonstrated. Let, then, ABC be an oblique-angled triangle; we are to prove that

sin. BC: sin. AC:: sin. A: sin. B.

Through the point C draw an arc of a great circle CD perpendicular to AB. Then, in the spherical triangle



ACD, right-angled at D, we have, by Napier's rule,

Also, in the triangle BCD, we have

Hence sin AC sin. A=sin. BC sin. B, sin. BC: sin. AC:: sin. A: sin. B.

(216.) Cor. 1. In any spherical triangle, the cosines of the sides are proportional to the cosines of the segments of the base, made by a perpendicular from the opposite angle.

For, by Theorem I., Cor. 2.

 \cos . CD: R:: \cos . AC: \cos . AD.

Also, \cos CD: R:: \cos BC: \cos BD.

Hence cos. AC: cos. BC:: cos. AD: cos. BD.

Cor. 2. The cosines of the angles at the base are proportional to the sines of the segments of the vertical angle.

For, by Theorem I., Cor. 3,

 \cos . CD: R:: \cos . A: \sin . ACD.

Also, cos. CD: R:: cos. B: sin. BCD. Hence cos. A: cos. B:: sin. ACD: sin. BCD.

Cor. 3. The sines of the segments of the base are reciprocally proportional to the tangents of the angles at the base.

For, by Theorem II.,

sin. AD: R:: tan. CD: tan. A.

Also, sin. BD: R:: tan. CD: tan. B.

Hence sin. AD: sin. BD:: tan. B: tan. A.

Cor. 4. The cotangents of the two sides are proportional to the cosines of the segments of the vertical angle.

For, by Theorem II., Cor. 2,

cos. ACD: cot. AC::tan. CD: R.

Also, cos. BCD: cot. BC:: tan. CD: R.

Hence cos. ACD: cos. BCD:: cot. AC: cot. BC.

THEOREM IV.

(217.) If from an angle of a spherical triangle a perpendicular be drawn to the base, then the tangent of half the sum of the segments of the base is to the tangent of half the sum of the sides, as the tangent of half the difference of the sides is to the tangent of half the difference of the segments of the base.

Let ABC be any spherical triangle, and let CD be drawn from C perpendicular to the base AB; then $\tan \frac{1}{2}(BD+AD)$: $\tan \frac{1}{2}(BC+AC)$: $\tan \frac{1}{2}(BD-AD)$.

Let BC=a, AC=b, BD=m, and AD=n. Then, by Theorem III., Cor. 1,

A n D m

 $\cos a : \cos b : \cos m : \cos n$

Whence, Geom., Prop. 7, Cor., B. II.,

cos. b+cos. a: cos. b-cos. a:: cos. n+cos. m: cos. n-cos. mBut by Trig., Art. 76,

cos. $b+\cos a: \cos b-\cos a: \cot \frac{1}{2}(a+b): \tan \frac{1}{2}(a-b)$. Also, by the same Art.,

cos. $n+\cos m : \cos n - \cos m : \cot \frac{1}{2}(m+n) : \tan \frac{1}{2}(m-n)$ Therefore

cot. $\frac{1}{2}(a+b)$: cot. $\frac{1}{2}(m+n)$:: tan. $\frac{1}{2}(a-b)$: tan. $\frac{1}{2}(m-n)$.

But, since tangents are reciprocally as their cotangents, Art. 28, we have

cot. $\frac{1}{2}(a+b)$: cot. $\frac{1}{2}(m+n)$:: tan. $\frac{1}{2}(m+n)$: tan. $\frac{1}{2}(a+b)$ Hence

 $\tan \frac{1}{2}(m+n) : \tan \frac{1}{2}(a+b) : : \tan \frac{1}{2}(a-b) : \tan \frac{1}{2}(m-n).$

(218.) In the solution of oblique-angled spherical triangles six cases may occur, viz.:

- 1. Given two sides and an angle opposite one of them.
- 2. Given two angles and a side opposite one of them.
- 3. Given two sides and the included angle.
- 4. Given two angles and the included side.
- 5. Given the three sides.
- 6. Given the three angles.

CASE I.

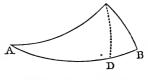
(219.) Given two sides and an angle opposite one of them, to find the remaining parts.

In the triangle ABC, let there be given the two sides AC

and BC, and the angle A opposite one of them. The angle B may be found by Theorem III.

sin. BC: sin. AC:: sin. A: sin. B.

From the angle C let fall the perpendicular CD upon the side AB.



The triangle ABC is divided into two right-angled triangles, in each of which there is given the hypothenuse and the angle at the base. The remaining parts may then be found by Napier's rule.

Ex. 1. In the oblique-angled spherical triangle ABC, the

side AC=70° 10′ 30″, BC=80° 5′ 4″, and the angle Λ =33° 15′ 7″. Required the other parts.

sin BC: sin. AC:: sin. A: sin. B=31° 34′ 38″

Then, in the triangle ACD,

R cos. $AC = \cot A \cot ACD$.

Whence

ACD=77° 27′ 47″.

Also, in the triangle BCD,

R cos. BC=cot. B cot. BCD.

Whence

BCD= $83^{\circ} 57' 29''$.

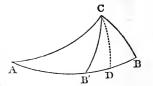
Therefore ACB=161° 25′ 16″.

To find the side AB.

sin. A: sin. ACB:: sin. BC: sin. AB=145° 5′ 0″.

When we have given two sides and an opposite angle, there are, in general, two solutions, each of which will satisfy the conditions of the problem. If the side AC, the angle A, and

the side opposite this angle are given, then, with the latter for radius, describe an arc cutting the arc AB in the points B and B'. The arcs CB, CB' will be equal, and each of the triangles ACB, ACB' will satisfy the



conditions of the problem. There is the same ambiguity in the numerical computation. The angle B is found by means of its sine. But this may be the sine either of ABC, or of its supplement AB'C (Art. 27). In the preceding example, the first proportion leaves it ambiguous whether the angle B is 31° 34′ 38′, or its supplement 148° 25′ 22″. In order to avoid false solutions, we should remember that the greater side of a spherical triangle must lie opposite the greater angle, and conversely (Geom., Prop. 17, B. IX.). Thus, since in the preceding example the side AC is less than BC, the angle B must be less than A, and, therefore, can not be obtuse.

If the quantity sought is determined by means of its cosine, tangent, or cotangent, the algebraic sign of the result will show whether this quantity is less or greater than 90°; for the cosines, tangents, and cotangents are positive in the first quadrant, and negative in the second. Hence the algebraic sign

of each term of a proportion should be preserved whenever one of them is negative.

Ex. 2. In the spherical triangle ABC, the side $a=124^{\circ}$ 53', $b=31^{\circ}$ 19', and the angle A=16° 26'. Required the remaining parts.

Ans.
$$\begin{cases} B = 10^{\circ} 19' 34' \\ C = 171^{\circ} 48' 22'' \\ c = 155^{\circ} 35' 22'' \end{cases}$$

CASE II.

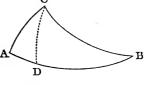
(220.) Given two angles and a side opposite one of them, to find the remaining parts.

In the triangle ABC let there be given two angles, as A and

B, and the side AC opposite to one of them. The side BC may be found by Theorem III.

sin. B: sin. A:: sin. AC: sin. BC.

From the unknown angle C draw CD perpendicular to AB; then will



the triangle ABC be divided into two right-angled triangles, in each of which there is given the hypothenuse and the angle at the base. Whence we may proceed by Napier's rule, as in Case I.

Ex. 1. In the oblique-angled spherical triangle ABC, there are given the angle $A=52^{\circ}$ 20', $B=63^{\circ}$ 40', and the side $b=83^{\circ}$ 25'. Required the remaining parts.

sin. B: sin. A:: sin. AC: sin. BC=61° 19′ 53″.

Then, in the triangle ACD,

cot. AC: R:: cos. A: tan. AD=79° 18′ 17″.

Also, in the triangle BCD,

cot. BC: R:: cos. B: tan. BD=39° 3′ 8″.

Hence AB=118° 21′ 25″.

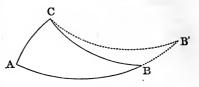
To find the angle ACB.

sin. BC: sin. AB:: sin. A: sin. ACB=127° 26′ 47″.

When we have given two angles and an opposite side, there are, in general, two solutions, each of which will satisfy the conditions of the problem. If the angle A, the side AC, and

the angle opposite this side are given, then through the point

C there may generally be drawn two arcs of great circles CB, CB', making the same angle with AB, and each of the triangles ABC, AB'C will satisfy the condi-



tions of the problem. There is the same ambiguity in the numerical computation, since the side BC is found by means of its sine (Art. 27). In the preceding example, however, there is no ambiguity, because the angle A is less than B, and, therefore, the side a must be less than b, that is, less than a quadrant.

Ex. 2. In the oblique-angled spherical triangle ABC, the angle A is 128° 45', the angle C=30°35', and BC=68°50'.

Required the remaining parts.

It will be observed that in this case the perpendicular BD, drawn from the angle B, falls without the triangle ABC, and therefore the side AC is the difference between the segment. CD and AD.

(AB=37° 28' 20'

Ans. $\begin{cases} AB=37^{\circ} 28' 20' \\ AC=40^{\circ} 9' 4'' \\ B=32^{\circ} 37' 58'' \end{cases}$

CASE III.

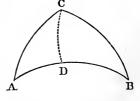
(221.) Given two sides and the included angle, to find the remaining parts.

In the triangle ABC let there be given two sides, as AE

AC, and the included angle A. Let fall the perpendicular CD on the side AB; then, by Napier's rule,

R cos. A=tan. AD cot. AC.

Having found the segment AD, the segment BD becomes known; then, by Theorem III., Cor. 3,



sin. BD: sin. AD:: tan. A: tan. B.

The remaining parts may now be found by Theorem III. Ex. 1. In the spherical triangle ABC, the side AB=73° 20, AC=41° 45′, and the angle A=30° 30′. Required the remaining parts.

cot. AC: cos. A:: R: tan. AD=37° 33′ 41″.

Hence BD=35° 46′ 19″.

sin. BD: sin. AD:: tan. A.: tan. B=31° 33′ 43″.

Also, by Theorem III., Cor. 1,

 \cos AD : \cos BD :: \cos AC : \cos BC=40° 13′ 0″.

Then, by Theorem III.,

sin. BC: sin. AB:: sin. A: sin. ACB=131° 8' 47'.

Ex. 2. In the spherical triangle ABC, the side AB=78° 15′, AC=56° 20′, and the angle A=120°. Required the other parts.

Ans. $\begin{cases} B = 48^{\circ} 57' 29''. \\ C = 62^{\circ} 31' 40''. \\ BC = 107^{\circ} 7' 45'' \end{cases}$

CASE IV.

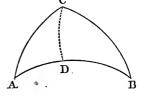
(222.) Given two angles and the included side, to find the remaining parts.

In the triangle ABC let there be given two angles, as A and

ACB, and the side AC included between them. From C let fall the perpendicular CD on the side AB. Then, by Napier's rule,

R cos. AC=cot. A cot. ACD.

Having found the angle ACD, the angle BCD becomes known; then, by Theorem III., Cor. 4,



cos. ACD: cos. BCD:: cot. AC: cot. BC.

The remaining parts may now be found by Theorem II1.

Ex. 1. In the spherical triangle ABC, the angle A=32° 10′, the angle ACB=133° 20′, and the side AC=39° 15′. Required the other parts.

cot. A: cos. AC:: R: cot. ACD=64° 1′ 57″.

Hence BCD=69° 18′ 3″.

Then

cos. ACD : cos. BCD :: cot. AC : cot. BC=45° 20′ 43′

Also, by Theorem III., Cor. 2,

sin. ACD: sin. BCD:: cos. A: cos. $B=28^{\circ} 15' 47''$. Then, by Theorem III.,

sin. B: sin ACB:: sin. AC: sin. AB=76° 23' 5".

Ex. 2. In the spherical triangle ABC, the angle A=125° 20′, the angle C=48° 30′, and the side AC=83° 13′. Required the remaining parts.

Ans.
$$\begin{cases} AB = 56^{\circ} 39' & 9''. \\ BC = 114^{\circ} 30' 24''. \\ B = 62^{\circ} 54' 38. \end{cases}$$

CASE V.

(223.) Given the three sides of a spherical triangle, to find the angles.

In the triangle ABC let there be given the three sides. From one of the angles, as C, draw CD perpendicular to AB. Then, by The-

orem IV., $\tan \frac{1}{2}AB : \tan \frac{1}{2}(AC+BC) : \tan \frac{1}{2}(AC-BC) : \tan \frac{1}{2}(AD-BD)$.

Hence AD and BD become known; then, by Napier's rule,

R cos. A=tan. AD cot. AC.

The other angles may now be easily found.

It is generally most convenient to let fall the perpendicular upon the longest side of the triangle.

Ex. 1. In the spherical triangle ABC, the side AB=112³ 25', AC=60° 20', and BC=81° 10'. Required the angles. tan. 56° $12\frac{1}{2}$ ': tan. 70° 45':: tan. 10° 25': tan. 19° 24' 26".

Hence $\overline{AD} = 36^{\circ} 48' 4''$, and $\overline{BD} = 75^{\circ} 36' 56''$.

Then R: tan. AD:: cot. AC: cos. A=64° 46′ 36″.

Also, R: tan. BD:: cot. BC: cos. B=52° 42′ 12″.

Then sin. AC: sin. AB:: sin. B: sin. ACB=122° 11′ 6″.

Ex. 2. In the spherical triangle ABC, the side AB= 40° 35' AC= 39° 10', and BC= 71° 15. Required the angles.

Ans.
$$\begin{cases} A=130^{\circ} \ 35' \ 55''. \\ B=30^{\circ} \ 25' \ 34'' \\ C=31^{\circ} \ 26' \ 32''. \end{cases}$$

CASE VI.

(224.) Given the three angles of a spherical triangle, to find the sides.

If A, B, C are the angles of the given triangle, and a, b, c its sides, then 180°-A, 180°-B, and 180°-C are the sides

of its polar triangle, whose angles may be found by Case V. Then the supplements of those angles will be the sides a, b, ϵ of the proposed triangle.

Ex. 1. In the spherical triangle ABC, the angle $A=125^{\circ}$ 34', $B=98^{\circ}$ 44', and $C=61^{\circ}$ 53'. Required the sides.

The sides of the polar triangle are

54° 26′, 81° 16′, and 118° 7′.

From which, by Case V., the angles are found to be 134° 6′ 21″, 41° 28′ 17″, and 53° 34′ 47″.

Hence the sides of the proposed triangle are

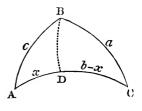
AB=45° 53′ 39″, BC=138° 31′ 43″, and AC=126° 25′ 13″

Ex. 2. In the spherical triangle ABC, the angle $A=109^{\circ}$ 55', $B=116^{\circ}$ 38', and $C=120^{\circ}$ 43'. Required the sides.

Ans.
$$\begin{cases} a = 98^{\circ} 21' 20'' \\ b = 109^{\circ} 50' 10'' \\ c = 115^{\circ} 13' 7'' \end{cases}$$

TRIGONOMETRICAL FORMULÆ.

(225.) Let ABC be any spherical triangle, and from the angle B draw the arc BD perpendicular to the base AC. Represent the sides of the triangle by a, b, c, and the segment AD by x; then will CD be equal to b-x.



By Theorem III., Cor., 1,

$$\cos c : \cos a :: \cos x : \cos (b-x)$$

$$:: \cos. x : \frac{\cos. b \cos. x + \sin. b \sin. x}{R}$$

(Trig., Art. 72), formula (4).

Whence

R cos. a cos. $x=\cos b \cos c \cos x + \sin b \cos c \sin x$, or, dividing each term by cos. x, and substituting the value of $\frac{\sin x}{\cos x}$ (Art. 28), we obtain

 $R^2 \cos a = R \cos b \cos c + \sin b \cos c \tan x$ But by Theorem II., Cor. 2, we have

tan.
$$x = \frac{\text{R cos. A}}{\text{cot. }c} = \frac{\text{cos. A sin. }c}{\text{cos. }c}$$
 (Art. 28).

Hence $R^2 \cos a = R \cos b \cos c + \sin b \sin c \cos A$, (1) from which all the formulæ necessary for the solution of spherical triangles may be deduced.

In a similar manner we obtain

$$R^2 \cos b = R \cos a \cos c + \sin a \sin c \cos B,$$
 (2)

$$R^2 \cos c = R \cos a \cos b + \sin a \sin b \cos C.$$
 (3)

These equations express the following Theorem:

The square of radius multiplied by the cosine of either side of a spherical triangle, is equal to radius into the product of the cosines of the two other sides, plus the product of the sines of those sides into the cosine of their included angle.

(226.) From equation (1) we obtain, by transposition,

$$\cos. A = \frac{R^2 \cos. a - R \cos. b \cos. c}{\sin. b \sin. c},$$

a formula which furnishes an angle of a triangle when the three sides are known.

If we add R to each member of this equation, we shall have

R+cos. A=
$$\frac{R^2 \cos. a+R \sin. b \sin. c-R \cos. b \cos. c}{\sin. b \sin. c}$$

But, by Art. 74, R+cos.
$$A = \frac{2 \cos^{\frac{21}{2}}A}{R}$$
.

And, by Art. 72, formula (2), by transposition,

R sin. b sin. c-R cos. b cos. $c=-R^2$ cos. (b+c).

Hence, by substitution, we obtain

$$\frac{2 \cos^{\frac{2}{2}A}}{R} = \frac{R^{2}(\cos a - \cos (b+c))}{\sin b \sin c}$$

$$= \frac{2R \sin^{\frac{1}{2}}(a+b+c) \sin^{\frac{1}{2}}(b+c-a)}{\sin b \sin c},$$

by Art. 75, formula (4).

If, then, we put $s=\frac{1}{2}(a+b+c)$, that is, half the sum of the sides, we shall find

$$\cos \frac{1}{2} A = R \sqrt{\frac{\sin s \sin (s-a)}{\sin b \sin c}}.$$
 (4)

By subtracting cos. A from R instead of adding, we shall obtain, in a similar manner,

$$\sin \frac{1}{2} A = R \sqrt{\frac{\sin (s-b) \sin (s-c)}{\sin b \sin c}}.$$
 (5)

Either formula (4) or (5) may be employed to compute the angles of a spherical triangle when the three sides are known, and this method may be preferred to that of Art. 223.

Ex. 1. In a spherical triangle there are given $a=63^{\circ}$ 50'. $b=80^{\circ}$ 19', and $c=120^{\circ}$ 47'. Required the three angles.

Here half the sum of the sides is $132^{\circ} 28'=s$.

Also,
$$s-a=68^{\circ} 38'$$
.

Using formula (4), we have

log. sine s, 132° 28′ . . 9.867862 log. sine (s-a), 68° 38′ . . 9.969075 —log. sine b, 80° 19′ comp. 0.006232 —log. sine c, 120° 47′ comp. 0.065952 Sum 19.909121

log. cos. $\frac{1}{2}$ A, 25° 45' 19" 9.954560.

Hence the angle A=51° 30′ 38″.

The remaining angles may be found by Theorem III., or by formulas similar to formula (4).

$$\cos \frac{1}{2}B = R\sqrt{\frac{\sin s \sin (s-b)}{\sin a \sin c}}.$$

$$\cos \frac{1}{2}C = R\sqrt{\frac{\sin s \sin (s-c)}{\sin a \sin b}}.$$

We thus find the angle $B = 59^{\circ} 16' 46''$, and $C = 131^{\circ} 28' 36''$.

Ex. 2. In a spherical triangle there are given $a=115^{\circ}$ 20', $b=57^{\circ}$ 30', and $c=82^{\circ}$ 28'. Required the three angles.

Ans.
$$\begin{cases} A=126^{\circ}\ 35'\ 2''. \\ B=\ 48^{\circ}\ 31'\ 42''. \\ C=\ 61^{\circ}\ 43'\ 58''. \end{cases}$$

(227.) By means of the polar triangle, we may convert the preceding formulæ for angles into formulæ for the sides of a triangle, since the angles of every triangle are the supplements of the sides of its polar triangle. Let, then, a', b', c', A', B', C' represent the sides and angles of the polar triangle, and we shall have

Therefore
$$A=180^{\circ}-a', B=180^{\circ}-b', C=180^{\circ}-c', a=180^{\circ}-A', b=180^{\circ}-B', c=180^{\circ}-C'$$

$$\sin \frac{1}{2}A=\sin (90^{\circ}-\frac{1}{2}a')=\cos \frac{1}{2}a', \cos \frac{1}{2}A=\cos (90^{\circ}-\frac{1}{2}a')=\sin \frac{1}{2}a',$$

sin.
$$b=\sin(180^{\circ}-B')=\sin B'$$
,
sin. $c=\sin(180^{\circ}-C')=\sin C'$.

Also, it we put S'=half the sum of the angles of the polar triangle, we shall have

$$a+b+c=540^{\circ}-(A'+B'+C'),$$
or $s=270^{\circ}-S',$
whence $\sin s=-\cos S',$
 $\sin (s-a)=\sin [90^{\circ}-(S'-A')]=\cos (S'-A')$
 $\sin (s-b)=\cos (S'-B'),$
 $\sin (s-c)=\cos (S'-C').$

By substituting these values in formula (5), Art. 226, and omitting all the accents, since the equations are applicable to any triangle, we obtain

$$\cos \frac{1}{2}a = R\sqrt{\frac{\cos (S-B)\cos (S-C)}{\sin B \sin C}};$$
 (6)

and formula (4) becomes

$$\sin \frac{1}{2}a = R\sqrt{\frac{-\cos S \cos (S-A)}{\sin B \sin C}},$$
 (7)

which formulæ enable us to compute the sides of a triangle when the three angles are known; and this method may be preferred to that of Art. 224.

In a similar manner, by means of the polar triangle, we derive from formula (1), Art. 225, the equation

$$R^2 \cos A = \cos a \sin B \sin C - R \cos B \cos C$$
; (8)

that is, the square of radius multiplied by the cosine of either angle of a spherical triangle, is equal to the product of the sines of the two other angles into the cosine of their included side, minus radius into the product of their cosines.

Ex. 1. In a spherical triangle ABC, there are given $A=130^{\circ}~30',~B=30^{\circ}~50',~and~C=32^{\circ}~5'.$ Required the three sides.

Here half the sum of the angles is 96° 42 30"==S.

Also,
$$S-A=-33^{\circ} 47' 30''$$
, $S-B=65^{\circ} 52' 30''$, $S-C=64^{\circ} 37' 30''$

Using formula (6), we have

log. cos. (S-B),
$$65^{\circ}$$
 $52'$ $30''$. 9.611435
log. cos. (S-C), 64° $37'$ $30''$. 9.631992
-log. sin. B; 30° 50' comp. 0.290270
-log. sin. C, 32° 5' comp. 0.274781
Sum 19.808478
log. cos. $\frac{1}{2}a$, 36° 40' 1" 9.904239.

Hence the side $a=73^{\circ} 20' 2''$.

The remaining sides may be found by Theorem III., or by formulas similar to formula (6).

cos.
$$\frac{1}{2}b = R\sqrt{\frac{\cos. (S-A)\cos. (S-C)}{\sin. A \sin. C}}$$
,
cos. $\frac{1}{2}c = R\sqrt{\frac{\cos. (S-A)\cos. (S-B)}{\sin. A \sin. B}}$.

We thus find the side $b=40^{\circ} 13^{\circ} 12''$, and $c=42^{\circ} 0' 12''$.

Ex. 2. In the spherical triangle ABC, the angle $A=129^{\circ}$ 30', $B=54^{\circ}$ 35', and $C=63^{\circ}$ 5'. Required the three sides.

Ans.
$$\begin{cases} a = 120^{\circ} 57' & 5''. \\ b = 64^{\circ} 55' 37'' \\ c = 82^{\circ} 19' & 0''. \end{cases}$$

(228.) Formula (1), Art. 225, will also furnish a new test for removing the ambiguity of the solution in Case I. of oblique angled triangles. For we have

$$\cos. A = \frac{R^2 \cos. a - R \cos. b \cos. c}{\sin. b \sin. c}.$$

Now if cos. a is greater than cos. b, we shall have $R^2 \cos a > R \cos b \cos c$,

or the sign of the second member of the equation will be the same as that of $\cos a$, since the denominator is necessarily positive, and $\cos c$ is less than radius. Hence $\cos A$ and $\cos a$ will have the same sign; or A and a will be of the same species when $\cos a > \cos b$, or $\sin a < \sin b$; that is,

If the sine of the side opposite to the required angle is less than the sine of the other given side, there will be but one triangle.

But if cos. a is less than cos. b, then such a value may be given to c as to render

$R^2 \cos a < R \cos b \cos c$,

or the sign of the second member of the equation will depend upon the value of $\cos c$; that is, c may be taken so as to render \cos . A either positive or negative. Hence

If the sine of the side opposite to the required angle is greater than the sine of the other given side, there will be two triangles which fulfill the given conditions.

(229.) Formula (8), Art. 227, will furnish a test for removing the ambiguity in Case II. of oblique-angled triangles. For we have

$$\cos a = \frac{R^2 \cos A + R \cos B \cos C}{\sin B \sin C};$$

trom which it follows, as in the preceding article, that if \cos . A is greater than \cos . B, A and a will be of the same species. But if \cos . A is less than \cos . B, then such values may be given to C as to render \cos . a either positive or negative. Hence

If the sine of the angle opposite to the required side is less than the sine of the other given angle, there will be but one triangle;

But, if the sine of the angle opposite to the required side is greater than the sine of the other given angle, there will be two triangles which fulfill the given conditions.

SAILING ON AN ARC OF A GREAT CIRCLE.

(230.) It is demonstrated in Geom., Prop. 3, B. IX., that the shortest path from one point to another on the surface of a sphere is the arc of a great circle which joins the two given points. Hence, if it is desired to sail from one port to another by the shortest route, it is necessary to follow an arc of a great circle, and this arc generally does not coincide with a rhumb line

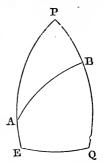
The bearing and distance from one place to another on the arc of a great circle may be computed from the latitudes and longitudes of the places by means of Spherical Trigonometry

Thus, let P be the pole of the earth, EQ a part of the equator, and A and B the two given places comprehended between the meridians PE and PQ. Then PA is the complement of the latitude of A, PB is the complement of the latitude of B₁

and the angle P is measured by the arc EQ, which is the

difference of longitude between the two places. Hence, in the triangle ABP, we have given two sides AP, BP, and the included angle P, from which we may compute the side AB, and the angles A and B, according to Case III. of oblique-angled triangles.

Ex. 1. Required the course and distance A from Nantucket Shoals, in latitude 41° 4′ N., longitude 69° 55′ W., to Cape Clear, in E Q latitude 51° 26′ N., longitude 9° 29′ W., on the arc of a great



circle. Here we have given

the angle $P=69^{\circ} 55' - 9^{\circ} 29' = 60^{\circ} 26'$;

the side PA=90° -41° 4'=48° 56'; the side PB=90° -51° 26'=38° 34'.

Then cot. PB: cos. P:: R: tan. PD=21° 28' 35".

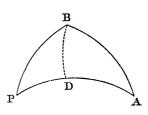
Whence AD=27° 27′ 25″.

Also sin. AD: sin. PD::tan. P: tan. A = 54° 27′ 21, and sin. A: sin. PB::sin. P: sin. AB=41° 47′ 28′.

41° 47′ 28″ is equal to 2507.47 nautical miles.

Hence the course from Nantucket Shoals to Cape Clear is N. 54° 27' E., and the distance is 2507.47 miles.

According to Mercator's sailing, the course on a rhumb-line, found on page 152, is N. 76° E., and the distance 2572.9 miles. Hence the dis-



tance on an arc of a great circle is 65.4 miles less than on a rhumb-line, and the former course is $21\frac{1}{2}$ degrees more northerly than the latter.

While sailing on a rhumb-line the course of a ship remains always the same, but while sailing on an arc of a great circle the course is continually changing. The preceding course is that with which the ship starts from Nantucket, and a new computation of the course should be made every day or two; or t might be more convenient to compute beforehand the position of the points in which the great circle intersects the meridians

for every five degrees of longitude, and the ship might be steered upon a direct course for these points successively.

Ex. 2. Required the course and distance from Nantucket Shoals to Gibraltar, in latitude 36° 6′ N., longitude 5° 20 w., on the shortest route.

Ans. The course is N. 73° 29′ E Distance 2974.1 miles.

Ex. 3. Required the course and distance from Sandy Hook, in latitude 40° 28′ N., longitude 74° 1′ W., to Madeira, in latitude 32° 38′ N., longitude 16° 55′ W., on the shortest route.

Ans. The course is N. 80° 53′ E. Distance 2744.1 miles.

Ex. 4. Required the course and distance from Sandy Hook to St. Jago, in latitude 14° 54′ N., longitude 23° 30′ W., on the shortest route.

Ans. The course is S. 74° 46′ E. Distance 3037.6 miles.

Ex. 5. Required the course and distance from Sandy Hook to the Cape of Good Hope, in latitude 34° 22′ S., longitude 18° 30′ E., on the shortest route.

Ans. The course is S. 63° 48′ E Distance 6792 miles.

EXAMPLES FOR PRACTICE.

PLANE TRIGONOMETRY.

Prob. 1. Given the three sides of a triangle, 627, 718.9, and 1140, to find the angles.

Ans. 29° 44′ 2″, 34° 39′ 26″, and 115° 36′ 32″.

Prob.~2. In the triangle ABC, the angle A is given 89° 45′ 43″, the side AB 654, and the side AC 460, to find the remaining parts.

Ans. BC=798; the angle B=35° 12′ 1″, and the angle C=55° 2′ 16″.

Prob. 3. In the triangle ABC, the angle A is given 56° 12′ 45″, the side BC 2597.84, and the side AC 3084.33, to find the remaining parts.

Ans. B=80° 39′ 40″, C=43° 7′ 35″, c=2136.8; or, B=99 20 20, C=24 26 55, c=1293.8.

Prob. 4. In the triangle ABC, the angle A is given 44° 13′ 24'', the angle B 55° 59′ 58′′, and the side AC 368, to find the remaining parts.

Ans. $C = 79^{\circ} 46' 38''$, AB = 436.844, and BC = 309.595.

Prob. 5. In a right-angled triangle, if the sum of the hypothenuse and base be 3409 feet, and the angle at the base 53° 12' 14'', what is the perpendicular?

Ans. 1707.2 feet.

Prob. 6. In a right-angled triangle, if the difference of the hypothenuse and base be 169.9 yards, and the angle at the base 42° 36' 12'', what is the length of the perpendicular?

Ans. 435.732 yards.

Prob. 7. In a right-angled triangle, if the sum of the base and perpendicular be 123.7 feet, and the angle at the base 58° 19′ 32″, what is the length of the hypothenuse?

Ans. 89.889 feet.

Prob. 8. In a right-angled triangle, if the difference of the base and perpendicular be 12 yards, and the angle at the base 38° 1′ 8″, what is the length of the hypothenuse?

Ans. 69.81 yards.

Prob. 9. A May-pole, 50 feet 11 inches high, at a certain time will east a shadow 98 feet 6 inches long; what, then, is the breadth of a river which runs within 20 feet 6 inches of the foot of a steeple 300 feet 8 inches high, if the steeple at the same time throws its shadow 30 feet 9 inches beyond the stream?

Ans. 530 feet 5 inches.

Prob. 10. A ladder 40 feet long may be so placed that it shall reach a window 33 feet from the ground on one side of the street, and by turning it over, without moving the foot out of its place, it will do the same by a window 21 feet high on the other side. Required the breadth of the street.

Ans. 56.649 feet.

Prob. 11. A May-pole, whose top was broken off by a blast of wind, struck the ground at the distance of 15 feet from the foot of the pole; what was the height of the whole May-pole, supposing the length of the broken piece to be 39 feet?

Ans. 75 feet.

Prob. 12. How must three trees, A, B, C, be planted, so that the angle at A may be double the angle at B, the angle at B double the angle at C, and a line of 400 yards may just go round them?

Ans. AB = 79.225, AC = 142.758, and BC = 178.017 yards.

Prob. 13. The town B is half way between the towns A and C, and the towns B, C, and D are equidistant from each other. What is the ratio of the distance AB to AD?

Ans. As unity to $\sqrt{3}$.

Prob. 14. There are two columns left standing upright in the ruins of Persepolis; the one is 66 feet above the plain, and the other 48. In a straight line between them stands an ancient statue, the head of which is 100 feet from the summit of the higher, and 84 feet from the top of the lower column, the base of which measures just 74 feet to the centre of the figure's base. Required the distance between the tops of the two columns.

Ans. 156.68 feet.

Prob. 15. Prove that tang.
$$(45^{\circ}-b) = \frac{1-\tan b}{1+\tan b}$$

Prob. 16. One angle of a triangle is 45°, and the perpendicular from this angle upon the opposite base divides the base into two parts, which are in the ratio of 2 to 3. What are the

parts into which the vertical angle is divided by this perpendicular?

Ans. 18° 26′ 6″ and 26° 33′ 54″.

Prob. 17. Prove that $\sin 3b = 3 \sin b - 4 \sin^3 b$.

Prob. 18. One side of a triangle is 25, another is 22, and the angle contained by these two sides is one half of the angle opposite the side 25. What is the value of the included angle?

Ans. 39° 58′ 51″.

Prob. 19. One side of a triangle is 25, another is 22, and the angle contained by these two sides is one half of the angle opposite the side 22. What is the value of the included angle?

Ans. 30° 46′ 38″.

Prob. 20. Two sides of a triangle are in the ratio of 11 to 9, and the opposite angles have the ratio of 3 to 1. What are those angles?

Ans. The sine of the smaller of the two angles is $\frac{2}{3}$, and of the greater $\frac{22}{27}$; the angles are 41° 48′ 37″ and 125° 25′ 51″.

Prob. 21. One side of a triangle is 15, and the difference of the two other sides is 6; also, the angle included between the first side and the greater of the two others is 60°. What is the length of the side opposite to this angle?

Ans. 57.

Prob. 22. One side of a triangle is 15, and the difference of the two other sides is 6; also, the angle opposite to the greater of the two latter sides is 60°. What is the length of said side?

Ans. 13.

Prob. 23. One side of a triangle is 15, and the opposite angle is 60°; also, the difference of the two other sides is 6 What are the lengths of those sides?

Ans. 11.0712 and 17.0712.

Prob. 24. The perimeter of a triangle is 100; the perpendicular let fall from one of the angles upon the opposite base is 30, and the angle at one and of this base is 50°. What is the length of the base?

Ans. 30.388

MENSURATION OF SURFACES AND SOLIDS.

Prob. 1. The base of a triangle is 20 feet, and its altitude 18 feet. It is required to draw a line parallel to the base so as to cut off a trapezoid containing 80 square feet. What is the length of the line of section, and its distance from the base of the triangle?

Ans. Length 14.907 feet; distance from base 4.584 feet.

Prob. 2. The base of a triangle is 20 feet, one angle at the base is 63° 26′, and the other angle at the base is 56° 19′. It is required to draw a line parallel to the base, so as to cut off a trapezoid containing 109 square feet. What is the length of the line of section, and its distance from the base of the triangle?

Ans. Length 12.070 feet; distance from base 6.797 feet.

Prob. 3. In a perpendicular section of a ditch, the breadth at the top is 26 feet, the slopes of the sides are each 45°, and the area 140 square feet. Required the breadth at bottom and the depth of the ditch.

Ans. Breadth 10.77 feet; depth 7.615 feet.

Prob. 4. The altitude of a trapezoid is 23 feet; the two parallel sides are 76 and 36 feet; it is required to draw a line parallel to the parallel sides, so as to cut off from the smaller end of the trapezoid a part containing 560 square feet. What is the length of the line of section, and its distance from the shorter of the two parallel sides?

Ans. Length 56.954 feet; distance 12.048 feet.

Prob. 5. From the greater end of a trapezoidal field whose parallel ends and breadth measure 12, 8, and $10\frac{1}{2}$ chains respectively, it is required to cut off an area of six acres by a fence parallel to the parallel sides of the field. What is the length of the fence, and its distance from the greater side.

Ans. Length of fence 9.914 chains; distance from greater side 5.476 chains.

Prob. 6. There are three circles whose radii are 20, 28, and 29 inches respectively. Required the radius of a fourth circle, whose area is equal to the sum of the areas of the other three.

Ans. 45 inches.

Prob. 7. In constructing a rail-road, the pathway of which

is 24 feet broad, it is necessary to make a cutting 40 feet in depth; what must be the breadth of the cutting at top, supposing the slopes of the sides to be 65°?

Ans. 61.305 feet.

Prob. 8. The sides of a quadrilateral field are 690 yards, 467 yards, 359 yards, and 428 yards; also, the angle contained between the first and second sides is 57° 30′, and the angle between the third and fourth sides 122° 30′. Required the area of the field.

Ans. 200677.2 square yards.

Prob. 9. There are two regular pentagons, one inscribed in a circle, and the other described about it; and the difference of the areas of the pentagons is 100 square inches. Required the radius of the circle.

. Ans. 8.926 inches.

Prob. 10. What is the length of a chord cutting off one third part of a circle, whose diameter is 289 feet.

Ans. 278.67 feet.

Prob. 11. The area of a triangle is 1012; the length of the side a is to that of b as 4 to 3, and c is to b as 3 to 2. Required the length of the sides.

Ans. a=52.470, b=39.353, c=59.029.

Prob. 12. The area of a triangle is 144, the base is 24, and one of the angles at the base is 30°. Required the other sides of the triangle.

Ans. 24 and 12.4233.

Prob. 13. Seven men bought a grinding-stone of 60 inches diameter, each paying one seventh part of the expense. What part of the diameter must each grind down for his share?

Ans. The 1st, 4.4508 inches; 2d, 4.8400 inches; 3d, 5.3535 inches; 4th, 6.0765 inches; 5th, 7.2079 inches; 6th, 9.3935 inches; 7th, 22.6778 inches.

Prob. 14. The area of an equilateral triangle is 17 square feet and 83 square inches. What is the length of each side?

Ans. 76.45 inches.

Prob. 15. The parallel sides of a trapezoid are 20 and 12 feet, and the other sides are 15 and 17 feet. Required the area of the trapezoid.

Ans. 240 square feet.

Prob. 16. How many square yards of canvas are required to make a conical tent which is 20 feet in diameter and 12 feet high?

Ans. 54.526 square yards.

Prob. 17. The circumference of an hexagonal pillar is 7 feet, and the height 11 feet 2 inches. Required the solid contents of the pillar.

Ans. 39.488 cubic feet.

Prob. 18. The base of the great pyramid of Egypt is a square whose side measures 746 feet, and the altitude of the pyramid is 450 feet. Required the volume of the pyramid.

Ans. 83,477,400 cubic feet.

Prob. 19. A side of the base of a frustum of a square pyramid is 25 inches, a side of the top is 9 inches, and the height is 20 feet. Required the volume of the frustum.

Ans. 43.102 cubic feet.

Prob. 20. Three persons, having bought a sugar-loaf, would divide it equally among them by sections parallel to the base. It is required to find the altitude of each person's share, supposing the loaf to be a cone whose height is 20 inches.

Ans. 13.8672, 3.6044, and 2.5284 inches.

Prob. 21. If a cubical foot of brass were to be drawn into wire of one thirtieth of an inch in diameter, it is required to determine the length of the said wire, allowing no loss in the metal.

Ans. 55003.94 yards; or 31 miles 443.94 yards.

Prob. 22. How high above the surface of the earth must a person be raised to see one third of its surface?

Ans. The height of its diameter.

Prob. 23. If a heavy sphere, whose diameter is 4 inches, be let fall into a conical glass full of water, whose diameter is 5, and altitude 6 inches, it is required to determine how much water will run over.

Ans. 26.272 cubic inches.

Prob. 24. The capacity of a cylinder is a cubic feet, and its convex surface is b square feet. Required the dimensions of the cylinder.

Ans. Radius of base $=\frac{2a}{b}$, and altitude $=\frac{b^2}{4a\pi}$.

Prob. 25. A triangular pyramid, the sides of whose base are

13, 14, and 15 inches respectively, and whose altitude is 16 inches, is cut, at the distance of 2 inches from the vertex, by a plane parallel to the base. Required the volume of the frustum of the pyramid.

Ans. 447.125 cubic inches.

Prob. 26. The altitude of a cone is 10 inches, and the radius of its base is 5 inches. At what distance from the base must a plane pass parallel to the base, so as to cut off a frustum whose capacity is 20 cubic inches?

Ans. 0.2614 inches.

SURVEYING.

Prob. 1. The angle of elevation of a spire I found to be 39° 27′, and going directly from it 225 feet on a horizontal plane, I found the angle to be only 24° 38′. What is the height of the spire, and the distance from its base to the second station?

Ans. Height 238.02 feet, distance 508.18 feet.

Prob. 2. Wishing to know the distance of an inaccessible object, I measured a horizontal base-line 1328 feet, and found the angles at the ends of this line were 84° 23′ and 43° 19′. What was the distance of the object from each end of the base-line?

Ans. 1151.44 feet, and 1670.35 feet.

Prob. 3. Wishing to know the distance between two inaccessible objects, C and D, I measured a base-line, AB, 3784 feet, and found the angle BAD=47° 32′, the angle DAC=39° 53′, the angle ABC=46° 34′, and the angle CBD=38° 1′. What is the distance from C to D?

Ans. 3257.36 feet.

Prob. 4. Suppose a light-house built on the top of a rock; the distance between the place of observation and that part of the rock which is level with the eye, and directly under the building, is 1860 feet; the distance from the top of the rock to the place of observation is 2538 feet, and from the top of the building 2550 feet. Required the height of the light-house.

Ans. 17 feet 7 inches.

Prob. 5. At 85 feet distance from the bottom of a tower, standing on a horizontal plane, the angle of its elevation was found to be 52° 30′. Required the altitude of the tower.

Ans. $110\frac{1}{2}$ feet.

Prob. 6. At a certain station, the angle of elevation of an inaccessible tower was 26° 30′; but, measuring 225 feet in a direct line toward it, the angle was then found to be 51° 30′. Required the height of the tower, and its distance from the last station.

Ans. Height 186 feet, distance 147 feet.

Prob. 7. To find the distance of an inaccessible castle gate, I measured a line of 73 yards, and at each end of it took the angle of position of the object and the other end, and found the one to be 90°, and the other 61° 45′. Required the distance of the castle from each station.

Ans. 135.8 yards, and 154.2 yards.

Prob. 8. From the top of a tower 143 feet high, by the seaside, I observed that the angle of depression of a boat was 35°. What was its distance from the bottom of the tower?

Ans. 204.22 feet.

Prob. 9. I wanted to know the distance between two places, A and B, but could not meet with any station from whence I could see both objects. I measured a line CD=200 yards; from C the object A was visible, and from D the object B was visible, at each of which places I set up a pole. I also measured FC=200 yards, and DE=200 yards, and at F and E set up poles. I then measured the angle AFC=83°, ACF=54° 31′, ACD=53° 30′, BDC=156° 25′, BDE=54° 30′, and BED=88° 30′. Required the distance from A to B.

Ans. 345.5 yards.

Prob. 10. From the top of a light-house, the angle of depression of a ship at anchor was 3° 38′, and at the bottom of the light-house the angle of depression was 2° 43′. Required the horizontal distance of the vessel, and the height of the promontory above the level of the sea, the light-house being 85 feet high.

Ans. Distance 5296.4 feet, height 251.3 feet.

Prob. 11. An observer, seeing a cloud in the west, measured its angle of elevation, and found it to be 64°. A second observer, situated half a mile due east from the first station, and on the same horizontal plane, found its angle of elevation at the same moment of time to be only 35°. Required the perpendicular height of the cloud, and its distance from each observer.

Ans. Perpendicular height 935.75 yards, distances 1041.1 and 1631.4 yards.

Prob. 12. An observer, seeing a balloon in the north, measured its angle of elevation, and found it to be 36° 52′. A second observer, situated one mile due south from the first station, and on the same horizontal plane, found its angle of elevation at the same instant to be only 30° 58′. Required the perpendicular height of the balloon, and its distance from each observer.

Ans. Perpendicular height 3.003 miles, distances 5.006 and 5.837 miles.

Prob. 13. From a window near the bottom of a house which seemed to be on a level with the bottom of a steeple, I found the angle of elevation of the top of the steeple to be 40°; then from another window, 21 feet directly above the former, the like angle was 37° 30′. What was the height and distance of the steeple?

Ans. Height 245.51 feet, distance 292.59 feet.

Prob. 14. Wanting to know my distance from an inaccessible object, P, on the other side of a river, and having no instrument for taking angles, but a chain for measuring distances, from each of two stations, A and B, which were taken at 300 yards asunder, I measured in a direct line from the object P 60 yards, viz., AC and BD each equal to 60 yards; also, the diagonal AD measured 330 yards, and the diagonal BC 336 yards. What was the distance of the object P from each station A and B?

Ans. AP=321.76 yards, BP=300.09 yards.

Prob. 15. Having at a certain (unknown) distance taken the angle of elevation of a steeple, I advanced 60 yards nearer on level ground, and then observed the angle of elevation to be the complement of the former. Advancing 20 yards still nearer, the angle of elevation now appeared to be just double of the first. Required the altitude of the steeple.

Ans. 74.162 yards.

B C

Prob. 16. In a garrison there are three remarkable objects, A, B, C, whose distances from each other are known to be, AB 213, AC 424, and BC 262 yards. I am desirous of knowing my position and distance at a station, P, from which I observed the angle APB, 13° 30′, and the angle CPB, 29° 50′.

Ans. AP = 605.7122, BP = 429.6814, CP = 524.2365.

Prob. 17. Supposing the object B to be on the opposite side of the line AC (see figure to Prob. 16), and that the distances of the objects were, AB=8 miles, AC=12 miles, and BC= $7\frac{1}{5}$ miles; also, the angle APB=19°, and the angle CPB=25°. It is required to find the distances AP, BP, and CP.

Ans. AP = 9.4711 miles, BP = 16.3369 miles, CP = 16.8485 miles.

Prob. 18. In a pentangular field, beginning with the south side, and measuring round toward the east, the first or south side was 27.35 chains, the second 31.15 chains, the third 23.70 chains, the fourth 29.25 chains, and the fifth 22.20 chains; also, the diagonal from the first angle to the third was 38.00 chains, and that from the third to the fifth was 40.10 chains. Required the area of the field.

Ans. 117 A. 2 R. 39 P.

Prob. 19. The following are the dimensions of a five-sided field, ABCDE: the side AB=19.40 chains, and the angle B 110° 30′; the side BC=15.55 chains, and the angle C 117° 45′; the side CD=21.25 chains, and the angle D 91° 20′; and the side DE=27.41 chains. Required the area of the field.

Ans. 66 A. 2 R. 24 P.

Prob. 20. From a station, H, near the middle of a field, ABCDEF, from which I could see all the angles, I measured the distances to the several corners, and measured the angles formed at H by those distances, as follows:

	tances	Angles.			
AH, 4	3.15	chains;	AHB,	60°	30′.
BH, 2	9.82	"	BHC,	47	40
CH, 3	5.61	"	CHD,	49	50
DH, 5	0.10	"	DHE,	57	10
EH, 4	6.18	"	EHF,	64	15
FH, 3	6.06	66	FHA,	80	35

Required the area of the field.

Ans. 412 A. 1 R. 17 P.

NAVIGATION.

Prob. 1. From a ship at sea I observed a point of land to bear east by south, and, after sailing northeast 12 miles, I ob-

served again, and found its bearing to be southeast by east. How far was the last observation made from the point of land?

Ans. 26.07 miles.

Prob. 2. If a ship in latitude 50° N., sails 52 miles in the direction southwest by south, what latitude has she arrived in, and how much farther to the west?

Ans. Latitude 49° 16.'8 N.; west, 28.9 miles.

Prob. 3. Two ships sail from the same port; the one sails east-northeast 85 miles, the other sails east by south till the first ship bears northwest by west. What is the distance of the second ship from the port, and also from the first ship?

Ans. From the port, 184.7 miles; from the first ship, 123.4 miles.

Prob. 4. Two ports lie east and west of each other; a ship sails from each, namely, the ship from the west port sails northeast 89 leagues, and the other sails 80 leagues, when she meets the former. Required the latter ship's course, and the distance between the two ports.

Ans. Course, N. 38° 8' W.; distance, 112.3 leagues.

Prob. 5. Two ships sail from a certain port; the one sails south by east 45 leagues, and the other south-southwest 64 leagues. What is the bearing and distance of the first ship from the second?

Ans. Bearing, N. 65° 44′ E.; distance, 36.5 leagues.

- Prob. 6. A ship sailing northwest, two islands appear in sight, of which the one bears north, and the other west-northwest; but, after sailing 20 leagues, the former bears northeast, and the latter west by south. What is the distance asunder of the two islands?

 Ans. 32.38 leagues.
- *Prob.* 7. To a vessel sailing on a certain course, a headland was observed to bear due west; four hours after which it was seen at west-southwest; and six hours after this, the vessel continuing to run at the same rate, its bearing was found to be south-southwest. What was the vessel's course at the time?

Ans. N. 42° 35′ W.

Prob. 8. Two ships of war, intending to cannonade a fort, are, by the shallowness of the water, kept so far from it that they suspect their guns can not reach it with effect. In order, therefore, to measure the distance, they separate from each other 500

rods; then each ship observes the angle which the other ship and the fort subtend, which angles are 38° 16′ and 37° 9′. What, then, is the distance between each ship and the fort?

Ans. 312 rods and 320 rods.

Prob. 9. A ship from the latitude 42° 18′ N., sails southwest by south until her latitude is 40° 18′ N. What direct distance has she sailed, and how many miles has she sailed to the westward?

Ans. Distance run 144.3 miles, and has sailed to westward 80.2 miles.

Prob. 10. A ship having run due east for three days, at the rate of eight knots an hour, finds she has altered her longitude 15 degrees. What parallel of latitude did she sail on?

Ans. Latitude 50° 12′.

Prob. 11. A ship in latitude 43° 30′ N., and longitude 44° W., sails southeasterly 532 miles, until her departure from the meridian is 420 miles. Required the course steered, and the latitude and longitude of the ship.

Ans. Course S. 52° 8′ E., latitude 38° 3.′5 N., longitude 34° 45′ W.

Prob. 12. A ship from latitude 43° 20′ N., and longitude 52° W., sails E.S.E. until her departure is 745 miles. Required the distance sailed, and the latitude and longitude of the ship.

Ans. Distance 806.4 miles, latitude 38° 11.′5 N., longitude 35° 36′ W.

Prob. 13. If the height of the mountain called the Peak of Teneriffe be 4 miles, and the angle taken at the top of it, as formed between a plumb-line and a line conceived to touch the earth in the horizon, or farthest visible point, be 87° 25′ 55″, it is required from hence to determine the magnitude of the whole earth, and the utmost distance that can be seen on its surface from the top of the mountain, supposing the earth to be a perfect sphere.

Ans. Distance 178.458 miles, diameter 7957.793 miles.

Prob. 14. Required the course and distance from St. Jago, one of the Cape Verd islands, in latitude 14° 56′ N., to the island of St. Helena, in latitude 15° 45′ S., their difference of longitude being 30° 12′.

Ans. Course S. 44° 12' E., distance 2567.8 miles.

Prob. 15. A ship from the latitude of 49° 57′ N., and longitude of 30° W., sails S. 39° W., till she arrives in the latitude of 45° 31′ N. Required the distance run, and the longitude of the ship.

Ans. Distance 342.3 miles, longitude of ship 35° 21′ W.

Prob. 16. Find the bearing and distance from San Francisco, latitude 37° 48′ N., longitude 122° 28′ W., to Jeddo, latitude 35° 40′ N., longitude 139° 40′ E., by Mercator's sailing.

Ans. Course S. 88° 26' W., distance 4705 miles.

Prob. 17. Find the bearing and distance from San Francisco to Batavia in Java, latitude 6° 9′ S., longitude 106° 53′ E., by Mercator's sailing.

Ans. Course S. 70° 12′ W., distance 7783 miles.

Prob. 18. Find the bearing and distance from San Francisco to Port Jackson, latitude 33° 51' S., longitude 151° 14' E., by Mercator's sailing.

Ans. Course S. 48° 18' W., distance 6462 miles.

Prob.~19. Find the bearing and distance from San Francisco to Otaheite, latitude 17° 29′ S., longitude 149° 29′ W., by Mercator's sailing.

Ans. Course S. 24° 44′ W., distance 3652 miles.

Prob. 20. Find the bearing and distance from San Francisco to Valparaiso, latitude 33° 2' S., longitude 71° 41' W., by Mercator's sailing.

Ans. Course S. 33° 47′ E., distance 5354 miles.

SPHERICAL TRIGONOMETRY.

Prob. 1. In the right-angled spherical triangle ABC, there are given the angle C 23° 27′ 42″, and the side b 10° 39′ 40″. Required the angle B, and the sides a and c.

Ans.
$$\begin{cases} a = 11^{\circ} 35' 49''. \\ c = 4^{\circ} 35' 26''. \\ B = 66^{\circ} 58' 1''. \end{cases}$$

Prob. 2. In the spherical triangle ABC, the side BC=90°, the side AB=32° 57′ 6″, and the side AC=66° 32′. Required the angles.

Ans.
$$\begin{cases} A = 132^{\circ} & 2' 44''. \\ B = 42^{\circ} 56' 12''. \\ C = 23^{\circ} 49' 26''. \end{cases}$$

Prob. 3. In the right-angled spherical triangle ABC, there are given the angle $B=47^{\circ}$ 54′ 20″, and the angle $C=61^{\circ}$ 50′ 29″. Required the sides.

Ans.
$$\begin{cases} a = 61^{\circ} & 4' \ 56'' \\ b = 40^{\circ} \ 30' \ 20'' \\ c = 50^{\circ} \ 30' \ 30'' \end{cases}$$

Prob. 4. In the spherical triangle ABC, the side AC=90°, the side AB=115° 9′, and the angle B=101° 40′. Required the remaining parts.

Ans.
$$\begin{cases} BC = 113^{\circ} \ 18' \ 7''. \\ A = 115^{\circ} \ 54' \ 46''. \\ C = 117^{\circ} \ 33' \ 49''. \end{cases}$$

Prob. 5. In the spherical triangle ABC, the angle $\Lambda=130^{\circ}$ 5′ 22″, the angle $C=36^{\circ}$ 45′ 28″, and the side $AC=44^{\circ}$ 13′ 45″. Required the remaining parts.

Ans.
$$\begin{cases} AB = 51^{\circ} & 6' \ 12''. \\ BC = 84^{\circ} \ 14' \ 29''. \\ B = 32^{\circ} \ 26' & 6''. \end{cases}$$

Prob. 6. In the spherical triangle ABC, the angle A=33° 15′ 7″, B=31° 34′ 38″, and C=161° 25′ 17″. Required the sides.

Ans.
$$\begin{cases} a = 80^{\circ} & 5' & 4''. \\ b = 70^{\circ} & 10' & 30''. \\ c = 145^{\circ} & 5' & 2''. \end{cases}$$

Prob. 7. In the spherical triangle ABC, the side AB=112° 22' 58'', AC= 52° 39' 4'', and BC= 89° 16' 53''. Required the angles.

Ans.
$$\begin{cases} A = 70^{\circ} 39' 0''. \\ B = 48^{\circ} 36' 0''. \\ C = 119^{\circ} 15' 0''. \end{cases}$$

Prob. 8. In the spherical triangle ABC, the side AB=76° 35′ 36″, AC=50° 10′ 30″, and the angle A=34° 15′ 3″. Required the remaining parts.

Ans.
$$\begin{cases} B = 42^{\circ} 15' 13''. \\ C = 121^{\circ} 36' 20''. \\ BC = 40^{\circ} 0' 10''. \end{cases}$$

Prob. 9. The latitudes of the observatories of Paris and Pekin are 48° 50′ 14″ N. and 39° 54′ 13″ N., and their difference of longitude is 114° 7′ 30″. What is their distance?

Ans. 73° 56′ 40″.

Prob. 10. Required the course and distance from New York, latitude 40° 43′ N., longitude 74° 0′ W., to San Francisco, latitude 37° 48′ N., longitude 122° 28′ W., on the shortest route.

Ans. The course is N. 78° 16′ W.

Distance, 2229.8 nautical miles.

Prob. 11. Required the course and distance from San Francisco, latitude 37° 48′ N., longitude 122° 28′ W., to Jeddo, in latitude 35° 40′ N., longitude 139° 40′ E., on the shortest route.

Ans. The course is N. 56° 41′ W.

Distance, 4461.9 nautical miles.

Prob. 12. Required the course and distance from San Francisco to Batavia in Java, latitude 6° 9′ S., longitude 106° 53′ E., on the shortest route.

Ans. The course is N. 67° 30′ W. Distance, 7516 nautical miles.

Prob. 13. Required the course and distance from San Francisco to Port Jackson, latitude 33° 51′ S., longitude 151° 14′ E., on the shortest route.

Ans. The course is S. 59° 50′ W. Distance, 6444 nautical miles.

Prob. 14. Required the course and distance from San Francisco to Otaheite, latitude 17° 29′ S., longitude 149° 29′ W., on the shortest route.

Ans. The course is S. 29° 45′ W. Distance, 3650.3 nautical miles.

Prob. 15. Required the course and distance from San Francisco to Valparaiso, latitude 33° 2′ S., longitude 71° 41 W., or the shortest route.

Ans. The course is S. 39° 22′ E. Distance, 5108.5 nautical miles.

Prob. 16. Suppose two ports, one in north latitude 30°, and the other in north latitude 40°, the difference of longitude between them being 50°. Required the bearing and distance from each of these ports to an island that lies in south latitude 18°, and which is equally distant from both of the said ports.

Ans. Bearing from first port, S. 40° 52′ 9″ E. Bearing from second port, S. 15 ′ 9 47 W.

The distance, 59° 23′ 19″ = 3563.3 nautical miles.







TABLES

OF

LOGARITHMS OF NUMBERS

AND OF

SINES AND TANGENTS

FOR EVERY

TEN SECONDS OF THE QUADRANT.

WITH OTHER USEFUL TABLES.

BY ELIAS LOOMIS, LL.D.,

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CONTENTS.

	Cago
EXPLANATIC VOF THE TABLES	
TABLE OF LOGARITHMS OF NUMBERS	. 1
LOGARITHMIC SINES AND TANGENTS	21
NATURAL SINES AND TANGENTS	. 116
NATURAL SECANTS	134
LENGTHS OF CIRCULAR ARCS	135
TRAVERSE TABLE	136
MERIDIONAL PARTS	
CORRECTIONS TO MIDDLE LATITUDE	
LOGARITHMS FOR COMPOUND INTEREST, ETC	. 150

PREFACE.

The accompanying tables were designed to afford the means of performing trigonometrical computations with facility and precision. The tables chiefly used in this country for purposes of education extend to six decimal places, like those in the present collection; but the precision which they are designed to furnish is only attained by a serious expenditure of labor. In the Table of Logarithms of Numbers they do not furnish the correction for a fifth figure in the natural number, and the labor of computing this correction is such that I always prefer the use of Hutton's Tables, extending to seven places, even in computations to which six-place logarithms are abundantly competent. In the present collection, the correction for a fifth figure of the natural number is introduced at the bottom of each page, and the table is thus rendered nearly as useful as one of the common kind extending to 100,000. The whole has been carefully compared with standard authors, and nearly a dozen errors have thus been detected in the common tables.

The principal table in this collection is that of Logarithmic Sines and Tangents. The common tables in this country extend only to minutes, with differences to 100". If, in a trigonometrical computation, angles are only required to the nearest minute, tables to five places are quite sufficient; but if the computation is to be carried to seconds, these can only be obtained from the common tables by a great expenditure of time and labor. In the present collection, the sines and tangents are furnished to every ten seconds of the quadrant, and at the bottom of each page is given the correction for any number of seconds less than ten, so that the precision of seconds can be obtained with almost the same facility as that of minutes with the tables in common use. near the limits of the quadrant, by means of an auxiliary table, sines and tangents are readily obtained, even for a fraction of a second. method of arrangement of the sines and tangents was suggested by a table in Mackay's Longitude; but the errors of that table, amounting to several thousand, have been corrected by a careful comparison with the work of Ursinus. By comparison with the same standard, more than two hundred errors (chiefly in the final figures) have been detected in the tables in common use.

The Table of Natural Sines and Tangents is of less use than the logarithmic; nevertheless, it is often important for reference, particularly in analytical geometry and the calculus; and it is useful as a stepping-stone to assist the beginner in comprehending the nature of logarithmic

i v

sines and tangents. The Traverse Table commonly used in this country furnishes the latitude and departure to every quarter degree of the quad rant, for distances from 1 to 100, and occupies ninety pages. The accompanying table occupies but six pages, and yields ten times greater precision.

The Table of Meridional Parts extends to tenths of a mile, and grea care has been taken to insure its accuracy. For this purpose, I have compared all the similar tables within my reach, and among them have found two which appeared to have been computed independently. Be tween them there were detected 674 discrepancies in the final figures. These cases were all recomputed, and 78 errors were detected in the pest copy compared. It is probable that the numbers in this table are not in every instance true to the nearest tenth of a mile; but it is be lieved that the remaining errors are few in number, as well as minute This table is confidently pronounced more accurate than any similar one with which I have been able to compare it.

The Table of Corrections to Middle Latitude was computed entirely anew. The corresponding table in common use, which was originally computed by Workman, contains more than four hundred errors, several of them amounting to two minutes.

On the whole, it is believed that the accompanying tables will be found more convenient to the computer than any tables of six decimal places hitherto published in this country; and that they will be pronounced sufficiently extensive for all purposes of academic and collegize instruction, as well as for practical mechanics and surveyors.

EXPLANATION OF THE TABLES.

Table of Logarithms of Numbers, pp. 1-20.

LOGARITHMS are numbers contrived to diminish the labor of Multiplication and Division by substituting in their stead Addition and Subtraction. All numbers are regarded as powers of some one number, which is called the *base* of the system; and the exponent of that power of the base which is equal to a given number, is called the logarithm of that number.

The base of the common system of logarithms (called, from their inventor, Briggs' logarithms) is the number 10. Hence all numbers are to be regarded as powers of 10. Thus, since

$10^{\circ} = 1$,	0	is the	logarithm	of 1	ın Br	iggs'	system;
101=10,	1	44	"	10		"	66
10°=100,	2	66	"	100		66	66
$10^3 = 1000$,	3	66	"	1000		66	44
104=10,000,	4	66	44	10,000	' '	14	66
&c.,			&c.	,		&	cc.;

whence it appears that, in Briggs' system, the logarithm of every number between 1 and 10 is some number between 0 and 1, i. e., is a proper fraction. The logarithm of every number between 10 and 100 is some number between 1 and 2, i. e., is 1 plus a fraction. The logarithm of every number between 100 and 1000 is some number between 2 and 3, i. e., is 2 plus a fraction, and so on.

The preceding principles may be extended to fractions by means of negative exponents. Thus, since

$$10^{-1}$$
=0.1, —1 is the logarithm of 0.1 in Briggs' system 0^{-2} =0.01, —2 " 0.01 " " 0^{-3} =0.001, —3 " 0.001 " " 0^{-4} =0.0001, —4 " 0.0001 " " 0^{-4} =0.0001, —4 " &c., &c.

Hence it appears that the logarithm of every number between 1 and 0.1 is some number between 0 and -1, or may be represented by -1 plus a fraction; the logarithm of every number between 0.1 and .01 is some number between -1 and -2, or may be represented by -2 plus

a fraction; the logarithm of every number between .01 and .001 is some number between —2 and —3, or is equal to —3 plus a fraction, and so on.

The logarithms of most numbers, therefore, consist of an integer and a fraction. The integral part is called the *characteristic*, and may be known from the following

Rule.

The characteristic of the logarithm of a number greater than unity, is one less than the number of integral figures in the given number.

Thus the logarithm of 297 is 2 plus a fraction; that is, the characteristic of the logarithm of 297 is 2, which is one less than the number of integral figures. The characteristic of the logarithm of 5673.29 is 3; that of 73254.1 is 4, &c.

The characteristic of the logarithm of a decimal fraction is a negative number, and is equal to the number of places by which its first significant figure is removed from the place of units.

Thus the logarithm of .0046 is —3 plus a fraction; that is, the characteristic of the logarithm is —3, the first significant figure 4 being removed three places from units.

The accompanying table contains the logarithms of all numbers from 1 to 10,000 carried to 6 decimal places.

To find the Logarithm of any Number between 1 and 100.

Look on the first page of the table, along the column of numbers under N, for the given number, and against it, in the next column, will be found the logarithm, with its characteristic. Thus,

opposite 13 is 1.113943, which is the logarithm of 13; 65 is 1.812913, "65.

To find the Logarithm of any Number consisting of three Figures.

Look on one of the pages from 2 to 20, along the left-hand column narked N, for the given number, and against it, in the column headed 0, will be found the decimal part of its logarithm. To this the character stic must be prefixed, according to the rule already given. Thus

the logarithm of 347 will be found, from page 8, to be 2.540329;
" " 871 " " 18, " 2.940018.

As the first two figures of the decimal are the same for several successive numbers in the table, they are not repeated for each logarithm reparately, but are left to be supplied. Thus the decimal part of the ogarithm of 339 is .530200. The first two figures of the decimal remain he same up to 347; they are therefore omitted in the table, and are to be supplied.

To find the Logarithm of any Number consisting of four Figures. Find the three left-hand figures in the column marked N as before

and the fourth figure at the head of one of the other columns. Opposite to the first three figures, and in the column under the fourth figure, will be found four figures of the logarithm, to which two figures from the column headed 0 are to be prefixed, as in the former case. The characteristic must be supplied by the usual rule. Thus

the logarithm of 3456 is 3.538574;
" 8765 is 3.942752.

In several of the columns headed 1, 2, 3, &c., small dots are found in the place of figures. This is to show that the two figures which are to be prefixed from the first column have changed, and they are to be taken from the horizontal line directly below. The place of the dots is to be supplied with ciphers. Thus

the logarithm of 2045 is 3.310693; " 9777 is 3.990206.

The two leading figures from the column 0 must also be taken from the horizontal line below, if any dots have been passed over on the same norizontal line. Thus

the logarithm of 1628 is 3.211654.

To find the Logarithm of any Number containing more than four Figures.

By inspecting the table, we shall find that within certain limits the logarithms are nearly proportional to their corresponding numbers. Thus the logarithm of 7250 is 3.860338;

" 7251 is 3.860398;

" 7252 is 3.860458;

" 7253 is 3.860518.

Here the difference between the successive logarithms, called the tabular difference, is constantly 60, corresponding to a difference of unity in the natural numbers. If, then, we suppose the logarithms to be proportional to their corresponding numbers (as they are nearly), a difference of 0.1 in the numbers should correspond to a difference of 6 in logarithms; a difference of 0.2 in the numbers should correspond to difference of 12 in the logarithms, &c. Hence

the logarithm of 7250.1 must be 3.860344;
" " 7250.2 " 3.860350;
" " 7250.3 " 3.860356;
&c., &c.

In order to facilitate the computation, the tabular difference is inserted on page 16 in the column headed D, and the proportional part for the fifth figure of the natural number is given at the bottom of the page. Thus, when the tabular difference is 60, the corrections for .1, .2, .3, &c., are seen to be 6, 12, 18, &c.

If the given number was 72501, the characteristic of its logarithm would be 4, but the decimal part would be the me as for 7250!

If it were required to find the correction for a sixth figure in the nat ural number, it is readily obtained from the Proportional Parts in the table. Thus, if the correction for .5 is 30, the correction for .05 is obviously 3.

As the differences change rapidly in the first part of the table, it was found inconvenient to give the proportional parts for each tabular difference; accordingly, for the first seven pages they are only given for the even differences, but the proportional parts for the odd differences will be readily found by inspection.

Required the logarithm of 452789.

The logarithm of 452700 is 5.655810

The tabular difference is 96.

Accordingly, the correction for the fifth figure, 8, is 77, and for the sixth figure, 9, is 8.6, or 9 nearly. Adding these corrections to the number before found, we obtain 5.655896.

The preceding logarithms do not pretend to be perfectly exact, bu only the nearest numbers having but six decimal places. Accordingly when the fraction which is omitted exceeds half a unit in the sixth decimal place, the last figure must be increased by unity.

Required the logarithm of 8765432.

7707000						
The logarithm of 8765000 is					6.942752	
Correction for the fifth figure 4,				20		
	66	46	sixth figure 3,		1.5	
	"	66	seventh figure 2		0.1	
Therefore the logarithm of 8765432 is				6.942	2774.	
	the logarithn					
The logarithm of 234500 is				5.370	143	
	Correction	for th	e fifth figure 6,		111	
	, 66	46	sixth figure 7,		13	
Therefore	the logarith	m of 2	-234567 is	5.3702	267.	

To find the Logarithm of a Decimal Fraction.

The decimal part of the logarithm of any number is the same as tha of the number multiplied or divided by 10, 100, 1000, &c. Hence, for a decimal fraction, we find the logarithm as if the figures were integers and prefix the characteristic according to the usual rule.

EXAMPLES.

The logarithm of 345.6				2.538574;
"	66	87.65	is	1.942752;
+4	66	2.345	is	0.370143;
44	. "	.1234	is	ī.091315;
	66	205678	is	$\bar{3}.754195.$

The minus sign is placed over the characteristic to show that this alone is negative, while the decimal part of the logarithm is positive.

To find the Logarithm of a Vulgar Fraction.

We may reduce the vulgar fraction to a decimal, and find its logs rithm by the preceding rule; or, since the value of a fraction is equal to the quotient of the numerator divided by the denominator, we may subtract the logarithm of the denominator from that of the numerator; the difference will be the logarithm of the quotient.

Required the logarithm of $\frac{3}{16}$, or 0.1875.

From the logarithm of 3, 0.477121, Subtract the logarithm of 16, 1.204120.

Leaves logarithm of $\frac{3}{16}$, or .1875, $\overline{1}$.273001. In the same manner we find

the logarithm of $\frac{4}{55}$ is $\overline{2}.861697$; " $\frac{1}{8}\frac{2}{7}\frac{3}{8}$ is $\overline{1}.147401$.

To find the natural Number corresponding to any Logarithm.

Look in the table in the column headed 0 for the first two figures of the logarithm, neglecting the characteristic; the other four figures are to be looked for in the same column, or in one of the nine following columns; and if they are exactly found, the first three figures of the corresponding number will be found opposite to them in the column headed N, and the fourth figure will be found at the top of the page. This num ber must be made to correspond with the characteristic of the given logarithm by pointing off decimals or annexing ciphers. Thus

the natural number belonging to the logarithm 4.370143 is 23450;
" " 1.538574 is 34.56.

If the decimal part of the logarithm can not be exactly found in the table, look for the nearest less logarithm, and take out the four figures of the corresponding natural number as before; the additional figures may be obtained by means of the Proportional Parts at the bottom of the page.

Required the number belonging to the logarithm 4.368399. On page 6, we find the next less logarithm .368287.

The four corresponding figures of the natural number are 2335. Their logarithm is less than the one proposed by 112. The tabular difference is 186; and, by referring to the bottom of page 6, we find that, with a difference of 186, the figure corresponding to the Proportional Part 112 is 6. Hence the five figures of the natural number are 23356; and, since the characteristic of the proposed logarithm is 4, these five figures are all integral.

Required the number belonging to logarithm 5.345678.

The next less logarithm in the table is .345570

Their difference is .108.

The first four figures of the natural number are 2216.

With the tabular difference 196, the fifth figure corresponding to 108 is seen to be 5, with a remainder of 10, which furnishes a sixth figure 5 nearly. Hence the required number is 221655.

In the same manner we find

the number corresponding to logarithm 3.538672 is 3456.78;

" 1.994605 is 98.7654;

" " \(\bar{1}.647817\) is .444444.

TABLE OF NATURAL SINES AND TANGENTS, pp. 116-133.

This is a table of natural sines and tangents for every degree and minute of the quadrant, carried to six places of figures. Since the radius of the circle is supposed to be unity, the sine of every arc below 90° is less than unity. These sines are expressed in decimal parts of the radius; and, although the decimal point is not written in the table, it must always be prefixed. The degrees are arranged in order at the top of the page, and the minutes in the left hand vertical column. Directly under the given number of degrees at the top of the page, and opposite to the minutes on the left, will be found the sine required. The two leading figures are repeated at intervals of ten minutes. Thus

the sine of 6° 27' is .112336;
" 28° 53' is .483028.

The same number in the table is both the sine of an arc and the cosine of its complement. The degrees for the cosines must be sought at the bottom of the page, and the minutes on the right. Thus

the cosine of 62° 25' is .463038;
" 84° 23' is .097872.

If a sine is required for an arc consisting of degrees, minutes, and seconds, it may be found by means of the line at the bottom of each page, which gives the proportional part corresponding to one second of arc

Required the sine of 8° 9' 10".

The sine of 8° 9' is .141765.

By referring to the bottom of page 116, in the column under 8°, we find the correction for 1" is 4.80; hence the correction for 10" must be 48, which, added to the number above found, gives for the sine of 8° 9′ 10", .141813.

In the same manner we find

the cosine of 56° 34' 28" is .550853.

It will be observed, that since the cosines decrease while the arcs magnetic transfer of the 28" is to be subtracted from the cosine of 56° 34'.

The arrangement of the table of natural tangents is similar to that of the table of sines. The tangents for arcs less than 45° are all less than radius, and consist wholly of decimals. For arcs above 45°, the tangents are all greater than radius and contain both integral and decimal

hgures. The proportional parts at the bottom of each page enable us readily to find the correction for seconds. Thus

the natural tangent of 32° 29′ 18″ is .636784;
" 74° 35′ 55″ is 3.63014.

To find the Number of Degrees, Minutes, and Seconds belonging to a given Sine or Tangent.

If the given sine or tangent is found exactly in the table, the corresponding degrees will be found at the top of the page, and the minutes on the left hand. But when the given number is not found exactly in the table, look for the sine or tangent which is next less than the proposed one, and take out the corresponding degrees and minutes. Find, also, the difference between this tabular number and the number proposed, and divide it by the proportional part for 1" found at the bottom of the page; the quotient will be the required number of seconds.

Required the arc whose sine is .750000.

The next less sine in the table is .749919, the arc corresponding to which is 48° 35′. The difference between this sine and that proposed is 81, which, divided by 3.21, gives 25. Hence the required arc is 48° 35′ 25″.

In the same manner we find

the arc whose tangent is 2.000000, to be 63° 26′ 6″.

TABLE OF NATURAL SECANTS, pp. 134-5.

This is a table of natural secants for every ten minutes of the quadrant carried to seven places of figures. The degrees are arranged in order in the first vertical column on the left, and the minutes at the top of the page. Thus

the secant of 21° 20' is 1.073561;
" 81° 50' is 7.039622.

If a secant is required for a number of minutes not given in the table, the correction for the odd minutes may be found by means of the last pertical column on the right, which shows the proportional part for one minute.

Let it be required to find the secant of 30° 33'.

The secant of 30° 30' is 1.160592.

The correction for 1' is 198.9, which, multiplied by 3, gives 597. Adding this to the number before found, we obtain 1.161189.

For a cosecant, the degrees must be sought in the right-hand vertical column, and the minutes at the bottom of the page. Thus

the cosecant of 47° 40' is 1.352742.

Table of Logarithmic Sines and Tangents, pp. 21-115.

This is a table of the logarithms of the sines and tangents for every ten seconds of the quadrant, carried to six places of decimals The de-

grees and seconds are placed at the top of the page, and the minutes in the left vertical column. After the first two degrees, the three leading figures in the table of sines are only given in the column headed 0", and are to be prefixed to the numbers in the other columns, as in the table of logarithms of numbers. Also, where the leading figures change, this change is indicated by dots, as in the former table. The correction for any number of seconds less than 10 is given at the bottom of the page.

To find the Logarithmic Sine or Tangent of a given Arc.

Look for the degrees at the top of the page, the minutes on the left hand, and the next less tenth second at the top; then, under the seconds, and opposite to the minutes, will be found four figures, to which the three leading figures are to be prefixed from the column headed 0"; to this add the proportional part for the odd seconds from the bottom of the page.

Required the logarithmic sine of 24° 27′ 34″.

The logarithmic sine of 24° 27′ 30″ is 9.617033.

Proportional part for 4" is

Logarithmic sine of 24° 27′ 34″ is 9.617051.

This is the logarithm of .414049 found in the table of natural sines on page 120. The natural sine being less than unity, the characteristic of its logarithm is negative. To obviate this inconvenience, the characteristics in the table nave all been increased by 10; or the logarithmic sines may be regarded as the logarithms of natural sines computed for a radius of 10,000,000,000.

Required the logarithmic tangent of 73° 35' 43".

The logarithmic tangent of 73° 35′ 40″ is 10.531031.

Proportional part for 3" is

23.

Logarithmic tangent of 73° 35′ 43″ 10.531054.

When a cosine is required, the degrees and seconds must be sought at the bottom of the page, and the minutes on the right, and the correction for the odd seconds must be subtracted from the number in the table.

Required the logarithmic cosine of 59° 33′ 47″.

The logarithmic cosine of 59° 33′ 40″ is 9.704682.

Proportional part for 7" is

25.

Logarithmic cosine of 59° 33′ 47″ is 9.704657.

So, also, the logarithmic cotangent of 37° 27′ 14″ is found to be 10.115744.

The proportional parts given at the bottom of each page correspond

to the degrees at the top of the page increased by 30', and are not strictly applicable to any other number of minutes; nevertheless, the differences of the sines change so slowly, except near the commencement of the quadrant, that the error resulting from using these numbers for every part of the page will so dom exceed a unit in the sixth decimal place. For the first two degrees, the differences change so rapidly

that the proportional part for 1" is given for each minute in the right-hand column of the page. The correction for any number of seconds less than ten will be found by multiplying the proportional part for 1' by the given number of seconds.

Required the logarithmic sine of 1° 17′ 33″.

The logarithmic sine of 1° 17′ 30″ is 8.352991

The correction for 3" is found by multiplying 93.4 by 3, which gives 280. Adding this to the above tabular number, we obtain

the sine of 1° 17′ 33″, 8.353271.

A similar method may be employed for several of the first degrees of the quadrant, if the proportional parts at the bottom of the page are not thought sufficiently precise. This correction may, however, be obtained pretty nearly by inspection from comparing the proportional parts for two successive degrees. Thus, on page 26, the correction for 1", corresponding to the sine of 2° 30', is 48; the correction for 1", corresponding to the sine of 3° 30', is 34. Hence the correction for 1", corresponding to the sine of 3° 0', must be about 41; and in the same manner we may proceed for any other part of the table.

Near the close of the quadrant, the tangents vary so rapidly, that the same arrangement of the table is adopted as for the commencement of the quadrant. For the last as well as the first two degrees of the quadrant, the proportional part to 1" is given for each minute separately. These proportional parts are computed for the minutes placed opposite to them. increased by 30', and are not strictly applicable to any other number of seconds; nevertheless, the differences for the most part change so slowly, that the error resulting from using these numbers for every part of the same horizontal line is quite small. When great accuracy is required, the table on page 114 may be employed for arcs near the limits of the quadrant. This table furnishes the differences between the logarithmic sines and the logarithms of the arcs expressed in seconds. Thus

the logarithmic sine of 0° 5' is 7.162696; the logarithm of 300'' (=5') is 2.477121; the difference is 4.685575.

This is the number found on page 114, under the heading \log sins A— \log . A'', opposite 5 min.; and in a similar manner the other numbers in the same column are obtained. These numbers vary quite slowly for two degrees; and hence, to find the logarithmic sine of an arc less than two degrees, we have but to add the logarithm of the arc expressed in seconds to the appropriate number found in this table.

Required the logarithmic sine of 0° 7' 22".

Tabular number from page 114, 4.685575. The logarithm of 442" is 2.645422.

Logarithmic sine of 0° 7' 22" is 7.330997

The logarithmic tangent of an arc less than two degrees is found in a similar manner.

Required the logarithmic tangent of 0° 27' 36".

Tabular number from page 114, 4.685584. The logarithm of 1656" is 3.219060.

The logarithm of 1656" is 3.219060.

Logarithmic tangent of 0° 27′ 36" is 7.904644.

The column headed log. cot. A+log. A'' is found by adding the log-arithmic cotangent to the logarithm of the arc expressed in seconds. Hence, to find the logarithmic cotangent of an arc less than two degrees, we must subtract from the tabular number the logarithm of the arc in seconds.

Required the logarithmic cotangent of 0° 27' 36".

Tabular number from page 114, 15.314416. The logarithm of 1656" is 3.219060.

The logarithm of 1656" is 3.219060.

Logarithmic cotangent of 0° 27' 36" is 12.095356.

The same method will, of course, furnish cosines and cotangents of arcs near 90°.

The secants and cosecants are omitted in this table, since they are easily derived from the cosines and sines.

The logarithmic secant is found by subtracting the logarithmic cosine from 20; and the logarithmic cosecant is found by subtracting the logarithmic sine from 20.

Thus we have found the logarithmic sine of 24° 27′ 34″ to be 9.617051. Hence the logarithmic cosecant of 24° 27′ 34″ is 10.382949.

The logarithmic cosine of 54° 12′ 40″ is 9.767008. Hence the logarithmic secant of 54° 12′ 40″ is 10.232992.

To find the Arc corresponding to a given Logarithmic Sine or Tangent

If the given number is found exactly in the table the corresponding degrees and seconds will be found at the top of the page, and the minutes on the left. But when the given number is not found exactly in the table, look for the sine or tangent which is next less than the proposed one, and take out the corresponding degrees, minutes, and seconds. Find, also, the difference between this tabular number and the number proposed, and, corresponding to this difference, at the bottom of the page will be found a certain number of seconds, which is to be added at the arc before found.

Required the arc corresponding to the logarithmic sine 9.750000.

The next less sine in the table is 9.749987.

The arc corresponding to which is 34° 13′ 0″.

The difference between its sine and the one proposed is 13, corresponding to which, at the bottom of the page, we find 4" nearly. Hence the required arc is 34° 13′ 4".

In the same manner we find the arc corresponding to logarithmic tan gent 10.250000, to be 60° 38′ 57″.

When the arc falls within the first two degrees of the quadrant, the odd seconds may be found by dividing the difference between the tabular number and the one proposed, by the proportional part for 1". We thus find the arc corresponding to logarithmic sine 8.400000, to be 1° 26′ 22" nearly.

We may employ the same method for the last two degrees of the quadrant when a tangent is given; but near the limits of the quadrant it is better to employ the auxiliary table on page 114. If we subtract the corresponding tabular number on page 114 from the given logarith mic sine, the remainder will be the logarithm of the arc expressed in seconds.

Required the arc corresponding to logarithmic sine 7.000000.

We see, from page 22, that the arc must be nearly 3'; the corresponding tabular number on page 114 is 4.685575.

The difference is 2.314425;

which is the logarithm of 206."265.

Hence the required arc is 3' 26."265.

In the same manner we find the arc corresponding to logarithmic tangent 8.184608, to be 0° 52′ 35″.

Table for the Lengths of Circular Arcs, p. 135.

This table contains the lengths of every single degree up to 60, and at intervals of ten degrees up to 180; also for every minute and second up to 20. The lengths are all expressed in decimal parts of radius.

Required the length of an arc of 57° 17' 44."8.

Take out from their respective columns the lengths answering to each of these numbers singly, and add them all together thus:

			0				
57°	•	•	•	•	•	•	0.9948377
17'							.0049451
40 ′′							.0001939
$4^{\prime\prime}$						٠.	.0000194
0.''8							.0000039
		Th	ne s	ยาท	is		1 0000000

That is, the length of an arc of 57° 17′ 44.″8 is equal to the radius of the circle.

Traverse Table, pp. 136-141.

This table shows the difference of latitude and the departure to four decimal places for distances from 1 to 10, and for bearings from 0° to 90°, at intervals of 15′. If the bearing is less than 45°, the angle will be found on the left margin of one of the pages of the table, and the distance at the top or bottom of the page; the difference of latitude wil

be found in the column headed lat. at the top of the page, and the departure in the column headed dep. If the bearing is more than 45°, the angle will be found on the right margin, and the difference of attitude will be found in the column marked lat. at the bottom of the page, and the departure in the other column. The latitudes and departures for different distances with the same bearing, are proportional to the distances. Therefore the distances may be reckoned as tens, hundreds, or thousands, if the place of the decimal point in each departure and difference of latitude be changed accordingly.

Required the latitude and departure for the distance 32.25, and the bearing 10° 30'.

On page 136, opposite to 10° 30′, we find the following latitudes and departures, proper attention being paid to the position of the decimal points.

Distance.	Diff. Lat.	Dep.
30	29.498	5.467
2	1.966	.364
.2	.197	.036
.05	.049	.009
32.25	31.710	$\overline{5.876}$.

Table of Meridional Parts, pp. 142-148.

This table gives the length of the enlarged meridian on Mercators Chart to every minute of latitude expressed in geographical miles and tenths of a mile. The degrees of latitude are arranged in order at the top of the page, and the minutes on both the right and left margins. Under the degrees and opposite to the minutes are placed the meridional parts corresponding to any latitude less than 80°. Thus

the meridional parts for latitude 12° 23' are 748.9;
" 57° 42' are 4260.5.

TABLE OF CORRECTIONS TO MIDDLE LATITUDE, p. 149.

This table is used in Navigation for correcting the middle latitude. The given middle latitude is to be found either in the first or last vertical column, opposite to which, and under the given difference of latitude, is inserted the proper correction in minutes, to be added to the middle latitude to obtain the latitude in which the meridian distance is accurately equal to the departure. Thus, if the middle latitude is 41°, and the difference of latitude 14°, the correction will be found to be 25′, which, added to the middle latitude, gives the corrected middle latitude 41° 25′.

ATABLE

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LOGARITHMS OF NUMBERS

FROM 1 TO 10,000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0.000000	26	1.414973	51	1.707570	76	1.880814
2	0.301030	27	1.431364	52	1.716003	77	1.886491
3	0.477121	28	1.447158	53	1.724276	78	1.892095
4	0.602060	29	1.462398	54	1.732394	79	1.897627
5	0.698970	30	1.477121	55	1.740363	80	1.903090
6 7 8 9	0.778151 0.845098 0.903090 0.954243 1.000000	31 32 33 34 35	1.491362 1.505150 1.518514 1.531479 1.544068	56 57 58 59 60	1.748188 1.755875 1.763428 1.770852 1.778151	81 82 83 84 85	1.908485 1.913814 1.919078 1.924279 1.929419
11	1.041393	36	1.556303	61	1.785330	86	1.934498
12	1.079181	37	1.568202	62	1.792392	87	1.939519
13	1.113943	38	1.579784	63	1.799341	88	1.944483
14	1.146128	39	1.591065	64	1.806180	89	1.949390
15	1.176091	40	1.602060	65	1.812913	90	1.954243
16	1.204120	41	1.612784	66	1.819544	91	1.959041
17	1.230449	42	1.623249	67	1.826075	92	1.963788
18	1.255273	43	1.633468	68	1.832509	93	1.968483
19	1.278754	44	1.643453	69	1.838849	94	1.973128
20	1.301030	45	1.653213	70	1.845098	95	1.977724
21 22 23 24 25	1.322219 1.342423 1.361728 1.380211 1.397940	46 47 48 49 50	1.662758 1.672098 1.681241 1.690196 1.698970	71 72 73 74 75	1.851258 1.857332 1.863323 1.869232 1.875061	96 97 98 99	1.982271 1.986772 1.991226 1.995635 2.000000

N.B. In the following table, the two leading figures in the first column of logarithms are to be prefixed to all the numbers of the same horizontal line in the next nine columns; but when a point (.) occurs, its place is to be supplied by a cipher, and the two leading figures are to be taken from the next lower line.

NT.	1 -	1	6	0	4	E	c	7	0	0	D
N	0	1	2	3	4	5	6		8	9	D.
100	4321	0434 4751	0868 5181	1301 560g	1734 6038	2166 6466	2598 6894	3029 7321	3461 7748	3891 8174	432 428
102	8600	9026	9451	9876	.300	.724	1147	1570	1993	2415	424
103	012837	3250	368o	4100	4521	4940	536o	5779	6197	6616	419
104	7033	745í	7868	8284	8700	9116	9532	9947	.36i	.775	416
105	021189	1603	2016	2428	2841	3252	3664	4075	4486	4896	412
106	5306	5715	6125	6533	6942	7350	7757	8164	8571	8978	408
107	9384	9789	.195	.600	1004	1408	1812	2216	2619	3021	404
108	033424 7426	3826 7825	4227	4628 8620	5029	5430	5830 9811	6230	6629	7028	400
110	041393	1787	8223 2182	2576	9017 2969	9414 3362	3755	.207 4148	4540	4932	396 393
						}					
III	5323	5714	6105	6495	6885	7275	7664	8053	8442	8830	389
112	9218	9606 3463	9993 3846	.380 4230	.766 4613	1153	1538 5378	1924 5760	2309 6142	2694 6524	386 382
113	053078 6905	7286	7666	8046	8426	4996 8805	9185	9563	9942	.320	379
115	060698	1075	1452	1829	2206	2582	2958	3333	3709	4083	376
116	4458	4832	5206	5580	5953	6326	6699	7071	7443	7815	373
117	8186	8557	8928	9298	9668	38	.407	.776	1145	1514	369
118	071882	2250	2617	2985	3352	3718	4085	4451	4816	5182	366
119	5547	5912	6276	6640	7004	7368	7731	8094	8457	8819	363
120	9181	9543	9904	.266	.625	.987	1347	1707	2067	2426	360
121	082785	3144	3503	3861	4219	4576	4934	5291	5647	6004	357
- N.	0	1	2	3	4	5	6	7	8	9	D.
ſ	434	43	87	130	174	217	260	304	347	391	
- 1	432	43	86	130	173	216	259	302	346	389	
	430	43	86 86	129	172	215	258	301 300	344 342	387 385	
1	428 426	43 43	85	128	171 170	214	257 256	298	341	383	
i	424	42	85	127	170	212	254	297	339	382	
J	422	42	84	127	169	211	253	295	338	380	
	420	42	84	126	168	210	252	294	336	378	
,	418	42	84	125	167	200	251	293	334	376	
!	416	42	83	125	166	208	250	291	333	374	
	414	41	83	124	166	207	248	290	331	373	
- 1	412	41	82	124	165	206	247	288	33o	371	
	410	41	82	123	164	205	246	287	328	369	
İ	408	41	82	122	163	204	245	286	326	367	
1	406	41	81	122	162	203	244	284	325	365	
	404 stra	40	81	121	162	202	242	283	323	364	
pi l		40	80	121	161	201	241	281	322	362	
8		40	80	120	160	200	240	280	320	36o 358	
6 {	398 Re 396 Si	40 40	80	119	159 158	199	239 238	279 277	318 317	356	
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	388	39 39 39	79 78 78 78	118 117 116	157 156 155	197 196 195	236 235 234 233	276 274 273 272	314 312 310	353 351 349	
	388 386	39 39 39 39	79 78 78 78 77	118 117 116 116	157 156 155 154	197 196 195 194 193	236 235 234 233 232	276 274 273 272 270	314 312 310 309	353 351 349 347	
	388	39 39 39	79 78 78 78 77	118 117 116	157 156 155	197 196 195 194 193	236 235 234 233	276 274 273 272	314 312 310	353 351 349	
	388 386 384 382 380	39 39 39 39 38	79 78 78 78 77 77	118 117 116 116 115	157 156 155 154 154 153 152	197 196 195 194 193	236 235 234 233 232 230	276 274 273 272 270 269	314 312 310 309 307	353 351 349 347 346 344 342	
	388 386 384 382 380 378	39 39 39 39 38 38 38	79 78 78 78 77 77 76 76	118 117 116 116 115 115 114 113	157 156 155 154 154 153 152	197 196 195 194 193 192 191 190	236 235 234 233 232 230 229 228 227	276 274 273 272 270 269 267 266 265	314 312 310 309 307 306 304 302	353 351 349 347 346 344 342 340	
	388 386 384 382 380	39 39 39 39 38 38	79 78 78 78 77 77 76	118 117 116 116 115 115	157 156 155 154 154 153 152	197 196 195 194 193 192 191	236 235 234 233 232 230 229 228	276 274 273 272 270 269 267 266	314 312 310 309 307 306 304	353 351 349 347 346 344 342	
	388 386 384 382 380 378 376	39 39 39 39 38 38 38 38	79 78 78 78 77 77 76 76 76 75	118 117 116 116 115 115 114 113	157 156 155 154 154 153 152 151 150	197 196 195 194 193 192 191 190	236 235 234 233 232 230 229 228 227	276 274 273 272 270 269 267 266 265 263	314 312 310 309 307 306 304 302 301	353 351 349 347 346 344 342 340 338	
	388 386 384 382 380 378 376 374	39 39 39 39 38 38 38 38 37	79 78 78 78 77 77 76 76	118 117 116 116 115 115 114 113	157 156 155 154 154 153 152 151 150 150	197 196 195 194 193 192 191 190 189 188	236 235 234 233 232 230 229 228 227 226	276 274 273 272 270 269 267 266 265 263 262	314 312 310 309 307 306 304 302 301 299 298	353 351 349 347 346 344 342 340 338 337 335	
	388 386 384 382 380 378 376 374 372	39 39 39 39 38 38 38 38 38 37 37	79 78 78 77 77 76 76 76 75 74	118 117 116 116 115 115 114 113 113 112 1112	157 156 155 154 154 153 152 151 150 149 148	197 196 195 194 193 192 191 190 189 188 187	236 235 234 233 232 230 229 228 227 226 224 223	276 274 273 272 270 269 267 266 265 263 262 260 259	314 312 310 309 307 306 304 302 301 299 298 296	353 351 349 347 346 344 342 340 338 337 335 333	
	388 386 384 382 380 378 376 374 372 370 368	39 39 39 39 38 38 38 38 37 37 37	79 78 78 77 76 76 76 75 74 74	118 117 116 116 115 115 114 113 113 112 1112 1111 110	157 156 155 154 154 153 152 151 150 149 148 147	197 196 195 194 193 192 191 190 189 188 187 186 185	236 235 234 233 232 230 229 228 227 226 224 223 222	276 274 273 272 270 269 267 266 265 263 260 259 258	314 312 310 309 307 306 304 302 301 299 298 296	353 351 349 347 346 344 342 340 338 337 335 333 331	
	388 386 384 382 380 378 376 374 372 370 368 366	39 39 39 39 38 38 38 38 37 37 37 37	79 78 78 77 76 76 76 76 77 74 74 73	118 117 116 116 115 115 114 113 113 112 112 111 110	157 156 155 154 154 153 152 151 150 149 148 147 146	197 196 195 194 193 192 191 190 188 187 186 185 184	236 235 234 233 230 229 228 227 226 224 223 222 221	276 274 273 272 270 269 267 266 265 263 260 259 258 256	314 312 310 309 307 306 304 302 301 298 298 296 294 293	353 351 349 347 346 344 342 340 338 337 335 333 331 329	
	388 386 384 382 380 378 376 374 372 370 368	39 39 39 39 38 38 38 38 37 37 37	79 78 78 77 76 76 76 75 74 74	118 117 116 116 115 115 114 113 113 112 1112 1111 110	157 156 155 154 154 153 152 151 150 149 148 147	197 196 195 194 193 192 191 190 189 188 187 186 185	236 235 234 233 232 230 229 228 227 226 224 223 222	276 274 273 272 270 269 267 266 265 263 260 259 258	314 312 310 309 307 306 304 302 301 299 298 296	353 351 349 347 346 344 342 340 338 337 335 333 331	

N.	0	1	2	3	4	5	6	7	8	9	D.
122	o8636o	6716	707I	7426	7781	8136	8490	8845	9198	9552	355
123	9905	.258	.611	.963	1315	1667	2018	2370	2721	3071	351
124	6910	3772 7257	7604	4471 7951	4820 8298	5169 8644	5518 8990	5866 9335	6215 9681	6562	349 346
126	100371	0715	1059	1403	1747	2001	2434	2777	3119	3462	343
127	3804	4146	4487	4828	5169	5510	5851	6191	6531	6871	3/11
128	7210	7549	7888	8227	8565	8903	9241	9579	9916	.253	338
129	110590 3943	4277	1263 4611	1599 4944	1934 5278	2270 5611	2605 5943	2940 6276	3275 6608	3609 6940	335 333
131	7271	7603	7934	8265	8595	8926	9256	9586	9915	.245	33o
132	120574	0903	1231	1560	1888	2216	2544	2871	3198	3525	328
133	3852	4178	4504	483o	5156	5481	5806	6131	6456	6781	325
134	7105	7429	7753	8076	8399	8722	9045	9368	9690	12	323
135 136	130334 3539	0655 3858	0977 4177	1298 4496	1619 4814	1939 5133	2260 5451	2580 5769	2900 6086	3219 6403	321 318
137	6721	7037	7354	7671	7987	8303	8618	8934	9249	9564	315
138	9879	.194	.508	.822	1136	1450	1763	2076	2389	2702	314
139	143015	3327	3639	3951	4263	4574	4885	5196	5507	5818	311
140 L41	6128	6438	6748 9835	7058 .142	7367	7676 .756	7985 1063	8294 1370	8603	8911	309
	9219	9527	1		.449				1676	1982	307
142	152288 5336	2594 5640	2900 5943	3205 6246	3510 6549	3815 6852	4120 7154	4424 7457	4728 7759	5032 8061	3o5 3o3
144	8362	8664	8965	9266	9567	9868	.168	.469	.769	1068	301
145	161368	1667	1967	2266	2564	2863	3161	346o	3758	4055	299
146	4353	4650	.4947	5244	5541	5838	6134	6430	6726	7022	297
147	7317 170262	7613 0555	7908 0848	8203 1141	8497 1434	8792 1726	9086	9380 2311	9674 2603	9968 2895	295 293
N.	0 1	1	2	3	4	5	6	7	8	9	D.
	358	36	72	107	143	179	215	251	286	322	
	356	36	71	107	142	178	214	249	285	320	,
	354 352	35 35	71 70	106 106	142 141	177	212 211	248 246	283 282	319 317	
	35o	35	70	105	140	175	210	245	280	315	
	348	35	70	104	139	174	209	244	278	313	
	346	35	69	104	138	173	208	242	277	311	
	344	34 34	69 68	103 103	138 137	172 171	206 205	241 239	275 274	310 308	
	340	34	68	102	136	170	204	238	272	306	
	338	34	68	101	135	169	203	237	270	304	
	336	34	67	101	134	168	202	235	269	302	
	334 332 🕏	33 33	67 66	100	134 133	167	200 199	234 232	267 266	301 299	
200	330 Parts	33	66	99	132	165	198	231	264	297	
nce		33	66	98	131	164	197	230	262	295	
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	320 SI	32	64	96	128	160	192	224	256	288	
	1	32	64	05	127	159	191	223	254	286	
	316 314	32 31	63 63	95 04	126 126	158 157	190 188	22I 220	253 251	284 283	
	314	31 31	62	94 94	125	156	187	218	250	281	
	310	31	62	93	124	155	186	217	248	279	
	308	31	62	92	123	154	185	216	246	277	
	306 304	31 30	61	92	122 122	153 152	184 182	214 213	245 243	275	
	304 302	30	60	91	121	151	181	213	243	274 272	
	300	3о	60	90	120	150	180	210	240	270	
	298	30	60	89	119	149	179	209	238	268	
	296 294	30 29	59 59	8 9 88	118	148	178 176	207 206	237 235	266 265	
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182	260071	0310	0548	0787	1025	1263	1501	1739	1976	2214	238
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582	237
:84	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937	235
185	7172	7406	7641	7875	8110	8344	8578	8812	9046	9279	234
186	9513	9746 2074	9980 2306	2538	.446	3001	.912 3233	3464	1377 3696	1609	233 232
187	4158	4389	4620	4850	2770 5081	5311	5542	5772	6002	3927 6232	230
189	6462	6692	6921	7151	7380	7609	7838	8067	8296	8525	229
190	8754	8982	9211	9439	9667	9895	.123	.35i	578	.806	228
191	281033	1261	í488	1715	1942	2169	2396	2622	2849	3075	227
192	33or	3527	3753	3979	4205	4431	4656	4882	5107	5332	226
193	5557	5782	6007	6232	6456	6681	6905	7130	7354	7578	225
194	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812	223
195	290035	0257	0480	0702	0925	1147	1369	1591	1813	2034	222
196	2256 4466	2478 4687	2699	2920 5127	3141 5347	3363 556 ₇	3584 5787	3804 6007	4025 6226	4246 6446	22I 220
197	1 2224	6884	4907 7104	7323	7542	7761	7979	8198	8416	8635	219
199	8853	9071	9289	9507	9725	9943	.161	.378	.595	.813	218
200	301030	1247	1464	168i	1898	2114	233 1	2547	2764	2980	217
201	3196	3412	3628	3844	4059	4275	4491	4706	4921	5136	216
202	535ı	5566	5781	5996	6211	6425	6639	6854	7068	7282	214
203	7496	7710	7924	8137	835ı	8564	8778	8991	9204	9417	213
204	9630	9843	56	.268	.481	.693	.906	1118	1330	1542	212
205	311754	1966	2177	2389	2600	2812	3023	3234	3445	3656	211
206	3867 5970	4078 6180	4289 6390	4499 6599	4710 6809	4920 7018	5130 7227	534o 7436	5551 7646	5760 7854	210
208	8063	8272	8481	8689	8898	9106	9314	9522	9730	9938	208
209	320146	0354	0562	0769	0977	1184	1391	1598	1805	2012	207
210	2219	2426	2633	2839	3646	3252	3458	36 6 5	3871	4077	206
211	4282	4488	4694	4899	5105	5310	5516	5721	5926	6131	205
212	6336	6541	6745	6950	7155	7359	7563	7767	7972	8176	204
213	8380	8583	8787	8991	9194	9398	9601	9805	8	.211	203
214	330414	0617 264c	0819 2842	1022 3044	1225 3246	1427 3447	1630 3649	1832 3850	2034 4051	2236 4253	202 202
216	4454	4655	4856	5057	5257	5458	5658	5859	6059	6260	201
217	6460	6660	686o	7060	7260	7459	7659	7858	8058	8257	200
218	8456	8656	8855	9054	9253	945i	9650	9849	47	.246	199
219	340444	0642	0841	1039	1237	1435	1632	1830	2028	2225	198
220	2423	2620	2817	3014	3212	3409	3606	3802	3999	4196	197
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	238 236	24	48	71	95	119	143	167	190	214	
	234	24 23	47 47	71 70	94 94 ·	118	142	165 164	187	212 211	
	232	23	47	70	93	116	139	162	186	209	
, ,	230	23	46	69	92	115	138	161	184	207	
1	228	23	46	68	91	114	137	160	182	205	
1 1	226	23	45	68	90	113	136	158	181	203	
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<u> </u>	218	22	44	65	87	109	131	153	174	196	
	216	22	43	65	86	108	130	151	173	194	
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	212 Å	2 I 2 I	42 42	63	84	105	127	140	168	191	
	208	21	42	62	83	104	125	146	166	187	
	206	21	41	62	82	103	124	144	165	185	
	204	20	41	6 r	82	102	122	143	163	184	
	202	20	40	61	81	IOI	121	141	162	182	
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1	198	20	40	59	79	99	119	139	158	178	

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234 9216 9401 9587 9772 9958 .143 .328 .513 .698 .883 .855 .236 .2912 .3096 .326 .3464 .3647 .3831 .4015 .4198 .4382 .4565 .237 .4748 .4932 .5115 .5298 .5481 .5664 .5846 .6029 .6212 .6394 .832 .238 .6577 .6576 .6942 .7124 .7366 .7488 .7670 .7852 .8034 .226 .239 .3082 .3565 .6942 .7124 .7366 .7488 .7670 .7852 .8034 .226 .230 .380211 .3032 .0573 .0754 .0344 .7115 .1296 .1476 .1656 .1837 .241 .2017 .2177 .2377 .2557 .2737 .2917 .3097 .3277 .3276 .3626 .3288 .3666 .7488 .7670 .3277 .3276 .3278 .3278 .3265 .3243 .3288 .7666 .7488 .7670 .7882 .7892 .3277 .3276 .3666 .7882 .7599 .777 .7300 .7568 .7746 .7023 .8011 .828 .465 .582 .759 .777 .248 .465 .582 .759 .777 .248 .465 .582 .759 .777 .248 .465 .3282 .759 .777 .248 .4627 .4802 .4977 .5152 .5366 .5561 .5826 .582 .759 .777 .248 .4627 .2697 .8273 .3048 .3224 .3400 .3575 .3751 .328 .405 .582 .759 .777 .249 .6199 .6374 .6548 .6722 .6896 .7071 .7245 .7419 .7592 .7766 .752 .7764 .722 .7964 .714 .7592 .7766 .7542 .7592 .7766 .7542 .7592 .7766 .7741 .7592 .7766 .7741 .7592 .7766 .7741 .7592 .7766 .7741 .7592 .7766 .7741 .7592 .7766 .7741 .7592 .7766 .7741 .7761 .77		1		l				6610	6796	6983	7169	187
235 371068 1253 1437 1652 1866 1991 2175 2360 2544 2728 184 236 2912 3096 3280 3464 3647 3831 4015 4198 4382 4565 237 44748 4932 5115 5298 5481 5664 5846 6029 6212 6394 183 238 6577 6759 6942 7124 7306 7488 7670 7852 8034 8216 182 240 380211 0392 0573 0754 0934 1115 1296 1476 1656 1837 241 2017 2197 2377 2557 2737 2917 3097 3277 3456 3636 180 242 3815 3995 4174 4353 4553 4712 4891 5070 5249 5428 179 243 5606 5785 5064 6142 6321 6499 6677 6856 7034 7212 244 7390 7568 7746 7923 8101 8279 8456 8634 8811 8989 245 9166 9343 0520 9688 9875 51 .228 .405 .552 .759 177 248 4452 4627 4892 4977 5152 5326 5501 5676 5850 6025 173 248 4452 4627 4892 4977 5152 5326 5501 5676 5856 6025 173 249 6199 6374 6548 6722 6886 7071 7245 7419 7592 7766 174 250 7940 8114 8287 8461 8634 8808 881 9154 9328 9501 173 251 9674 9847 20 29 .365 .533 .711 .883 1056 1228 252 401401 1573 1745 1917 2089 2261 2433 2605 2777 2949 172 256 41600 1753 1745 1917 2089 2261 2433 2605 2777 2949 172 256 41620 1788 1956 2124 2293 2461 2629 2796 2964 3132 168 256 41620 1788 1956 2124 2293 2461 2629 2796 2964 3132 168 256 41620 1788 1956 2124 2293 2461 2629 2796 2964 3132 168 256 41620 1788 1956 2124 2293 2461 2629 2796 2964 3132 168 262 830 8467 8363 8798 8964 9129 9295 9460 9625 9791 165 166 170 38 58 77 96 115 134 154 173 166 174 24 17 34 55 67 74 99 110 127 146 164					7915							
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242 3815 3995 4174 4353 4533 4712 4891 5070 5249 5428 179 243 5606 5785 5964 6142 6321 6499 6677 6856 7034 7212 178 244 7390 7568 7746 7923 8101 8279 8456 8634 8811 8989 245 9166 9343 9520 9698 9875 51 228 .405 .582 .759 177 246 247 2697 2873 3048 3224 3400 3575 3751 3926 4101 4277 248 4452 4627 4802 4977 5152 5326 5501 5676 5850 6025 175 224 6199 6374 6548 6722 6886 7071 7245 7410 7592 7766 174 250 7940 8114 8287 8461 8634 8808 8981 9154 9328 9501 173 251 9674 9847 20 .192 .365 .538 .711 .883 1365 1228 252 401401 1573 1745 1917 2089 2261 2433 2605 2777 2949 172 253 3121 3292 3464 3635 3807 3078 4149 4320 4492 4663 .71 256 8340 8410 8579 8749 8918 9087 9257 9426 9595 9764 169 257 9933 .102 .271 .440 .609 .777 .946 1114 1283 1451 258 411620 1788 1956 2124 2293 2461 2622 2796 2964 3132 168 259 3300 3467 3635 3803 3970 4137 4305 4472 4639 4806 167 261 6641 6887 6973 7139 7306 7472 7638 7804 7970 8135 166 262 8301 8467 8633 8798 8964 9129 9295 9460 9625 9791 165 165 165 169 188 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 173 190 19 38 58 77 96 115 134 154 175 175 176 173 188 19 37 56 74 99 108 122 147 166 18 35 53 70 88 106 123 141 158 157 175 176 174 164 168 173 175 175 176 174 166 177 34 50 667 84 100 116 133 149 157 176		1										180
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249			4627									1.75
251			6374	6548	6722	6896	7071	7245	7419			
252 401401 1573 1745 1917 2089 2261 2433 2605 2777 2949 172 253 3121 3292 3464 3635 3807 3978 4149 4320 4492 4663 271 254 4834 5005 5176 5346 5517 5688 5858 6029 6199 6370 255 6540 6710 6881 7051 7221 7391 7561 7731 7901 8070 170 256 8240 8410 8579 8749 8918 9087 9257 9426 9595 9764 169 257 9933 102 1271 1440 1609 1777 1946 1141 1283 1451 168 259 3300 3467 3635 3803 3970 2461 2629 2796 2964 3132 168 259 3300 3467 3635 3803 3970 4137 4305 4472 4639 4806 167 260 4973 5140 5307 5474 5641 5808 5974 6141 6308 6474 261 6641 6642 6807 6973 7139 7306 7472 7638 7804 7970 8135 166 262 8301 8467 8633 8798 8964 9129 9295 9460 9625 9791 165 263 9956 121 1286 1451 616 1781 194 113 132 157 176 176 194 19 39 58 78 97 116 136 155 175 176 194 19 39 58 78 97 116 136 155 175 176 184 64 18 37 55 74 92 110 127 146 164 24 18 18 36 55 73 91 109 127 146 164 24 18 36 55 73 91 109 127 146 164 24 18 36 55 73 91 109 127 146 164 24 18 36 53 70 88 106 123 141 158 174 21 17 35 52 70 87 104 122 139 157 176 176 176 176 176 176 177 1												173
253 3121 3292 3464 3635 3807 3978 4149 4320 4492 4663 271 254 4834 5005 5176 5346 5517 5688 5858 6029 6199 6370 255 6540 6710 6881 7051 7221 7391 7561 7731 7901 8070 170 256 8240 8410 8579 8749 8918 9087 9257 9426 9595 9764 169 257 9933 .102 .271 .440 .609 .777 .946 1114 1283 1451 1283 1451 1458 1956 2124 2293 2461 2629 2796 2964 3132 168 259 3300 3467 3635 3803 3970 4137 4305 4472 4639 4806 167 260 4973 5140 5307 5474 5641 5808 5974 6141 6308 6474 2611 6641 6807 6973 7139 7306 7472 7638 7804 7970 8135 166 262 830 8467 8633 8798 8964 9129 9295 9460 9625 9791 165 263 9956 .121 .286 .451 .616 .781 .945 1110 1275 1439							1 1					
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256			1					-		7901		170
258			8410	8579		8918	9087	9257	9426	9595		
259 3300 3467 3635 3803 3970 4137 4305 4472 4639 4806 167 260												-
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192					58	78					170	
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186 19 19 37 56 74 .93 112 130 149 167 184 18 18 37 55 74 92 110 129 147 166 182 18 36 55 73 91 109 127 146 164 162 180 18 36 53 71 89 107 125 142 160 178 18 36 53 70 88 106 123 141 158 174 21 17 35 52 70 87 104 122 139 157 172 17 34 52 69 86 103 120 138 155 168 17 34 50 67 84 101 118 134 151 166 17 33 50 66 83 100 116 133 149		190	19		57	76	95	114		- 1	171	
184 18 18 37 55 74 92 110 129 147 166 182 18 18 36 55 73 91 109 127 146 164 180 180 18 36 53 71 89 107 125 142 160 178 18 36 53 70 88 106 123 141 158 174 21 17 35 52 70 87 104 122 139 157 172 17 34 52 69 86 103 120 138 155 168 17 34 50 67 88 100 116 133 149 166 17 33 50 66 83 100 116 133 149 169 160 160 178 179						75	94					
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172	1000	182 =		36	55	74 73				147		
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264	421604	1768	1933	2097	2261	2426	2590	2754	2918	3082	164
265	3246 4882	3410 5045	3574 5208	3737 5371	3901 5534	4065 5697	4228 5860	4392 6023	4555 6186	4718 6349	163
267	6511	6674	6836	6999	7161	7324	7486	7648	7811	7973	162
268	8135	8297	8459	8621	8783	8944	9106	9268	9429	9591	- 6-
269	9752 431364	1525	1685	.236 1846	2007	2167	.720 2328	.881 2488	1042 2649	1203 2809	161
271	2969	3130	3290	3450	3610	3770	3930	4090	4249	4409	160
272	4569	4729	4888	5048	5207	5367	5526	5685	5844	6004	159
273	6163	6322	6481	6640	6799	6957	7116	7275	7433	7592	
274	7751 9333	7909 9491	8067 9648	8226 9806	8384 9964	8542	8701 •279	8859	.594	9175	158
276	440909	1066	1224	1381	1538	1695	1852	2009	2166	2323	157
277	2480	2637	2793	2950	3106	3263	3419	3576	3732	3889	
278	4045 5604	4201 5760	4357 5915	4513 6071	4669 6226	4825 6382	4981 6537	5137 6692	5293 6848	5449 7003	156 155
280	7158	7313	7468	7623	7778	7933	8088	8242	8397	8552	
281	8706	8861	9015	9170	9324	9478	9633	9787	9941	95	154
282	450249 1786	0403	0557 2093	0711 2247	0865 2400	2553	1172 2706	1326 2859	1479 3012	1633 3165	r53
284	3318	3471	3624	3777	3030	4082	4235	4387	454o	4692	
285	4845	4997	5150	5302	5454	5606	5758	5910	6062	6214	152
286	6366	6518	6670	6821	6973	7125	7276	7428	7579	7731	e.
287 288	7882 9392	8033 9543	8184 9694	8336 9845	8487 9995	8633	8789	8940 •447	909 1	9242	151
289	460898	1048	1198	1348	1499	1649	1799	1948	2098	2248	150
290	2398	2548	2697	2847	2997	3146	3296	3445	3594	3744	-/-
291	3893 538 3	4042 5532	4191 5680	4340 5829	4490 5977	4639	4788 6274	4936 6423	5085 6571	5234 6719	149
293	6868	7016	7164	7312	7460	7608	7756	7904	8052	8200	148
294	8347	8495	8643	8790	8938	9085	9233	9380	9527	9675	
295	9822	9969	.116	.263	.410	.557	.704	.851	.998	1145	147
296 297	471292 2756	1438 2903	1585 3049	1732 3195	1878 3341	2025 3487	3633	2318 3779	2464 3925	2610 4071	146
298	4216	4362	4508	4653	4799	4944	5090	5235	5 3 81	5526	
300	5671 7121	5816 7266	5962 7411	6107 7555	6252 7700	6397	6542 7989	668 ₇ 8133	6832 8278	6976 8422	145
301	8566	8711	8855	8999	9143	9287	9431	9575	9719	9863	144
302	480007	0151	0294	o438	0582	0725	0869	1012	1156	1299	
303	1443	1586	1729	1872	2016	2159	2302	2445	2588	2731	143
304 305	2874 4300	3016 4442	3159 4585	3302 4727	3445 4869	3587 5011	3730 5153	3872 5295	4015 5437	4157 5579	142
306	5721	5863	6005	6147	6289	6430	6572	6714	6855	6997	142
307	7138	7280	7421	7563	7704	7845	7986	8127	8269	8410	141
308	8551 9958	8692	8833 .239	8974 .380	9114 .520	9255 .661	9396 .801	9537 •941	9677 1081	9818	140
3ro	491362	1502	1642	1782	1922	2062	2201	2341	2481	2621	-
311	2760	2900	3040	3179	3319	3458	3597	3737	3876	4015	139
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	162 160	16 16	32 32	49 48	6.5 6.4	81 80	97 96	113	130 128	146 144	l i
		16	32	47	63		95	III	126	142	
, ₂₀	156 🖫	16	31	47 47	62	79 78	94	109	125	140	
Differences.	154 A	15 15	31 30	46 46	62 61	77 76	92 91	108 106	123 122	139 137	
ere!	152 150 146 144 Lobortional	15	30	45	6o	75	90	105	120	135	
)iff	148 6	15	30	44	59 58	74	89	104	120	133	
	146 do.	15	29	44	58	73	89 88	102	117	131	
	144 Å 142	14 14	29 28	43 43	58 57	72 71	86 85	101	115	130 128	
	140	14	28	42	57 56	70	84	98	112	126	
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312	494155	4294	4433	4572	4711	485o	4989	5128	5267	5406	139
313	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791	1
314	6930	7068 8448	7206 8586	7344 8724	7483 8862	7621 8999	7759	7897 9275	8035 9412	8173 9550	138
316	9687	9824	9962	99	.236	.374	.511	.648	.785	.922	137
317	501059	1196 2564	1333	1470 2837	1607 2973	1744 3109	1880 3246	2017 3382	2154	2291	
319	2427 3791	3927	4063	4199	4335	4471	4607	4743	3518 4878	3655 5014	136
320	5150	5286	5421	5557	5693	5828	5964	6099	6234	6370	
321	6505	6640	6776	6911	7046	7181	7316	7451	7586	7721	135
322	7856 9203	7991 9337	8126 9471	8260 9606	8395 9740	853o 9874	8664	8 7 99	8934	9068	134
324	510545	0679	0813	0947	1081	1215	1349	1482	1616	1750	
325 326	1883 3218	2017 3351	2151 3484	2284 3617	2418 3750	2551 3883	2684	2818 4140	2951	3084	133
327	4548	4681	4813	4946	5079	5211	4016 5344	5476	4282 5609	4415 5741	
328	5874	6006	6139	6271	6403	6535	6668	6800	6932	7064	132
329 330	7196	7328 8646	7460 8777	7592 8909	7724 9040	7855	79 ⁸ 7 9303	9434	8251 9566	838 ₂ 9697	131
331	9828	9959	90	.221	.353	.484	.615	.745	.876	1007	
332	521138	1269	1400	153o	1661	1792	1922	2053	2183	2314	,
333	2444 3746	2575 3876	2705 4006	2835 4136	2966 4266	3096 4396	3226 4526	3356 4656	3486 4785	3616 4915	130
335	5045	5174	5304	5434	5563	5693	5822	5951	6081	6210	129
336 337	6339	6469	6598 7888	6727	6856	6985	7114	7243	7372	7501	
338	7630 8917	77 ⁵ 9 9045	9174	8016 9302	8145 9430	8274 9559	8402 9687	8531 9815	866o 9943	8788	128
339	530200	0328	o456	o584	0712	0840	0968	1096	1223	1351	
34o 341	1479 275 4	1607 2882	1734 3009	1862 3136	1990 3264	2117 3391	2245 3518	2372 3645	2500 3772	262 7 3899	127
342	4026	4153	4280	4407	4534	4661	4787	4914	5041	5167	
343	5294	5421	5547	5674	5800	5927	6053	6180	6306	6432	126
344	6558 7819	6685 7945	6811 8071	6937 8197	7063 8322	7189 8448	7315 8574	7441 8699	7 567 8825	7693 8951	
346	9076	9202	9327	9452	9578	9703	9829	9954	79	.204	125
347	540329 1579	0455 1704	0580 1829	0705	0830 2078	0955.	1080 2327	1205 2452	1330 2576	1454 2701	
349	2825	2950	3074	3199	3323	3447	3571	3696	3820	3944	124
350	4068 5307	4192 5 431	4316 5555	4440 5678	4564 5802	4688 5925	4812	4936 6172	5060	5183	
352	6543	6666	6789	6913	7036	7159	6049 7282	7405	6296 7529	7652	123
353	7775	7898	8021	8144	8267	8389	8512	8635	8758	8881	123
354 355	9003	9126	9249	9371	9494	9616	9739	9861	9984	.106	
356	550228 1450	0351	0473 1694	0595	0717	0840 2060	0962 2181	1084 2303	1206 2425	1328 2547	122
357	2668	2790	2911	3033	3155	3276	3398	3519	3640	3762	121
358	3883 5094	4004 5215	4126 5336	4247 5457	4368 5578	4489 5699	4610 5820	473 1 5940	4852 6061	4973 6182	
360	6363	6423	6544	6664	6785	6905	7026	7146	7267	7387	120
361	7507	7627	7748	7868	7988	8108	8228	8349	8469	8589	- D
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ı si	134 H	13	27 26	40	54 53	67	80	94	107	121	
nce	130 E	13	20 26	40 39	52	66 65	79 78	92 91	106	119	
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Diff	126 d	13	25	38	5o	63	77 76	88	101	113	
	136 136 130 130 130 130 130 130 130 130 130 130	12 12	25 24	37 37	50 40	62 61	74 73	87 85	99 98	112	
	120	12	24	3 ₇ 36	49 48	60	72	84	96	108	
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	362	558709	8829	8948	9068	9188	9308	9428	9548	9667	9787	120
1	363	9907	26	.146	.265	.385	.504	.624	.743	.863	.982	
	364	561101	1221	1340	1459 2650	1578	1698	1817	1936 3125	2055 3244	2174 3362	119
	365 366	2293 3481	2412 3600	2531 3718	3837	2769 3955	2887 4074	3006 4192	4311	4429	4548	1
1	367	4666	4784	4903	5021	5139	5257	5376	5494	5612	5730	118
	368	5848	5966	6084	6202	6320	6437	6555	6673	6791	6909	
1	369 370	7026 8202	7144 8319	7262 8436	7 ³ 79 8554	7497 8671	7 614 8788	7732 8905	7849 9023	79 ⁶ 7 9140	8084 9257	117
	371	9374	9491	9608	9725	9842	9959	76	.193	.309	.426	/
1 :	372	570543	0660	0776	0893	1010	1126	1243	1359	1476	1592	
1 :	373	1709	1825	1942	2058	2174	2291	2407	2523	2639	2755	116
	374	2872	2988	3104	3220	3336	3452 4610	3568 4726	3684 4841	3800 4957	3915 5072	
	375 376	4031 5188	4147 53o3	4263 5419	4379 5534	4494 5650	5765	588o	5996	6111	6226	115
1:	377	6341	6457	6572	6687.	6802	6917	7032	7147	7262	7377	
	378	7492	7607	7722	7836	7951	8066	8181	8295 9441	8410	8525	/
	379 380	8639 9784	8754 9898	8868	8983	9097 .241	.355	9326 .469	.583	9555	9669 .811	114
	381	580925	1039	1153	1267	1381	1495	1608	1722	1835	1950]
, :	382	2063	2177	2291	2404	2518	2631	2745	2858	2972	3085	
	383	3199	3312	3426	3539	3652	3765	3879	3992	4105	4218	113
	384 385	4331 5461	4444 5574	4557 5686	4670 5 7 99	4783 5912	4896 6024	5009 6137	5122 6250	5235 6362	5348 6475	
	386	6587	6700	6812	6925	7037	7149	7262	7374	7486	7599	112
	387	7711	7823	7935	8047	8160	8272	8384	8496	8608	8720	
	388 389	8832 9950	8944	9056 .173	9167 .284	9279 .396	9391 .507	9503 .619	9615 •730	9726 .842	9838 .953	
	390	591065	1176	1287	1399	1510	1621	1732	1843	1955	2066	111
1:	391	2177	2288	2399	2510	2621	2732	2843	2954	3064	3175	
1 :	392	3286	3397	3508	3618	3729	3840	3950	4061	4171	4282	
	393 394	4393 5496	45o3 56o6	4614	4724 5827	4834 5937	4945 6047	5055	5165 6267	5276 6377	5386	110
	395	6597	6707	5717 6817	6927	7037	7146	7256	7366	7476	7586	
1:	396	7695	7805	7914	8024	8134	8243	8353	8462	8572	8681	
	397	8791	8900	9009	9119	9228	9337	9446	9556 .646	9665	9774	109
	398 399	9883 600973	9992 1082	101	1299	.319 1408	1517	1625	1734	.7 ⁵⁵	1951	
1 4	400	2060	2169	2277	2386	2494	2603	2711	2819	2928	3036	108
1 4	401	3144	3253	3361	3469	3577	3686	3794	3902	4010	4118	
	402	4226	4334	4442	4550	4658	4766	4874	4982	5089	5197	
	4o3 4o4	2085 188€	5413 6489	5521 6596	5628 6704	5736 6811	5844	5951 7026	6059 7133	6166	6274	107
	405	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419	. ,
4	406	8526	8633	8740	8847	8954	9061	9167	9274	9381	9488	
	407 408	9594 610660	9701	9808	9914	1086	1192	1298	.341 1405	1511	1617	106
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-			12	24	36	48	60	71	83	95	107	
		118	12	24	35	47	59	71	83	94	106	
1		117	12 12	23 23	35 35	47 46	59 58	70 70	82 81	94	105	
}	z	Parts.	12	23	35	46	58	69	8 r	92	104	4
	осе	114	11,	23	34	46	57	68	, 80	91	103	
	Differences.	Proportional	11	23	34	45	57	68	79	90	102	
İ)iff	112 tod	11	22	34	45 44	56 56	67 67	78 78	90 89	101	
	T	110 5	11	22	33	44	55	66	70	88	99	'
		109	11	22	33	44	55	65	76	87	98	
		108 107	11	22 2 I	32	43	54 54	65	76 75	86 86	97	
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409	611723	1829	1936	2042	2148	2254	2360	2466	2572	2678	106
410	2784	2890	2996 4053	3102 4159	320 7 4 2 64	3313 4370	3419	3525	3630	3736	
411	3842 4897	3947	5108	5213	5319	5424	4475 5529	4581 5634	4686 5740	4792 5845	105
413	5950	6055	6160	6265	6370	6476	6581	6686	6790	6895	100
414	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943	
415	8048 9093	9198	8257 9302	9406	8466 9511	8571 9615	8676	8780 9824	8884	8989	104
417	620136	0240	0344	0448	0552	0656	0760	0864	0968	1072	104
418	1176	1280	1384	1488	1592	1695	1799	1903	2007	2110	
419	2214	2318	2421	2525	2628	2732	2835	2939	3042	3146	
420	3249 4282	3353 4385	3456 4488	3559 4591	3663 4695	3766	3869	3973	4076	4179	103
422	5312	5415	5518	5621	5724	4798 5827	4901 5929	5004 6032	5107 6135	5210 6238	
423	634o	6443	6546	6648	6751	6853	6956	7058	7161	7263	
424	7366	7468	7571	7673	7775	7878	7980	8082	8185	8287	102
425	8389 9410	8491 9512	8593 9613	8695	8797 9817	9919	9002	9104	9206	9308	
427	630428	0530	0631	0733	ó835	0936	1038	1139	1241	1342	
428	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356	101
429	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367	
430	3468 4477	3569 4578	3670 4679	3771 4779	3872 4880	3973 4981	4074 5081	4175 5182	4276 5283	43 ₇ 6 5383	100
432	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388	100
433	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390	
434	7490 8489	7590 8589	7690 8689	7790 8789	7890 8888	7990 8988	8090 9088	9188	8290	8389 9387	00
436	9486	9586	9686	9785	9885	9984	84	.183	.283	.382	99
437	640481	ó581	ó68o	0779	6879	0978	1077	1177	1276	1375	
438	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366	
439	2465	2563	2662	2761	2860	2959	3058	3156	3255	3354	- 0
440	3453 4439	3551 4537	365o 4636	3749 4734	3847 4832	3946 4931	4044 5029	4143	4242 5226	4340 5324	98
442	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306	
443	6404	6502	6600	6698	6796	6894	6992	7089	7187	7285	
444 445	7383 8360	7481 8458	7579 8555	7676 8653	7774 8750	7872 8848	7969 8945	8067 9043	8165 9140	8262 9237	97
446	9335	9432	9530	9627	9724	9821	9919	16	.113	.210	,,
447	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181	
448	1278	1375	1472	1569	1666	1762	1859	1956	2053	2150	
449 450	2246 3213	2343 3309	2440 3405	2536 3502	2633 3598	2730 3695	2826 3791	2923 3888	3019 3984	3116 4080	96
451	4177	4273	4369	4465	4562	4658	4754	4850	4946	5042	90
452	5138	5235	533i	5427	5523	5619	5715	5810	5906	6002	
453 454	6098 7056	6194 7152	6290 7247	6386 7343	6482 7438	6577 7534	6673 7629	6769 7725	6864 7820	6960 7916	
455	8011	8107	8202	8298	8393	8488	8584	8679	8774	8870	95
456	8965	9060	9155	9250	9346	9441	9536	963i	9726	9821	11
457	9916	11	.106		.296	.391	.486	.581	.676	·771	-
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	106	II II	2 I 2 I	3 ₂ 3 ₂	42 42	53 53	64 63	74 74	85 84	95 95	1
	104	10	21	31	42	52	62	73	83	94 93	
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	97 64	10	19	29	39 38	49 48	58 58	68 67	78 77	87 86	
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İ	458	660865	0960	1055	1150	1245	1339	1434	1529	1623	1718	95
1	459	1813	1907	2002	2096	2191	2286	2380	2475	2569	2663	
1	460	2758	2852	2947	3041	3135	3230	3324	3418	3512	3607	94
i	461	3701	3795	3889	3983	4078	4172	4266	4360	4454	4548	
	462	4642	4736	4830	4924	5018	5112	5206	5299	5393	5487	
ĺ	463 464	558 1 6518	5675	5769 6705	5862 6799	5956 6892	6050	6143 7079	6237 7173	6331 7266	6424 7360	
1	465	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293	y3
1	466	8386	8479	8572	8665	8759	8852	8945	9038	9131	9224	
1	467	9317	9410	9503	9596	9689	9782	9875	9967	60	.153	
1	468	670246	0339	o431	0524	0617	0710	0802	0895	0988	1080	
	469	1173	1265	1358	1451	1543	1636	1728	1821	1913	2005	
1	470	2098	2190	2283	2375	2467	2560	2652	2744	2836	2929	92
1	471	3021	3113	3205	3297	(3390	3482	3574	3666	3758	385o	
١	472	3942	4034	4126	4218	4310	4402	4494	4586	4677	4769	
ı	473	4861 5==8	4953	5045 5962	5137 6053	5228 6145	5320 6236	5412 6328	5503 6419	5595 6511	5687 6602	
1	474 475	5778 6694	5870 6785	6876	6968	7059	7151	7242	7,333	7424	7516	91
	476	7607	7698	7789	7881	7972	8063	8154	8245	8336	8427	۱ ۲۰
1	477	8518	8609	8700	8791	8882	8973	9064	9155	9246	9337	
1	478	9428	9519	9610	9700	9791	9882	9973	63	.154	.245	1
1	479	680336	0426	0517	0607	0698	0789	0879	0970	1060	1151	
1	480	1241	1332	1422	1513	16ó3	1693	1784	1874	1964	2055	90
1	481	2145	2235	2326	2416	2506	2596	2686	2777	2867	2957	-
1	482	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857	.
1	483	3947	4037	4127	4217	4307	4396	4486	4576	4666	4756	
	484 485	4845 5742	4935 5831	5025 5921	5114 6010	5204 6100	5294 6189	5383 6279	5473 6368	5563 6458	5652 6547	89
1	486	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440	9
ı	487	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331	
ł	488	8420	8509	8598	8687	8776	8865	8953	9042	9131	9220	
1	489	9309	9398	9486	9575	9664	9753	9841	9930	19	.107	i
	490	690196	0285	6373	0462	o550	0639	0728	0816	0905	0993	\
	491	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877	88
I	492	1965	2053	2142	2230	2318	2406	2494	2583	2671	2759	
	493	2847	2935	3023 3903	3111	3199	3287	3375	3463	3551	3639	
	494 495	3727 4605	3815 4693	4781	3991 4868	4078 4956	4166 5044	4254 5131	4342 5219	4430 5307	4517 5394	
1	496	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269	87
	497	6356	6444	653i	6618	6706	6793	688o	6968	7055	7142	,
	498	7229	7317	7404	7491	7578	7665	7752	7839	7926	8014	
	499	8101	8188	8275	8362	8449	8535	8622	8709	8796	8883	
1	500	8970	9057	9144	9231	9317	9404	9491	9578	9664	9751	
1	501	9838	9924	11	08	.184	.271	.358	.444	.531	.617	20
1	502 503	700704	0790	0877	c963	1050	1136	1222	1309	1395	1482	36
1	504	1568 2431	1654 2517	1741 2603	1827 2689	1913	1999 2861	2086 2947	3033	2258 3119	2344 3205	
1	505	3291	3377	3463	3549	3635	3721	3807	3893	3979	4065	
1	506	4151	4236	4322	4408	4494	4579	4665	475ı	4837	4922	1
L	507	5008	5094	5179	5265	535o	5436	5522	5607	5693	5778	
5	N.	0	1	2	3	4	5	6	7	8	9	D.
1	7	95	10	19	29	38	48	57	67	76	86	
		94 strs.	9	19	28	38	47	56	66	75	85	
1	υ'n	93 E	9	19 18	28 28	3 ₇ 3 ₇	47 46	56 55	65 64	74 74	84 83	ļ
-	nce	92 7	9	18	27	36	46	55	64	74 73	82	
-	Differences.	· · · · · · · · · · · · · · · · · · ·		18		36	45					
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1	A	89 30 30 30 30 30 30 30 30 30 30 30 30 30	9	18	26	35	44	53	62	71 70	79	
	_	87 Å	9	17	26	35	44	52	6 r	70	78	
1		86	ģ	17	26	34	43	52	6 0	69	77	
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508	705864	5949	6035	6120	6206	6291	6376	6462	6547	6632	85
509	6718	68o3	6888	6974	7059	7144	7229	7315	7400	7485	
510	7570	7655	7740	7826 8676	7911 8761	7996 8846	8081	8166	8251	8336	
511 512	8421 9270	85o6 9355	8591 9440	9524	9609	9694	8931 9779	9015	9100	9185	
513	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879	
514	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723	84
5 15	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566	
516	2650	2734	2818 365g	2902	2986	3070	3154	3238	3323	3407	
517	3491	3575	•	3742	3826	3910	3994	4078	4162	4246	
518 519	4330 5167	4414 5251	4497 5335	4581 5418	4665 5502	4749 5586	4833 5669	4916 5753	5000 5836	5084 5920	
520	6003	6087	6170	6254	6337	6421	6504	6588	6671	6754	83
521	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587	
522	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419	
523	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248	
524 525	9331 720159	9414	9497 0325	9580 0407	9663 0490	9745 0573	9828 0655	9911	9994 0821	•• 7 7	
526	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728	82
527	1811	1893	1975	2058	2140	2222	2305	2387	2469	2552	
528	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374	
529	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194	
53o	4276	4358	4440	4522	4604	4685	4767	4849	4931	5013	
531	5095	5176	5258	5340	5422	55c3	5585	5667	5748	5830	
532 533	5912	5993	6075 6890	6156	6238	6320	6401	6483	6564	6646 7460	81
534	6727 7541	6809 7623	7704	6972. 7785	7053 7866	7948	7216	7297 8110	7379 8191	8273	01
535	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084	
536	9165	9246	9327	9408	9489	9570	9651	9732	9813	9893	
537	9974	55	.136	.217	.298	.378	.459	.540	.621	.702	•
538	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508	
539	1589 2394	1669	1750 2555	183 o 2635	1911	1991	2072 2876	2152 2956	2233 3037	2 313	80
540 541	3197	2474 3278	3358	3438	2715 3518	2796 3598	3679	3759	3839	3919	- 00
542	3999	4079	4160	4240	4320	4400	4480	4560	464o	4720	
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519	
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317	
545 546	6397	6476 7272	6556 7352	6635 7431	6715 7511	6795 7590	6874 7670	6954 7749	7034 7829	7113 7908	7 9
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701	/ 7
548	8781	886o	8939	9018	9097	9177	9256	9335	9414	9493	
549	9572	9651	9731	9810	9889	9968	47	.126	.205	.284	
55o	74 o 363	0442	0521	0600	ó678	0757	0836	0915	0994	1073	
551	1152	1230	1309	1388	1467	1546	1624	1703	1782	1860	
552 553	1939	2018 2804	2096 2882	2175	2254 3039	2332 3118	2411 3196	2489 3275	2568 3353	2647 3431	78
554	2725 3510	3588	3667	3745	3823	3902	3980	4058	4136	4215	,,
555	4293	4371	4449	4528	4606	4684	4762	4840	4919	4997	
556	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777	
557 558	5855 6634	5933	6790	6089 6868	6167 6945	6245 7023	6323	6401 7179	6479 7256	7334	
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	86	9	=7	26	34	43	52	60	69	77	
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enc	82 1	8	17	25	33	41	49	57	66	74	
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	79 H	8	16	23	31	39	47	55	62	70	

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559	747412	7489	7567	7645	7722	7800	7878	7955	8033	8110	78
56o	8188	8266	8343	8421	8498	8576	8653	8731	8808	8885	777
561	8963	9040	9118	9195	9272	9350	9427	9504	9582 .354	9659 •43	}
562	9736 750508	9814 0586	9891 0663	9968 0740	0817	0894	.200 0971	·277 1048	1125	1202	1
564	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972	
565	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740	
566 567	2816 3583	289 3 3660	2970 3736	3047 3813	3123 3889	3200 3966	3277 4042	3353	3430 4195	3506 4272	4
568	4348	4425	4501	4578	4654	4730	4807	4883	4960	5036	76
569	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799	
570	5875	595i	6027	6103	6180	6256	6332	6408	6484	656o	
571	6636	6712	6788 7548	6864 7624	6940	7016	7092 7851	7168	7244 8003	7320 8079	
572 573	7396 8155	7472 8230	8306	8382	7700 8458	8533	8609	8685	8761	8836	
574	8912	8988	9063	9139	9214	9290	9366	9441	9517	9592	_
575	9668	9743	9819	9894	9970	45	0875	.196 0950	.272 1025	.347	75
5 ₇ 6	760422 1176	0498 1251	0573 1326	0649 1402	0724	0799 1552	1627	1702	1778	1853	
578	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604	
579	, 2679	2754	2829	2904	2978	3053	3128	3203	3278	3353	
580 581	3428	35o3 4251	3578 4326	3653 4400	3727 4475	3802 4550	3877 4624	3952 4699	4027 4774	4101 4848	1
582	4176 4923	4998	5072	5147	5221	5296	5370	5445	5520	5594	
583	5669	5743	5818	5892	5966	6041	6115	6190	6264	6338	74
584	6413	6487 7230	6562	6636	6710 7453	6785	6859	6933	7007	7082 7823	
585 586	7156 7898	7972	7304 8046	7 ³ 79 8120	8194	7527 8268	7601 8342	8416	7749 8490	8564	
587	8638	8712	8786	886o	8934	9008	9082	9156	9230	9303	
588	9377	9451	9525	9599	9673	9746	9820	9894	9968	42	
589	770115	0189	0263	0336	0410	0484	0557	0631	0705	0778	Ì
590 591	0852 1587	0926 1661	0999 1734	1073 1808	1146 1881	1220	1293	1367	1440	1514	73
592	2322	2395	2468	2542	2615	2688	2762	2835	2908	2081	,
593	3055	3128	3201	3274	3348	3421	3494	3567	3640	3713	
594 595	3786 4517	386 o 4590	3933 4663	4006 4736	40 7 9 4809	4152	4225 4955	4298 5028	4371	4444 5173	
596	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902	
597	5974 6701	6047 6774	6120 6846	6193	6265 6992	6338	6411	6483	6556	6629	
1 1				' '		1 '		1	8006	*	70
599 600	7427 8151	7499 8224	7572 8296	7644 8368	7717 8441	77 ⁸ 9 8513	7862 8585	7934 8658	8730	8079 88 0 2	72
601	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524	
602 603	9596 780317	9669 0389	9741 0461	9813 0533	9885 0605	9957	0749	0821	0893	0965	
604	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684	
605	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401	
606 607	2473 3180	2544 3260	2616 3332	2688 3403	2759 3475	2831 3546	2902 3618	2974 3689	3046 3761	3117 3832	71
608	3189	3975	4046	4118	4189	4261	4332	4403	4475	4546	7 1
609	4617	4689	4760	4831	4902	4974	5045	5116	5187	5259	
610	533o	5401	5472	5543	5615	5686	5757	5828	5899	5970	
611	6041	6112		6254	6325	6396	6467	6538	6609	6680	
N.	0	8	15	3	31	39	6 46	54	$\frac{8}{62}$	9 69	D.
38.	77 75 75 Parts.	8	15	23	30	38	46	53	61	68	
nce		8	15	23	30	38	45	53	60	68	
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	71 ~	7	14	21	28	36	43	5o	57	64	

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612	786751	6822	6893		7035	7106	7177	7248	7319	7390	71
613	7460		7602	7673	7744	7815	7885	7956	8027	8098	'
614 615	8168 8875	8239	9016	8381 9087	9157	8522	8593	8663	8734	8804	
616	9581	9651	9722	9792	9863	9228	9299	9369	9440		
617	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918	70
618	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620	
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322	
620	2392	2462	2532	2602	2672	2742	2812	2882	2952	3022	
€21	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721	1
622	3790	386o	3930	4000	4070	4139	4209	4279	4349	4418	
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115	
624	5185	5254		5393	5463	5532	5602	5672	5741	5811	
625	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505	69
626	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198	
627 628	7268	7337	7406 8098	7475	7545	7614	7683	7752	7821	7890	
629	7960 8651	8029	8789	8167	8236	8305	8374	8443	8513	8582	
630	9341	9409	9478	9547	8927 [.] 9616	8996 9685	9065	9134	9203	9272	
631	800029	0098	0167	0236	0305	0373	0442	9023	0580	9961 0648	
632	_	0786	0854			H			1		
633	0717 1404	1472	1541	1609	0992 1678	1061	1129	1198	1266	1335	
634	2089	2158	2226	2295	2363	2432	2500	188J 2568	1952 2637	2021 2705	
635	2774	2842	2010	2979	3047	3116	3184	3252	3321	3389	68
636	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071	
637	4139	4208	4276	4344	4412	4480	4548	4616	4685	4753	
638	482î	4889	4957	5025	5093	5161	5229	5297	5365	5433	
639	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112	
640 641	6180 6858	6248	6316	6384	6451	6519	6587	6655	6723	6790	
541 542	6858 7535	6926 7603	6994	7061 7738	7129	7197	7264	7332	7400	7467	
643	7333 8211	8279	7670 8346	7738 8414	7806 8481	7873 8549	7941 8616	8008 8684	8076 8751	8143 8818	6-
544	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492	67
645	9560	9627	9694	9762	9829	9896	9964	31	98	.165	
546	810233	0300	0367	0434	0501	0569	0636	0703	0770	0837	
647	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508	
648	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178	
349	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847	
550	2913	2980	3047	3114	3181	3247	3314	3381	3448	3514	
551	3581	3648	3714	3781	3848	3914	3981	4048	4114	4181	
552	4248	4314	4381	4447	4514	4581	4647	4714	4780	4847	
553 554	4913	4980	5046	5113	5179	5246	5312	5378	5445	5511	66
555	5578 6241	5644 6308	5711 6374	5777 6440	5843 6506	5910 6573	5976 6639	6042 6705	6109	6175 6838	
556	6904	6970	7036	7102	7169	7235	7301	7367	6771 7433	7499	
57	7565	7631	7698	7764	7830	7896	7962	8028	8094	8160	
58	8226	8292	8358	8424	8490	8556	8622	8688	8754	8820	
59	8885	8951	9017	9083	0140	0215	0281	9346	9412	9478	
60	9544	9610	\$676	9741	9807	9873	9939	4	70	.136	
61	820201	0267	o333	0399	0464	0530	0595	0661	0727	0792	
662	0858	0924	0989	1055	1120	1186	1251	1317	1382	1448	cr
64	1514	1579 2233	1645	1710 2364	1775 2430	1841 2495	1906 2560	1972 2626	2037 2691	2103 2756	65
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<u>'</u>	1	7	14	21	28	36	43	5o	57	64	
ses	70 E	7	14	21	28	35	42	49 48	56	63	
ou	69 64	7	14	21	28	35	41		55	62	
Differences.	Propor. Parts.	7	14	20	27	34	41	48	54 54	61 60	
91	66 8	7 7	13	20	27 26	33	40 40	47 46	53	59	
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665	822822	2887	2952	3018	3083	3148	3213	3279	3344	3409	65
666	3474	3539	3605	3670	3735	3800	3865	3930	3996	4061	
667	4126	4841	4256	4321	4386 5o36	4451 5101	4516 5166	4581 5231	4646 5296	4711 5361	
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670	6075	6140	6204	6269	6334	6399	6464	6528	6593	6658 7305	
671	6723 7369	6787	6852	6917 7563	6981	7046 7692	7111	7175 7821	7240 7886	7951	
673	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595	64
674	8660	8724	8789	8853	8918	8982	9046	9111	9175	9239	
675	9304	9368	9432	9497	9561	9625	9690	9754	9818	9882	
676 677	9947	0653	0717	0781	0845	0909	0973	1037	.460	.525 1166	
678	1230	1294	1358	1422	1486	155o	1614	1678	1742	1806	
679 680	1870 2500	1934 2573	1998 2637	2062 2700	2126 2764	2189 2828	2253	2317 2956	3020	2445 3083	
681	3147	3211	3275	3338	3402	3466	3530	3593	3657	3721	
682	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357	
683 684	4421 5056	4484 5 1 20	4548 5183	4611 5247	4675 5310	4739 5373	4802 5437	4866 5500	4929 5564	4993 5627	63
685	5691	5754	5817	5881	5944	6007	6071	6134	6197	6261	
686	6324	6387	6451	6514	6577	6641	6704	6767	6830	6894	
687	6957	7020	7083	7146	7210	7273	7336	7399	7462	7525	
688 689	7588 8210	7652 8282	7715 8345	7778 8408	7841 8471	7904 8534	7967 8597	8030 8660	8093 8723	8156 8786	
690	8849	8912	8975	9038	9101	9164	9227	9289	9352	9415	
691	9478	9541	9604	9667	9729	9792	9855	9918	9981	43	
692 693	840106 0733	0169	0232	0294	0357 0984	1046	0482	0545	1234	0671	
694	. 1359	1422	1485	1547	1610	1672	1735	1797	1860	1922	,
695	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547	61
696 697	2609 3233	2672 3295	2734 3357	2796 3420	2859 3482	2921 3544	2983 3606	366g	3108 3731	3170 3793	
698	3855	3918	3980	4042	4104	4166	4229	4291	4353	4415	
699	4477	4539	4601	4664	4726	4788	4850	4912	4974 5594	5036	
700 701	5098	5160 5780	5222 5842	5284 5904	5346 5966	5408 6028	5470 6090	5532 6151	6213	5656 6275	
702	6337	6399	646 1	6523	6585	6646	6708	6770	6832	6894	
703 7 04	6955 7573	7017 7634	7079 7696	7141	7202 7819	7264	7326 7943	7388 8004	7449 8066	7511 8128	
705	8189	8251	8312	8374	8435	8497	8559	8620	8682	8743	ł
706	8805	8866	8928	8989	905 I	9112	9174	9235	9297	9358	6 r
707	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972	J
708 709	850033 0646	0095	0156 0769	0217 0830	0279 0891	0340	0401 1014	0462 1075	0524 1136	0585	
710	1258	1320	1381	1442	1503	1564	1625	1686	1747	1809	
711	1870 2480	1931 2541	1992 2602	2053 2663	2114	2175 2785	2236 2846	2297 2907	2358 2968	2419 3029	
712 713	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637	
714	3698	3759	3820	3881	3941	4002	4063	4124	4185	4245	İ
715	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852	
716	4913 5519	4974 5580	5034 5640	5095 5701	5156 5761	5216 5822	5277 5882	5337 5943	5398 6003	5459 6064	
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668	60
719 N.	6729	6789 1	685o	6910	6970	7031 5	7091	7152	7212	7272	D.
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720 721 722 723 724	857332 7935 8537 9138 9739	7393 7995 8597 9198 9799	7453 8056 8657 9258 9859	7513 8116 8718 9318 9918	7574 8176 8778 9379 9978	7634 8236 8838 9439 38	7694 8297 8898 9499	7755 8357 8958 9559	7815 8417 9018 9619	7875 8477 9078 9679	60
725 726 727 728 729	866338 0937 1534 2131 2728	0398 0996 1594 2191 2787	0458 1056 1654 2251 2847	0518 1116 1714 2310 2906	0578 1176 1773 2370 2966	0637 1236 1833 2430 3025	0697 1295 1893 2489 3085	0757 1355 1952 2549 3144	0817 1415 2012 2608 3204	0877 1475 2072 2668 3263	-
730 731 732 733 734 735 736 737 738 739	3323 3917 4511 5104 5696 6287 6878 7467 8056 8644	3382 3977 4570 5163 5755 6346 6937 7526 8115 8703	3442 4036 4630 5222 5814 6405 6996 7585 8174 8762	3501 4096 4689 5282 5874 6465 7055 7644 8233 8821	3561 4155 4748 5341 5933 6524 7114 7703 8292 8879	3620 4214 4808 5400 5992 6583 7173 7762 8350 8938	3680 4274 4867 5459 6051 6642 7232 7821 8409 8997	3739 4333 4926 5519 6110 6701 7291 7880 8468 9056	3799 4392 4985 5578 6169 6760 7350 7939 8527 9114	3858 4452 5045 5637 6228 6819 7409 7998 8586 9173	59
740 741 742 743 744 745 746 747 748 749	9232 9818 870404 0989 1573 2156 2739 3321 3902 4482	9290 9877 0462 1047 1631 2215 2797 3379 3960 4540		9408 9994 0579 1164 1748 2331 2913 3495 4076 4656	9466 53 .0638 1223 1806 2389 2972 3553 4134 4714	9525 .111 .0696 1281 1865 2448 3030 3611 4192 4772	9584 .170 0755 1339 1923 2506 3088 3669 4250 4830	9642 .228 0813 1398 1981 2564 3146 3727 4308 4888	9701 •287 0872 •456 2040 2622 3204 3785 4366 4945	9760 .345 .0930 .1515 .2098 .2681 .3262 .3844 .4424 .5003	58
750 751 752 753 754 755 756 757 758 759	5061 5640 6218 6795 7371 7947 8522 9096 9663	5119 5698 6276 6853 7429 8004 8579 9153 9726 0299	5177 5756 6333 6910 7487 8062 8637 9211 9784 0356	5235 5813 6391 6968 7544 8119 8694 9268 9841 0413	5293 5871 6449 7026 7602 8177 8752 9325 9898 0471	5351 5929 6507 7083 7659 8234 8809 9383 9956 0528	5409 5987 6564 7141 7717 8292 8866 9440 13 0585	5466 6045 6622 7199 7774 8349 8924 9497 70 0642	5524 6102 6680 7256 7832 8407 8981 9555 .127 0699	5582 6160 6737 7314 7889 8464 9039 9612 .185 0756	5 7
760 761 762 763 764 765 766 767 768 769	0814 1385 1955 2525 3093 3661 4229 4795 5361	0871 1442 2012 2581 3150 3718 4285 4852 5418 5983	0928 1499 2069 2638 3207 3775 4342 4909 5474 6039	0985 1556 2126 2695 3264 3832 4399 4965 5531 6096	1042 1613 2183 2752 3321 3888 4455 5022 5587 6152	1099 1670 2240 2809 3377 3945 4512 5078 5644 6209	1156 1727 2297 2866 3434 4002 4569 5135 5700 6265	1213 1784 2354 2923 3491 4059 4625 5192 5757 6321	1271 1841 2411 2980 3548 4115 4682 5248 5813 6378	1328 1898 2468 3037 3605 4172 4739 5305 5870 6434	56
770 771 772 773 774	6491 7 054 761 7 8179 8741	6547 7111 7674 8236 8797	6604 7167 7730 8292 8853	6660 7223 7786 8348 8909	6716 7280 7842 8404 8965	6773 7336 7898 8460 9021	6829 7392 7955 8516 9077	6885 7449 8011 8573 9134	6942 7505 8067 8629 9190	6998 7561 8123 8685 9246	
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775 776 777 778 779 780 781 782 783 784	889302 9862 890421 0980 1537 2095 2651 3207 3762 4316		9414 9974 0533 1091 1649 2206 2762 3318 3873 4427	9470 30 0589 1147 1705 2262 2818 3373 3928 4482	9526 86 0645 1203 1760 2317 2873 3429 3984 4538	9582 .141 0700 1259 1816 2373 2929 3484 4039 4593	9638 .197 0756 1314 1872 2429 2985 3540 4094 4648	9694 .253 0812 1370 1928 2484 3040 3595 4150 4704	9750 .309 0868 1426 1983 2540 3096 3651 4205 4759	9806 .365 0924 1482 2039 2595 3151 3706 4261 4814	56
785 786 787 788 789 790 791 792 793	4870 5423 5975 6526 7077 7627 8176 8725 9273 9821	4925 5478 6030 6581 7132 7682 8231 8780 9328 9875	4980 5533 6085 6636 7187 7737 8286 8835 9383 9930	5036 5588 6140 6692 7242 7792 8341 8890 9437 9985	5091 5644 6195 6747 7297 7847 8396 8944 9492 39	5146 5699 6251 6802 7352 7902 8451 8999 9547 ••94	5201 5754 6306 6857 7407 7957 8506 9054 9602	5257 5809 6361 6912 7462 8012 8561 9109 9656	5312 5864 6416 6967 7517 8067 8615 9164 9711 .258	5367 5920 6471 7022 7572 8122 8670 9218 9766 .312	
795 796 797 798 799 800 801 802 803 804	900367 0913 1458 2003 2547 3090 3633 4174 4716 5256	0422 0968 1513 2057 2601 3144 3687 4229 4770 5310	0476 1022 1567 2112 2655 3199 3741 4283 4824 5364	0531 1077 1622 2166 2710 3253 3795 4337 4878 5418	0586 1131 1676 2221 2764 3307 3849 4391 4932 5472	0640 1186 1731 2275 2818 3361 3904 4445 4986 5526	0695 1240 1785 2329 2873 3416 3958 4499 5040 5580	0749 1295 1840 2384 2927 3470 4012 4553 5094 5634	0804 1349 1894 2438 2981 3524 4066 4607 5148 5688	0859 1404 1948 2492 3036 3578 4120 4661 5202 5742	54
805 806 807 808 809 810 811 812 813	5796 6335 6874 7411 7949 8485 9021 9556 910091 0624	5850 6389 6927 7465 8002 8539 9074 9610 0144 0678	5904 6443 6981 7519 8056 8592 9128 9663 0197 0731	5958 6497 7035 7573 8110 8646 9181 9716 0251 0784	6012 6551 7089 7626 8163 8699 9235 9770 0304 0838	6066 6604 7143 7680 8217 8753 9289 9823 0358 0891	6119 6658 7196 7734 8270 8807 9342 9877 0411	6173 6712 7250 7787 8324 8860 9396 9464 998	6227 6766 7304 7841 8378 8914 9449 9984 0518 1051	6281 6820 7358 7895 8431 8967 9503 37 0571 1104	53
815 816 817 818 819 820 821 822 823 824	1158 1690 2222 2753 3284 3814 4343 4872 5400 5927	1211 1743 2275 2806 3337 3867 4396 4925 5453 5980	1264 1797 2328 2859 3390 3920 4449 4977 5505 6033	1317 1850 2381 2913 3443 3973 4502 5030 5558 6085	1371 1903 2435 2966 3496 4026 4555 5083 5611 6138	1424 1956 2488 3019 3549 4079 4608 5136 5664 6191	1477 2009 2541 3072 3602 4132 4660 5189 5716 6243	1530 2063 2594 3125 3655 4184 4713 5241 5769 6296	1584 2116 2647 3178 3708 4237 4766 5294 5822 6349	1637 2169 2700 3231 3761 4290 4819 5347 5875 6401	
825 826 827 828 829 830	6454 6980 7506 8030 8555 9078	6507 7033 7558 8083 8607 9130	6559 7085 7611 8135 8659 9183	6612 7138 7663 8188 8712 9235	6664 7190 7716 8240 8764 9287	6717 7243 7768 8293 8816 9340	6770 7295 7820 8345 8869 9392	6822 7348 7873 8397 8921 9444	6875 7400 7925 8450 8973 9496	6927 7453 7978 8502 9026 9549	52
N.	0	1	2	3	4	5	6	7	8	9	D.
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831 832	919601	9653 0176	9706 0228	9758 0280	9810 0332	9862 0384	9914 0436	9967 0489	0541	0593	52
833	0645	0697	0749	0801	0853	0906 1426	0958	1010	1062 1582	1114	
834	1166 1686	12.8	1270	1322 1842	1374	1946	1998	2050	2102	2154	
836	2206	2258	2310	2362	2414	2466	2518	2570	2622	2674	
837	2725 3244	2777 3296	2829 3348	2881 3399	2933 3451	2985 3503	3037 3555	3089 3607	3140 3658	3192	
839	3762	3814	3865	3917	3969	4021	4072	4124	4176	4228	
840	4279	4331	4383	4434	4486	4538	4589	4641	4693	4744	
841	4796	4848	4899	4951	5003	5054	5106	5157	5209	5261	
842 843	5312 5828	5364 5879	5415 5931	5467 5982	5518 6034	5 5 70 6085	5621 6137	5673 6188	5725 6240	5776 6291	51
844	6342	6394	6445	6497	6548	6600	665ı	6702	6754	6805	••
845	6857	6908	6959	7011	7062	7114	7165	7216	7268	7319	
846	7 ³ 70 7883	7422 7935	7473 7986	7524 8037	7576 8088	7627 8140	7678 8191	7730 824 2	7781 8293	7832 8345	
848	8396	8447	8498	8549	8601	8652	8703	8754	8805	8857	
849	8908	8959	9010	906i	9112	9163	9215	9266	9317	9368	
850	9419	9470	9521	9572	9623	9674	9725	9776	9827	9879	
851	9930	9981	32	83	.134	.185	.236	.287	0847	.389 $.0898 $	
852 853	930 4 40 0949	0491	0542 1051	0592	o643 1153	0694	0745	0796 1305	1356	1407	
854	1458	1509	156o		1661	1712	1763	1814	1865	1915	
855	1966	2017	2068	2118	2169	2220	2271	2322	2372	2423 2930	
856 857	2474 2981	2524 3031	2575 3082	2626 3133	2677 3183	3234	2778 3285	2829 3335	2879 3386	3437	
858	3487	3538	3589	3639	3690	3740	3791	3841	3892	3943	
859	3993	4044	4094	4145 4650	4195	4246	4296 4801	4347 4852	4397	4448 4953	50
860	4498	4549	4599		4700	4751	5306	5356	· ·	5457	30
861	5003 5507	5054 5558	5104 5608	5154 5658	5205 5709	5255 5759	5809	586o	5406 5910	5960	
863	6011	6061	6111	6162	6212	6262	6313	6363	6413	6463	
864	6514	6564	6614	6665	6715	6765	6815	6865 7367	6916	6966 7468	
865	7016 7518	7066 7568	7117	7167	7217	7267	7317	7869	7919	7969	
867	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470	
868	8520	8570	8620	8670	8720	8770	9320	9369	9419	8970 9469	
869	9020 9519	9070 9569	9120	9170	9220 9719	9270	9819	9869	9918	9968	
871	940018	0068	0118	0168	0218	0267	0317	0367	0417	0467	
872	0516	0566	0616	0666	0716	0765	0815	0865	0915	0964	
873	1014	1064	1114	1163	1213	1263	1313	1362	1412	1462	
874 875	1511	1561	1611	1660	1710 2207	1760 2256	1809	1859	1909	2455	
876	2504	2554	2603	2653	2702	2752	2801	2851	2901	2950	
877	3000	3049	3099	3148	3198	3247 3742	3297	3346	3396 3890	3445 3939	49
878 879	3495 3989	3544 4o38	3593 4088	3643	3692 4186	4236	4285	4335	4384	4433	
880	4483	4532	4581	4631	468o	4729	4779	4828	4877	4927	
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419	
882	5469	5518	5567	5616	5665 6157	5715	5764 6256	5813 6305	586 ₂ 6354	5912 6403	
883 884	5961 6452	6501	6059	6600	6649	6207 6698	6747	6796	6845	6894	
885	6943	6992	7041	7090	7140	7189	7238	7287	7336	7385	
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875	T.
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j ::	50 A Parts.	$\begin{cases} 5 \\ 5 \end{cases}$	10	16	21	26 26	31	36	42	47 46	
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887	947924 8413	797 ³ 846 ₂	8022 8511	8070 8560	8119	8168 8657	8217	8266 8755	8315 8804	8364 8853	49
889	8902	8951	8999	9048	9097	9146	9195	9244	9292 9780	9341	
891	9390 9878	9439	9488	9536	9585	9634	9683	9731	.267	9829	
892	950365	0414	0462	0511	0560 1046	0608	0657	0706	1240	0803	
894 895	1338	1386	1435	1483	1532	1580 2066	1629	1677	1726	1775 2260	48
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744	40
897	2792 3276	2841 3325	2889 3373	2938 3421	2986 3470	3o34 3518	3o83 3566	3131 3615	3180 3663	3228 3711	
899	3760	3808	3856	3905	3953	4001	4049	4098	4146	4194	
900	4243	4291	4339	4387	4435	4484	4532 5014	4580 5062	4628 5110	4677 5158	
902	5207 5688	5255 5736	53o3 5784	535í 5832	5399 5880	5447 5928	5495 5976	5543 6024	5592 6072	5640 6120	
904	6168	6216	6265	6313	636ı	6409	6457	6505	6553	6601	
905	6649	6697 7176	6745	6793 7272	6840 7320	6888 7368	6936 7416	6984 7464	7032	7080 7559	
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038	
908	8086 8564	8134	8181	8229 8707	8277 8755	8325 8803	8373 8850	8421 8898	8468 8946	8516 8994	
910	9041	9089 9566	9137 9614	9185 9661	9232 9 7 09	9280 9757	9328 9804	9375 9852	9423 9900	9471 9947	
912	9995	42	90	.138	.185	.233	.280	.328	.376	.423	
913	960471 0946	0518	0566 1041	1089	0661	0709	0756 1231	0804 1279	0851 1326	0899 1374	47
915 916	1421 1895	1469	1516	1563 2038	1611 2085	1658	1706 2180	1753 2227	1801 2275	1848	
917	2369	2417	2464	2511	2559	2606	2653	2701	2748	2795	
918	2843 3316	2890 3363	2937 3410	2985 3457	3032 3504	3079 3552	3126 3599	3174 3646	3221 3693	3268 3741	
920	3788	3835	3882	3929	3977	4024	4071	4118	4165	4212	
921	4260 4731	4307 4778	4354 4825	4401 4872	4448	4495 4966	4542 5013	4590 5061	4637 5108	4684 5155	
923	5202 5672	5249 5719	5296 5766	5343	5390 5860	5437 5907	5484 5954	5531 6001	5578 6048	5625 6095	
925	6142 6611	6189 6658	6236 6705	6283 6752	6329 6799	6376 6845	6423 6892	6470 6939	6517 6986	6564 7033	
927	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501	
928	7548 8016	7595 8062	7642 8100	7688 8156	7735 8203	7782 8240	7829 8296	7875 8343	7922	7969 8436	
929	8483	853o	8576	8623	8670	8716	8763	8810	8390 8856	8903	
931	8950 9416	8996 9463	9043 9509	9090	9136	9183 9649	9229	9276	9323 9789	9369 9835	
933 934	9882 970347	9928 0393	9975	0486	68 o533	0579	.161 0626	.207 0672	.254	.300	46
935	0812	o858	0904	0951	0997	1044	1090	1137	1183	1229	40
936	1276	1322	1369	1415	1461	1508	1554 2018	2064	1647 2110	1693	
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619	Í
939	2666 3128	2712 3174	2758 3220	2804 3266	285 r 33 r 3	2897 3359	2943 3405	2989 3451	3o35 3497	3082 3543	
941 942	3590 4051	3636 4097	368 ₂ 4143	3728 4189	3774 4235	3820 4281	3866 4327	3913 4374	3959 4420	4005 4466	
943	4512	4558	4604	4656	4696	4742	4788	4834	488o	4926	
N.	0	5	2	3	4	5	6	7	8	9	D.
Differ.	48 s { 47 S }	5	10	14	19	24 24	29 28	34 33	38 38	43 42	
0	<u> 46 من ا</u>	5	9	14	18	23	28	32	37	41	

N.	0	1	2	3	4	5	6	7	8	9	D
944	974972 5432	5018 5478	5064 5524	5110 5570	5156 5616	5202 5662	5248 5707	5294 5753	5340 5799	5386 5845	46
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304	
947	635o	6396	6442	6488	6533	6579	6625	6671	6717	6763	
948	6808 7266	6854 7312	6900 7358	6946 7403	6992 7449	7037 7495	7083 7541	7129 7586	7175 7632	7220 7678	
950	7724	7769	7815	7861	7906	7952	7998	8043	8089	8135	
951	8181	8226	8272	8317	8363	8409	8454	8500	8546	8591	
952	863 7 909 3	8683 q138	8728 9184	8774 9230	8819 9275.	8865 9321	8911 936 6	8956 9412	9002 9457	9047 9503	
954	9548	9594	9639	9685	9730	1 .	9821	9867		9958	
955	980003	00.19	0094	0140	0185	9776	0276	0322	9912 0367	0412	45
956	0458	0503	0549	0594	0640	o685	0730	0776	0821	0867	
957 958	1366	0957	1003	1048 1501	1093 1547	1139	1184	1229	1275	1320	
959	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226	
960	2271	2316	2362	2407	2452	2497	2543	2588	2633	2678	
961	2723 3175	2769 3220	2814 3265	2859 3310	2904 3356	2949 3401	2994	3040	3o85 3536	3130 3581	
963	3626	3671	3716	3762	3807	3852	3446 3897	3491 3942	3987	4032	
964	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482	
965	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932	
966	4977 5426	5022	5067 5516	5112 5561	5157 5606	5202 5651	5247	5292	5337	5382 5830	
967	5875	5471 5 92 0	5965	6010	6055	6100	5696 6144	5741 6189	5786 6234	6279	
969	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727	
970	6772	6817	6861	6906	6951	6996	7040	7085	7130	7175	-
971	7219 7666	7264	7309 7756	7353 7800	7398 7845	7443 7890	7488 7934	7532 7979	7577 8024	7622 8068	
973	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514	
974	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960	
975	9005 9450	9049	9094 9539	9138 9583	9183 9628	9227 9672	9272 9717	9316	9361 9806	9405 9850	44
977	9895	9939	9983	28	72	.117	.161	.206	.250	.294	-7-7
978	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738	
979	0783 1226	0827	0871 1315	0916 1359	0960 1403	1448	1049	1093 1536	1137 1580	1182 1625	
981	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067	
982	2111 2554	2156	2200 2642	2244 2686	2288	2333	2377	2421 2863	2465	2509 2951	
983		2598			2730	2774 3216	2819		2907 3348	3392	
984	2995 3436	3o39 3480	3083 3524	3127 3568	3172 3613	3657	3260 3701	3304 3745	3789	3833	
986	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273	
987	4317	4361	4405	4449	4493	4537	4581	4625 5065	4669 5108	4713 5 1 52	
988	4757 5196	4801 5240	4845 5284	4889 5328	4933 5372	4977 5416	5021 5460	5504	5547	5591	
990	5635	5679	5723	5767	5811	5854	5898	5942	5986	6030	
991	6074 6512	6117 6555	6161 6599	6205 6643	6249 6687	6293	6337 6774	638o 6818	6424 6862	6468 6906	
992	6949	6993	7037	7080	7124	7168	7212	7255	7299	7343	
994	7386	743o	7474	7517	7561	7605	7648	7692	7736	7779	
995	7823	7867	7910	7954	7998	8041	8085 8521	8129 8564	8172 8608	8216 8652	
996	8259 8695	83o3 873g	8347 8782	8390 8826	8434 8869	8477	8956	9000	9043	9087	
998	9131	9174	9218	9261	93oŚ	9348	9392	9435	9479	9522	43
999 N.	9565	9609	9652	9696	9739	9783 5	9826	9870 7	9913	9957	D.
		5	9	14	18	23	28	32	37	41	
ie l	45 E	5	9	14	18	23	27	32	36	41	
Differ.	44 H	4	9	13 13	18	22 22	26 26	31 30	35 34	40 39	
			9	1 13	17	22	20	1 30		1 39	

TABLE

oF

LOGARITHMIC SINES AND TANGENTS

FOR EVERY

TEN SECONDS OF THE QUADRANT.

Min.	1		Sine of (Degree.				P. Part
	0"	10"	20"	30"	40"	50"		to 1.".
0	Inf. Neg.	5.685575	5.986605	6.162696	6.287635	6.384545	59	
1	0.463726	6.530673	6.588665	639817	685575	726968	58	
2	764756	799518	831703	861666	889695	916024	57	
3	940847	964328	986605	7.007794	7.027997	7.047303	56	
4	7.065786	7.083515	7.100548	116939	132733	147973	55	1
5	162696	176936	190725	204080	217054	229643	54	
6	241877	253776	265358	276639	287635	298358	53	
7	308824	319043	329027	338787	348332	357672	52	
7 8	366816	375771	384544	393145	401578	409850	51	
9	417968	425937	433762	441449	449002	456426	50	
				1				
10	463726	470904	477966	484915	491754	498488	49	689.4
ΙI	505118	511649	518083	524423	530672	536832	48	629.4
12	542906	548897	554806	560635	566387	572065	47	579.1
13	577668	583201	588664	594059	599388	604652	46	536.2
14	609853	614993	620072	625093	630056	634964	45	499.2
15	639816	644615	649361	654056	658701	663297	44	467.0
16	667845	672345	676799	681208	685573	689895	43	438.7
17	694173	698410	702606	706762	710879	714957	42	413.6
18	718997	722999	726965	730896	734791	738651	41	391.3
19	742478	746270	750031	7 53758	757455	761119	40	371.2
•	-6/-5/	-60250	20		9/	-00/00	30	353.1
20	764754	768358	771932	775477	778994	782482	39	ı
21	785943	789376	792782	796162	799515	802843	38	336.7
23	806146	809423	812677	815906	819111	822292	37	321.7
23	825451	828586	831700	834791	837860	840907	36	308.0
24	843934	846939	849924	852889	855833	858757	35	295.4
25	861662	864548	867415	870262	873092	875902	34	283.8
26	878695	881470	884228	886968	889690	892396	33	273.1
27	895085	897758	900414	903054	905678	908287	32	263.2
28	910879	913457	916019	918566	921098	923616	31	254.0
29	926119	928608	931082	933543	935989	938422	30	245.4
30	940842	943248	945641	948020	950387	952741	29	237.3
31	955082	957411	959727	962031	964322	966602	28	229.8
32	968870	971126	973370	975603	977824	980034	27	222.7
33	982233	984421	986598	988764	990919	993064	26	2:6.1
34	995198	997322	999435	8.001538	3.003631	8.005714	25	209.8
35	8.007787	8.009850	8.011903	013947	015981	018005	24	203.9
36	020021	022027	024023	026011	027989	029959	23	198.3
37	031919	033871	035814	037749	039675	041592	22	193.0
38	043501	045401	047294	049178	051054	052922	21	188.0
39	054781	056633	058477	060314	062142	063963	20	183.2
-								
40	065776	067582	069380	071171	072955	074731	19	178.7
41	076500	078261	080016	081764	083504	085238	18	174.4
42	086965	088684	090398	092104	093804	095497	17	170.3
43	097183	098863	100537	102204	103864	105519	16	166.4
44	107167	108809	110444	112074	113697	115315	15	162.6
45	116926	118532	120131	121725	123313	124895	14	159.1
46	126471	128042	129607	13:166	132720	134268	13	155.6
47	135810	137348	138879	140406	141927	143443	12	152.4
48	144953	146458	147959	149453	150943	152428	11	149.2
49	153907	155382	156852	158316	159776	161231	10	146.2
5o	162681	164126	165566	167002	168433	169859	9	143.3
5 r	171280	172697	174109	175517	176920	178319	9 8	140.5
52	179713	181103	182488	18386g	185245	186617		137.9
53	187985	189348	190707	192062	193413	194760	7	135.3
54	196102	197440	198774	200104	201430	202752	5	132.8
55	204070	205384	206694	208000	209302	210601	4	130.4
56	211895	213185	214472	215755	217034	218309	3	128.1
57	219581	220849	222113	223374	224631	225884	2	125.9
58	227134	228380	229622	230861	232096	233328	1	123.7
59	234557	235782	237003	238221	239436	240647	0	121.6
	60"	50"	40"	30"	20"	10"		
				9 Degrees.			Min.	
	L			2 251000				

		110	GARITH	MIC I	NGENT	3.	,	
Min.				of 0 Degree				P. Part to 1.
	0"	10"	20"	30"	40"	50"		
0	Inf. Neg.	5.685575	5.986605	6.162696	6.287635	6.384545	59	1
I	6.463726	6.530673	6.588665	639817	685575	726968	58	
3	764756	799518	831703 986605	861666	889695	916024 7.047303	5 ₇	!
4	940847	964329	7.100548	7.007794	7 027998	147973	55	1
5	162696	176937	190725	204089	217054	229643	54	
6	241878	253777	265359	276640	287635	298359	53	
	308825	319044	329028	338788	348333	357673	52	
7 8	366817	375772	384546	393146	401579	409852	5 r	
9	417970	425939	433764	441/51	449004	456428	5o	
10	463727	470906	477968	484917	491756	498490	49	689.4
II	505120	511651	518085	524426	530675	536835	48	629.4
12	542909	548900	554808	560638	566390	572068	47	579.1
13	577672	583204	588667	594062	599391	604655	46	536.2
14	609857	614996	620076	625097	630060	634968	45	499.2
15	639820	644619	649366	65406r	658706	663302	44	467.0
16	667849	672350	676804	681213	685578	689900	43	438.7
17	694179	698416	702612	706768	710885	714963	42	413.6
18	719003	723005 746277	726972 750037	730902 753765	734797 757462	738658 761127	41	391.3
19	742484						40	371.2
20	764761	768365	771940	775485	779002	782490	39	353.1
21	785951	789384	792790	796170	799524	802852	38	336.7
22	806155	809433	812686	815915	819120	822302	37	321.7 308.0
23 24	825460	82859 6 846950	831710	834801	837870 855844	840918	36 35	
24 25	843944	86456o	849935 867426	852900	873104	858769	34	295.4 283.9
26	861674 878708	881483	884240	870274 886981	889704	875915 892410	33	273.2
27	895099	897772	900428	903068	905692	908301	32	263.2
28	910894	913471	916034	918581	921113	923631	31	254.0
29	926134	928623	931098	933559	936006	938439	30	245.4
30	940858	943265	945658	948037	950404	952758	29	237.3
31	955100	957428	959745	962049	964341	966621	28	229.8
32	968889	971145	973389	975622	977844	980054	27	222.7
33	982253	ç84441	986618	988785	990940	993085	26	216.2
34	995219	997343	999457	8.001560	8.003653	3.005736	25	209.8
35	8 007809	8.009872	8.011926	013970	016004	018029	24	203 9
36	020044	022051	024048	026035	028014	029984	23	198.3
37	031945	033897	035840	037775	039701	041618	22	193.0
38	043527	045428 056662	047321 058506	049205 060342	051081	052949 063992	21	188.o 183.3
39	054809				062171	1	20	
40	065806	067612	069410	071201	072985	074761	19	178.7
41	076531	078293	080047	081795	083536	085270	18	174.4
42	086997	088717	090431	092137	093837 103900	095530 105554	17 16	170.3 166.4
44	097217	098897 108845	100571 110481	102239	113734	115352	15	162.7
45	116963	118569	120169	121763	123351	124933	14	159.1
46	126510	128081	129646	131206	132760	134308	13	155.7
47	135851	137389	138921	140447	141969	143485	12	152.4
48	144996	146501	148001	149497	150987	152472	11	149.3
49	153952	155426	156896	158361	159821	161276	10	146.2
50	162727	164172	165613	167049	16848o	169906	9	143.4
51	171328	172745	174158	175566	176969	178368	8	140.6
52	179763	181153	182538	183919	185296	186668		137 :
53	188036	189400	190760	192115	193466	194813	7 6	135.3
54	196156	197494	198829	200159	201485	202808	5	132.8
55	204126	205440	206750	208057	209359	210658	4	130.4
56	211953	213243	214530	215814	217093	218369	3	128.1
57 58	219641	220909	222174	223434	224692	225945	2	125.9
50	227195 234621	228442 235846	229685 237068	230924 238286	232160 339502	233392 240713	0	123.8
	60"	50"	40"	30"	20"	10'		121.7
				89 Degree			Min.	
			angent of	. Jo Degree	•	W V		

4	T		Sing of 1		DINES.			
Min	0,	10"	20"	Degree.	40"	50"		P. Part to 1".
0	8.241855	8.243060	8.244261	8.245459	8.246654	8.247845	50	119.6
1	249033	250218	251400	252578	253753	254925	58	117 7
2	256094	257260	258423	259582	260739		57	115.8
3	263042	264190	265334	266475	267613	268749	56	114.0
4	269881	271010	272137	273260	274381	275499	55.	112.2
5	276614	277726	278835	279941	281045	282145	54	170.5
6	283243	284339	285431	286521	287608	288692	53	108.8
7 8	289773	290852	291928	293002	294073	295141	52	107.2
	296207	297270	298330	299388	300443	301496	51	105.7
9	302546	363594	304639	305681	306721	307759	50	104.1
10	8.308794	8.309827	8.310857	8.311885	8.312910	8.313933	49	102.6
II	314954	315972	316987	318001	319012	320021	48	101.2
12	321027	322031	323033	324032	325029	326024	47	99.8
13	327016	328007	328995	329980	330964	331945	46	98.5
14	332924	333901	334876	335848	336819	337787	45	97.1
15	338753	339717	340679	341638	342596	343551	44	95.8
16	344504	345456	346405	347352	348297	349240	43	94.6
17	350181	351119	352056	352991	353924	354855	42	93.4
18	355783	356710	357635	358558	359479	360398	41	92.2
19	361315	362230	363143	364055	364964	365871	40	91.0
20	8.366777	8.367681	8.368582	8.369482	8.370380	8.371277	. 39	89.0
21	372171	373063	373954	374843	375730	376615	38	88.8
22	377499	378380	379260	380138	381015	381889	37	87.
23	382762	383633	384502	385370	386236	387100	36	86.
24	387962	388823	389682	390539	391395	392249	35	85.6
25	393101	393951	394800	395647	396493	397337	34	84.
26	398179	399020	399859	400696	401532	402366	33	83.
27	403199	404030	404859	405687	406514	407338	32	82.
28	408161	408983	409803	410621	411438	412254	31	81.8
29	413068	413880	414691	415500	416308	417114	30	80.8
30	8.417919	8.418722	8.419524	8.420325	8.421123	8.421921	29	80.0
31	422717	423511	424304	425096	425886	426675	28	79.1
32	427462	428248	429032	429815	430597	431377	27	78.2
33	432156	432934	433710	434484	435257	436029	26	77.
34	436800	437569	438337	439103	439868	440632	25	76.
35	441394	442156	442915	443674	444431	445186	24	75.
36	445941	446694	447446	448196	448946	449694	23	75.
37	450440	451186	451930	452673	453414	454154	22	74 .:
38	454893	455631	456368	457103	457837	458570	21	73.
39	4593ó1	460032	460761	461489	462215	462941	20	72.
40	8.463665	8.464388	8.465110	8.465830	8.466550	8.467268	19	72.
41	467985	468701	469416	470129	470841	471553	18	71.
42	472263	472971	473679	474386	475091	475795	17	70.
43	476498	477200	477901	4786o1	479299	479997	16	69.
44	480693	481388	482083	482776	483467	484158	15	69.
45	484848	485536	486224	486910	487596	488280	14	68.
46	488963	489645	490326	491006	491685	492363	13	67.0
47	493040	493715	494390	495064	495736	496408	12	67.
48	497078	497748	498416	499084	499750	500416	11	66.
49	561080	501743	502405	503067	503727	504386	10	66.
5o	8.505045	8.505702	8.506358	8.507014	8.507668	8.508321	9	65.
51	508974	509625	510275	510925	511573	512221	8	64.
52	512867	513513	514157	514801	515444	516086	7	64.
53	516726	517366	518005	518643	519280	519916	6	63.
54	520551	521186	521819	522451	523083	523713	5	63.
55	524343	524972	525599	526226	526852	527477	4	62.6
56	528102	528725	529347	529969	530590	531209	3	62.
57	531828	532446	533063	533679	534295	534909	2	61.0
- /	535523	536136	536747	537358	537969	538578	I	61.1
58				1 5/	5/-6-0	542216	0	60.
	539186	539794	54o4o1	541007	541612			00.
58		539794	540401	30"	20"	10"	Min.	00.

			· ·					
Min.	1		Tangent of	of 1 Degree	э.			P. Part
	0"	10"	20"	30"	40"	50"		to 1".
0	8.241921	8.243126	8.244328	8.245526	8.246721	8.247913	59	119.7
I	249102	250287	251469	252648 259654	253823	254996	58	117.7
3	256165	257331 264263	258494 265408	266549	260811 267688	261965	5 ₇	115.8
4	269956	271086	272213	273337	274458	275576	55	114.0
5	276691	277804	278913	280020	281124	282225	54	110.5
6	283323	284419	285512	286602	287689	288774	53	108.9
	289856	290935	292012	293086	294157	295226	52	107.2
8	296292	297355	298416	299474	300530	301583	51	105.7
9	302634	303682	304727	305770	306811	307849	50	104.2
10	8.308884	8.309917	8.310948	8.311976	8.313002	8.314025	49	102.7
ΙI	315046	316065	317081	318095	319106	320115	48	101.3
12	321122	322127	323129	324129	325126	326121	47	99.8
13	327114	328105	329093	330080	331064	332045	46	98.5
14	333025	334002	334977	335950	336921	337890	45	97.2
15	338856 344610	339821 345562	340783 346512	341743 347459	342701	34365 ₇ 349348	44	95.9
16	350289	351229	352166	353101	3484o5 354o35	354966	43 42	94.6
18	355895	356823	357748	358671	359593	360512	41	93.4
19	361430	362345	363259	364171	365081	365988	40	91.1
20	8.366895	8.367799	8.368701	8.369601	8.370500	8.371397	39	89.9
21	. 372292	373185	374076	374965	375853	376738	38	88.8
22	377622	378504	379385	380263	381140	382015	37	87.8
23	382889	383760	38463o	385498	386364	387229	36	86.7
24	388092	388953	389813	390670	391526	392381	35	85.7
25	393234	394 0 85	394934	395782	396628	397472	34	84.7
26	398315	399156	399996	400834	,401670	402505	33	83.7
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28	408304 413213	409126	409946	410765 415647	411583	412399	31	81.8
29		414026	414837			417263	30	80.9
30 31	8.418068	8.418872	8.419674 424458	8.420475 425250	8.421274	8.422072	29	80.0
32	422869 427618	423664 428404	424436	423230	426041 430755	426830 431536	28 27	79.1 78.3
33	432315	433og3	433870	434645	435419	436191	26	77.5
34	436962	437732	438500	439267	440033	440797	25	76.6
35	441560	442322	443082	443841	444599	445355	24	75.8
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42 43	472454 476693	473163 477396	473872 478097	474579 478798	475285	475990 480195	17	70.7
44	480892	481588	482283	482976	479497 483669	48436o	16	70.0 69.3
45	485050	485740	486428	487115	487801	488486	14	68.6
46	489170	489852	490534	491215	491894	492573	13	68.0
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5 r	509200	509852	510503	511153	511802	512451	8	65.0
52 53	513098	513744	514389	515034	515677	516320	7 6	64.4
54	516961 520790	517602 521425	518241 522059	518880 522692	519518 523324	520154 523956	5	63.8
55	524586	525215	525844	526472	527098	527724	4	63.3 62.7
56	528349	528973	529596	530218	530840	531460	3	62.2
57	532080	532698	533316	533933	534549	535164	2	61.6
58	535779	536392	537005	537617	538227	538837	1	61.1
59	539447	540055	540662	541269	541875	542480	0	60.6
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4	3	8 553539	4126 4713	5300	5885	6470	56			5972	6367	6762	7156	7550	7943	56
6 3999 457-5 5146 5719 6296 6861 53 6 30-23 3416 33-6 4179 4279 4279 5286 58.570836 14.11 1965 2528 30-31 3653 51 7 74318 30-8 3566 9137 9704 2270 52 7667 8052 8436 8820 2023 3586 51 7666 8122 8578 9232 9786 7441 13 5580 892 1444 1995 2546 30-66 3645 48 11 48.590 21 444 1995 2546 30-66 3645 48 11 48.590 21 444 1995 2546 30-66 3645 48 11 48.590 21 444 1995 2546 30-66 3645 48 11 48.590 21 160 1799 2338 2875 3412 45 13 3484 4848 5919 5555 6057 6619 44 15 3048 4848 5919 5555 6057 6619 44 15 3048 4848 5919 5555 6057 6619 44 15 3488 3489 4012 4536 5058 5580 6102 41 18 8561 2037 2339 2700 3063 3445 360 4871 5313 38 3489 4012 4536 5058 5580 6102 41 18 8576 511 6573 6009 7417 7924 8311 7955 8313 6889 5049 4020 6909 7417 7924 8311 7955 8313 6889 5049 4020 6909 7417 7924 8311 7955 8313 6889 5049 4020 6909 7417 7924 8311 7955 8313 6889 5049 4020 6909 7417 7924 8311 7955 8313 6889 7944 9047 4522 5056 6619 6619 6757 6703	4							4	{	3337	8729	9122	9514	9906	.207	55
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9	8	8.570836	1401 1965	2528	3091	3653	51	8		7667	8052	8436	8820	0203	0586	51
10		4214	4774 5334	5893	6451	7009	50	9		9969	.352	.734	1115	1497	1878	50
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188		7152	7683 8214	8745	9274	9803	43	16	5	747	6116	6484	6852	7220	7587	43
9 6623 7143 7662 818 8699 9217 40 10 2337 2700 3663 3425 3787 4149 21 3237 2700 3663 3425 3787 4149 4179 22 3488 3636 4871 5381 38 21 6675 7034 7304		3.000332	0859 1387	1913	2439	2964	42		o _c7	7955	8321	8688	9054	9420	9786	42
20		6623	71/3/7662	8181	8600	0102	41		0.700	337	0210	3063	3/05	1009	1973	41
22	•	9734	.251 .766	1282	1706	2310	30		1	511	4872	523/	550/	5055	63±5	30
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23 8937 9442 9947 . 452 . 956 1459 36 238 . 770970 1326 1681 2037 2392 2474 3124 3616 3616 2616 3	22	5891	6400 6909	7417	7924	8431	37		8	828	9185	9543	9900	.257	.613	37
25		8937	9442 9947	.452	.956	1459	36		8.770	970	1326	1681	2037	2392	2747	36
26		8.021902	2464 2965 5464 566	6450	6056	4466	35		3	101	3456	3810	4163	4517	4870	35
27 8. 630911 1403 1894 2385 2595 3365 32 27 3434 9783 132 .430 .829 1177 329 6776 7262 7746 8230 8714 9197 30 29 3605 3351 4296 4641 4986 5331 30 3642 5320 3998 4475 4952 28 31 7736 8078 8421 8762 9104 9466 332 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 27 28 .468 .888 1149 1488 27 27 27 27 28 .468 .888 1149 1488 27 27 27 27 27 27 27		70/8	8444 8038	0439	0930	7455	33		. 5	333	7684	3927 8035	8385	8-35	0982	34
28		8.630011	1403 1804	2385	2875	3365	32									
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32	30	9680	. 162 . 643	1124	1604	2084	29		5	675	6019	6363	6707	7050	7393	29
33 8.274 8.747 9219 9690 .161 .632 26 334 3.791828 2.167 2506 2845 3183 3521 24 35 3911 4377 4843 5308 5773 6238 24 35 5881 6218 6553 6889 7224 7559 24 35 6702 7165 7628 8090 8552 9014 23 36 7894 8229 8563 8897 9231 9564 23 36 7894 8229 8563 8897 9231 9564 23 36 7894 8229 8563 8897 9231 9564 23 36 7894 8229 8563 8897 9231 9564 23 37 9897 .230 .563 .866 1228 1560 23 38 8.662230 2688 3145 3602 4058 4513 21 38 8.801892 2223 2554 2885 3216 3546 22 37 7689 8141 8592 9443 9444 944		5/08/	5042 3320	6854	4475	4952	28		7	736	8078	6421	8762	9104	9446	28
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51 6543 6966 7388 7810 8232 8653 8 51 7011 7324 7637 7949 8261 8573 8 9073 9494 9913 .333 .752 1171 7 52 8884 9196 9507 9818 .129 .439 7 53 8.701589 2007 2424 2841 3258 3674 6 53 8.830749 1060 1369 1679 1988 2298 6 577 6990 7402 7815 8226 8638 4 55 42607 2015 3224 3532 3840 4148 5 56 9049 9460 9870 .280 .690 1099 3 56 6297 6603 6909 7215 7520 7825 57 8.711507 1916 2324 2731 3139 3546 2 58 3052 4358 4764 5169 5574 5979 1 58 3052 4358 4764 5169 5574 5979 1 58 3052 4358 4764 5169 5574 5979 1 58 6383 6787 7190 7503 7996 8398 0 60" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" 50" 40" 30"		8.691438 1	866 2293	2720	3146 3	3572	10		3	240	3556	3871	4186	4501	4816	
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53 8.701589 2007 2424 2841 3258 3674 6 538 .830749 1060 1369 1679 1988 2298 6 4090 4505 4920 5335 5749 6163 5 54 2607 2915 3224 3532 3840 4148 5 55 6577 6990 7402 7815 8226 8638 4 55 4456 4763 5070 5377 5684 5991 6 57 8.711507 1916 2324 2731 3139 3546 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8437 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8437 8740 9044 9348 9652 2 57 8130 8437 8740 9044 9348 9652 2 57 8130 8435 8740 9044 9348 9652 2 57 8130 8437 8740 9044 9348 9678 9678 9678		0043	140410013	7010	759	177	- 11	- 1	7	88/	7324	0507	7949	120	. //30	
54		8.7015802	2007 2424	2841	3258	3674	6		3.83o	740	1060	1360	1670	1988	2208	7 6
55 6577 6590 7402 7815 8226 8638 4 55 4456 4763 5070 5377 5684 5991 456 9870 280 .690 1099 3 57 8.711507 1916 2324 2731 3139 3546 2 57 8130 8435 8740 9044 9348 9652 2 58 3952 4358 4764 5169 5574 5979 1 58 9956 .260 .563 .866 1169 1472 1 1 1 1 1 1 1 1 1	54	4090 4	505 4920	5335	749	63			2	607	2915	3224	3532	3840	4148	5
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59 6383 6787 7190 7593 7996 8398 0 59 8 .841774 2076 2378 2680 2982 3283 0 60" 50" 40" 30" 20" 10" 50 60" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" 50 50" 50" 50" 40" 50" 50" 50" 50" 50" 50" 50" 50" 50" 5		9049	460 9870	.280	690 1	099	- 11		6	297	6603	6909	7215	7520	7825	3
59 6383 6787 7190 7593 7996 8398 0 59 8 .841774 2076 2378 2680 2982 3283 0 60" 50" 40" 30" 20" 10" 50 60" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" 50 50" 50" 50" 40" 50" 50" 50" 50" 50" 50" 50" 50" 50" 5		3050	910 2324	2731	5139	046	li li		8	056	3435	563	9044	9348	9002	2
Co-sine of 87 Degrees.		6383	787 7100	7503	700618	7979	- 11		9.84+	930	2076	2378	2680	2082	3283	0
Co-sine of 87 Degrees.						7.0//	-									
77 (1"2" 3" 4" 5" 6" 7" 8" 9" 77 (1"2" 3" 4" 5" 6" 7" 8" 9"	- 1						H Hi	-								Min
P.Part \ \\ \frac{48}{96} \frac{145}{192} \frac{192}{241} \frac{289}{289} \frac{338}{386} \frac{434}{434} \ \ \frac{P.Part}{241} \frac{24}{34} \frac{69}{69} \frac{103}{103} \frac{138}{138} \frac{172}{207} \frac{241}{241} \frac{275}{275} \frac{310}{241} \frac{138}{275} \frac{172}{241} \frac{138}{275} \frac{172}{241} \frac{138}{275} \frac{138}{241} \frac{138}{280} \frac{138}{280} \f		(1// 9/													8"	
(P. F	art \ 48 96	145 193 2	41 289	338 3	386 43	34	P. F	art } 3	$\frac{1}{69}$	103	138 1	72 207	241		

				L 0 6	AL	Tangent of 2 Degrees. F Tangent of 3 Degrees.													
Min.	Tai	ngent	of 2	Degr	rees.			Min.		Tai	ngent	of 3	Degr	rees.					
	0"	10"	20"	30"	40	50"				0"	10"	20′′	30"	40"	50"				
	8.543084							0	8.	719396	9798	.201	.603	1004	1405	59			
I	8 550268	7289	7887	8483	9079	9674	58		0.	721806					6191				
3		4405						3		6588	6084	7380	7775	8170	8565	56			
4	7336	7920	8503	9085	9667	.248	55	4		8959	9353	9746	. 140	.533	.925	55			
	8.560828	1407	1985	2563	3140	3716	54	5	8.	731317	1709	2101	2492	2883	3273	54 ;			
6	4291	4866	5440	6013	6585	7157	53	6							5608				
7	7727	8298	8867	9435	32.5	.570	52	7							7931				
	8.571137	1702 5081						8	Q	6317 740626					242				
10		8434						9 10	.	2022	330/	3685	4066	4447	4827	40			
	8.581208							II		5207	5586	5966	6344	6723	7101	48			
12	4514	5062	5610	6157	6704	7249	47	12		7479	7857	8234	8611	8988	9364	47			
13	7795	8339	8883	9426	9968	.510	46	13		9740	.116	.491	.866	1241	1615	46			
	8.591051								8.	751989									
15 16		4820						15 16							6083 8300				
	8.600677	8024	1733	2260	2787	3313	42	17							.505				
18		4363						18	8	760872									
19		7499						19		3065	3429	3793	4157	4520	4884	40			
	8.610094							20							7056				
21		3702						21		7417	7778	8139	8499	8859	9218	38			
22 23	0202	6772	7281	7790	8298	8806	36	22	Q	9278 771727	9937	293	.004	3,55	1370	36			
	8.622343	9819	33/8	. 030 3850	/35t	1859	35	24	0	3866	1222	1577	1032	5287	5641	35.			
25		5851						25							7761				
26	8340	8836	9332	9827	.321	.815	33	26							9871				
27	8.631308	1801	2293	2785	3276	3766	32	27	8	. 780222	0572	0922	1272	1622	1971	32			
28		4746						28							4061				
29		7671						29							6140				
31	8.640093	3462						30 31							8210				
32	5853	6329	6805	7281	7756	8230	27		8	.790613									
33	8704	9178	9651	.123	.595	1067	20	33	-						4362				
34	8.651537	2008	2478	2947	3416	3884	25	34							6394				
35		4820						35		6731	7069	7406	7743	8079	8416	24			
36		7613						36		8752	9088	9423	9759	94	.429	23			
37	8.662689	37.68						37		.800763					4427				
39	5/33	5889	6344	6700	7253	4977	20	39	1						6412				
40	8160	8613	9065	9517	9968	.410	19	40							8389				
41	8.670870							41		8717	9046	9374	9701	29	.356	18			
42	3563	4010	4457	4903	5349	5794	17			.810683	1010	1337	1663	1989	2315	17			
43	6239	6684	7128	7572	8015	8457	16	43	1						4265				
44	8,681544	9341						44							6207 8140				
46		4608						45		8461	8782	9103	0423	9744	64	13			
47		7218						47	8	.820384	0703	1023	1342	1661	1080	12			
48	9381	9813	. 244	.674	1104	1534	11	48		2298	2617	2935	3253	3570	3888	II			
	8.691963	2392	2820	3248	3675	4103	10	49		4205	4522	4838	5155	5471	5787	10			
50		4956						50		6103	6418	0733	7049	7363	7678	9			
51		7504	7928	88	0773	9195	8	5 ₁		7992	0307	500	0934	9248	9561 1436	8			
	8.702139									.831748	2050	2371	2682	2002	3303	7			
54	4646	5063	5470	5895	6310	6725	5	54							5162	5			
55	7140	7554	7967	8381	8794	9206	4	55		5471	5780	6089	6397	6705	7013	4			
56	9618	3030	.442	.853	1263	1674	3	56		7321	7629	7936	8243	8550	8857	3			
	8.712083	2493	2902	3311	3719	4127	2	57							.692				
58		4942								.840998	3.03	3/3	1912	1020	2521 4341	I			
59	60"	50"	40"	30"	20"	100	-	59	-	60"	50"	40"	30"	20"	10"				
		ingen			-	-	Mi.		-			-		٠		Min.			
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P.	Part { 1" 2 48 9	; 3'' 7 145	193 9	ა" ნ' 242-90	7" 90 338	87 387	9" 435	Ρ.	Pa	$\operatorname{art} \left\{ \begin{array}{l} 1^{\prime\prime} & 2 \\ 35 & 6 \end{array} \right.$	3" 39 104	138	ə∵ 6 173-90	7"	276	311			
	(10 0	. 140	100 /			. 557	200	II		(00 (100	~ (~ ± A	. ~10				

Sime of 4 Degrees.		0	·	£ A T		O G A	RIT	H	Sing of 5 December								
S. 833585 5886 4186 4487 4787 5087 59 1 5387 595 5987 598 1 5387 5987 5988 5988 5988 6488 5488 5987 597 5988 5988 5988 5988 5888 5884 5888 5884 5988	Min						507		Mir						EOII		
1 5387,5687,5987,6987,69876,6986,878,878,678,678,678,678,678,678,678,6	_							50								50	
2		5387	5687	5087	6286	6585	6884	58		1738	1077	2217	2457	2606	2035	58	
3	2									3174	3413	3652	3891	4120	4368	57	
5		8971	9268	9565	9862	. 159	.455	56		4606	4844	5083	5321	5558	5796	56	
6		8.850751	1047	1343	1639	1934	2229	55									
7 6649 (6342 (6344 (6926) 7218 7310) ≥ 78 . 950287) 6522 (757) (9924 1234) 8 878018 (8928) 8333 (85748) 8665 (9525) 5 9 (3546) 8366 . 1240, 2438 2726 (49) 11 3043 (302) 3589 (3877 4164 4451 48 11 36455 (6740) 7025 7310 7595 7880. (46 11 34 302) 3589 (3877 4164 4451 48 11 36455 (6740) 7025 7310 7595 7880. (46 11 34 302) 3589 (3877 4164 4451 48 11 3645 (8744) 8733 (9017) 9301 9585 45 14 8 1658 (844) 8733 (9017) 9301 9585 45 14 8 1658 (844) 8733 (9017) 9301 9585 45 14 8 1658 (884) 8733 (9017) 9301 9585 45 14 8 1658 (884) 8733 (9017) 9301 9585 45 14 8 1658 (884) 8743 (9017) 12 14 9 1616 8847 1219 2410 2692 2073 43 16 2801 3030 3358 3486 3714 3044 43 17 3255 3536 (3817) 4097 4378 4658 44 17 4 4397 4625 4852 5 080 5 307 42 19 4016 6844 7172 7451 7729 8007 40 18 5534 5761 5987 (6414 6450) 48 18 5534 5761 5987 (6414 6441 6667 41 19 6616 6844 7172 7451 7729 8007 40 18 5534 5761 5987 (6414 6450) 48 18 5534 5761 5987 (6414 6450) 48 18 5534 5761 5987 (6414 6450) 48 18 5534 5761 5987 (6414 6450) 48 18 5534 5761 5987 (6414 6451 6441 6460 4441 4451										7456	7693	7929	8166	8402	8638	54	
8	1									0074 8 05008#	9110	9545	9551	9017	7/6	50	
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10 S. 861 te 83 1572 1861 2149 2438 2726 49 10 4499 4732 4965 5197 5529 5662 49 11 3014 3024 3589 3877 4164 4451 48 11 5894 6126 6358 6599 6821 7053 6455 6740 7025 7310 7595 7880 46 13 8670 8091 713 13636 2952 2822 46 14 8163 8449 8733 9017 9301 9585 45 14 8.96065 9820 511 7741 970 1200 45 16 8.871 565 1847 120 2410 2602 2973 43 16 2801 3303 3558 3468 3714 3424 515 1658 1887 116 2344 573 44 15 8498 5498 5777 6057 6336 41 18 5534 5761 5987 6214 6441 6667 41 10 615 6894 7172 7451 7729 8007 40 10 6893 7120 7346 7572 7797 8033 40 822 8.881607 1883 158 2433 2708 2983 37 28 28 28 28 28 28 28 2									1 1	3100	3333	3567	3800	4033	4266	50	
11	10	8.861283	1572	1861	2149	2438	2726	49		4499	4732	4965	5197	5429	5662	49	
13		3014	3302	3589	3877	4164	4451	48	11	5894	6126	6358	6590	6821	7053	48	
14 8165 8449 8733 917 9301 9385 45 14 8.96005 2028 9511 0741 070 1200 45 15 9868 1.511. 434 717 1000 1282 44 16 8.871565 1847 2129 2410 2692 2973 43 17 3255 3336 3817 4007 4378 4685 42 18 4938 5218 6348 5777 6057 6336 41 19 6615 6894 7179 7451 7729 8007 40 20 8285 8563 8841 9118 9395 9672 30 21 9949 226 5.03 779 1055 1331 38 22 8.881607 1883 2158 2433 2708 2983 37 23 3283 3533 3807 4807 4855 4629 36 24 4903 5177 5450 5723 5996 6269 35 25 6542 6814 7087 7359 7531 7938 20 26 8148 8446 8478 7359 7531 38 28 8.881611 1690 1000 2229 2498 2767 31 28 8.881611 1690 1000 2229 2498 2767 31 28 8.881611 1690 1600 2229 2498 2767 31 28 8.881611 1690 1600 2229 2498 2767 31 29 3035 3304 3572 3840 4108 4376 30 30 4643 4911 178 5445 5712 5979 293 31 31 6466 6512 6778 7044 7310 7576 83 32 7842 8107 8378 8638 8903 9168 27 33 33 9432 9677 9744 7310 7576 83 34 8.991017 1280 1544 1807 2070 2333 25 256 2858 8121 3383 3645 3079 24 33 35 256 2858 8121 3383 3645 3079 24 33 3983 3101 3313 3536 3545 3491 5708 5924 6141 6357 6573 26 33 4149 4206 2462 4719 2976 2331 81 4838 3744 4000 4264 4511 4767 17 434 4000 4264 4511 4767 17 434 4000 4264 4511 4767 17 434 4000 4264 4511 4767 17 438 4004		4738	5024	5311	5597	5883	6169	47	1 -1								
15	1 .	6455	6740	7025	7310	7595	7880	46	1 1								
16 8.8 1555 1547 129 124 10 269 2973 43 16 280 1303 3258 3358 3486 3714 3974 498 5174 4974 4974 496 498 5174 506 530 42 4938 5218 5498 5777 6057 6336 41 19 6615 6894 7172 7451 7729 8007 40 19 6893 7120 7346 5752 7797 8023 20 9040 .226 .503 .779 1055 1331 38 22 8.881607 1883 2158 2433 208 2384 3834 398		8100	0449	0733	9017	9301	9383	43									
17		8 871565	18/17	2120	2/17	2602	2073	44	1 - 1	2801	3030	3058	3/86	301/	30/0	144	
18		3255	3536	3817	4007	4378	4658	42	1 1								
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20 8285 8563 8841 118 3355 6572 39 20 8246 8474 8700 8925 150 3375 33 32 28 8.881607 1883 2158 2433 2708 2983 37 228 970947 1171 135 1619 1842 2066 37 224 403 5177 5450 5723 5966 6263 52 4 3688 3851 4073 4264 5458 804 4087 7359 7631 7903 34 25 6542 6814 7087 7359 7631 7903 34 25 6542 6814 7087 7359 7631 7903 34 25 6263 6514 6735 6956 7177 7388 33 27 88 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960 2222 2498 2767 31 28 891421 1690 1960	19	6615	6894	7172	745 I	7729	8007	40	19	6893	7120	7346	7572	7797	8023	40	
228	20	8285	8563	8841	9118	9395	9672	39		8249	8474	8700	8925	9150	9375	39	
23		9949	.226	.503	.779	1055	1331	38									
24										8.970947	1171	1395	1619	1842	2000	37	
25	1 .									2209 3608	3857	2730	2939	15102	3,400	35	
26	1 -	65/2	681/	7087	7350	763r	7003	3/1		/062	5184	5/06	5628	5850	6071	3/	
28 8.891421 1690 1960 2229 2498 2767 31 29 8,0419161 331 9600 982033 31 329 3.035 3304 3572 3840 4108 4376 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1354 30 29 8.980259 0478 0697 0916 1135 1355 1606 1858 2109 2360 154 4 2665 2477 2577 5532 5787 6041 6296 115 4 2665 2277 2486 25 277 24	1 -	8174	8446	8717	8088	0250	0530	33	1								
29	27																
30	28	8.891421	1690	1960	2229	2498	2767	31									
31		3035	3304	3572	3840	4108	4376	30									
32									1								
33		0240	8107	0770	8638	7310	7370	20									
34 8.901017 1280 1544 1807 2070 2333 25 34 6789 7005 7221 7437 7652 7868 25 2596 2858 3121 3383 3645 3907 24 355 8083 8299 8514 8729 8944 9159 24 328 3779 7557 7817 8076 8335 8595 21 38 390660 874 9588 9803 .17 .232 .446 23 38 8533 9112 9371 9629 9888 .146 20 39 3222 3435 3647 3860 4072 4285 20 40 8.910404 6662 0917 1177 1434 1692 19 40 4497 4709 4921 5133 53455 5556 19 42 3488 3744 4000 4256 4511 4767 17 42 4285 20 4497 4709 4921 5133 53455 5556 16 44 6550 6805 7059 7313 7566 7820 15 44 6550 6805 7059 7313 7566 7820 15 44 4508 4									4 -								
35									1								
36									11	8083	8299	8514	8729	8944	9159	24	
38	36									9374	9588	9803	17	.232	.446	23	
39		5736	5997	6257	6517	6778	7038	22									
40 8.910404 0662 0919 1177 1434 1692 19 40 4497 4700 4921 5133 5345 5556 19 41 1949 2206 2462 2719 2976 3232 18 41 5768 5980 6191 6402 6614 6825 18 42 3488 3744 4000 4256 4511 4767 17 42 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7247 7457 7668 7879 8089 17 7036 7349 7356 7880 15 44 7569 7699 7979 188 .398 .607 15 44 7560 7699 7979 7188 .398 .607 15 44 7560 7869 7879 715 7100 7348 7468 7661 7867 8073 9 7100 7348 7566 7844 8092 8339 8 51 8278 8484 8689 8894 9100 9305 8 7100 7348 7499 7449 7250 7456 7661 7867 8073 9 755 7561 7564 7568 7594 6185 6422 6671 6914 7156 2 7564 7661 7867 8073 1 7594 6185 6428 6671 6914 7156 2 7308 7641 7883 8125 8366 8608 1 5860 5909 9332 9573 9814 .555 5613 5815 5007 7227 7428 7629 7830 1 7447 7457 7457 7458 7468 7464 7455 7468 7464 7455 7468 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7458 7469 7469 7458 7469 7	- 1	7297	7557	7817	8076	8335	8595	21	II .								
41										3222	3435	3047	5-22	4072	4280	20	
42									11 .								
43									14 -								
44																	
45		655o	6805	7059	7313	7566	7820	15		9560	9769	9979	1.188	.398	.607	15	
46	1 -	8073	8327	8580	8833	9086	9338	14		9.000816	1025	1234	1443	1652	1860	14	
48		9591	9843	196	.348	.600	.852	13	н.								
49		8.921103	1355	1000	1858	2109	2360	12		3318	3520	3733	5.941	4149	4330	12	
So		2010	4360	6112	1861	5777	5360	11		5805	6012	6978	6/25	6631	683	110	
51 7100 7348 7596 7844 8092 8339 8 51 8278 8484 8689 894 9100 9305 8 52 8587 8834 9081 9328 9575 9821 7 52 9510 9715 9919 124 329 1533 7 53 8.930068 0314 0560 0806 1052 1298 6 53 9.010737 0942 1146 1350 1554 1758 6 54 1544 1789 2035 2280 2525 2770 5 54 1962 2165 2369 2572 2776 2979 5 55 3015 3260 3504 3749 3993 4237 4 55 3182 3385 3588 3791 3994 4197 4 56 4481 4725 4969 5212 5456 5699 3 56 4400 4602 4805 5007 5209 5411 3 57 5942 6185 6428 6671 6914 7156 2 57 5613 5815 6017 6219 6421 6622 2 </td <td></td> <td>5600</td> <td>5858</td> <td>6107</td> <td>6355</td> <td>6604</td> <td>6852</td> <td>0</td> <td>50</td> <td>7044</td> <td>7250</td> <td>7/156</td> <td>7661</td> <td>7865</td> <td>8073</td> <td></td>		5600	5858	6107	6355	6604	6852	0	50	7044	7250	7/156	7661	7865	8073		
53 3 3 3 3 3 3 3 3 3		7100	7348	7506	7844	8002	8339	8		8278	8484	8689	8894	0100	9305	8	
53 3 3 3 3 3 3 3 3 3	52	8587	8834	9081	9328	9575	9821	7	52	9510	9715	9919	. 124	.329	.533	3 7	
55		,8.930068	0314	0560	0806	1052	1298	0	53	9.010737	0942	1146	i 35c	1554	1 758	8 6	
56		1544	1789	2035	2280	2525	2770	1 .		1962	2165	2360	2572	2776	2979	5	
57		3015	3260	3504	3749	3993	4237		11								
58	1								H								
59 8850 9091 9332 9573 9814																	
60" 50" 40" 30" 20" 10"									11	8031	8232	8433	8633	8832	9032	0	
Co-sine of 85 Degrees.	1-3							-								-	
								Min		Co	-sine		-	rees.		Mir	
	P.	Part 5 1" 5	2" 3"	4"	5" 6'	′ 7″			P.	Part \ \ \frac{1''}{99}						-	

	Tangent of 4 Degrees. s Tangent of 5 Degrees.														28
Min.								Min.							
_	0'.	10"		30"	40"	50"			0"	10"	20"	30"	40"	50"	<u>_</u> _
	8.844644	4946 6757						0 I	8.941952 3/0/	2194 3676	2437 3888	4120	4370	3163 4611	58 58
2	8260	8560	885a	0150	0458	17959	57	2	4852	5093	5334	5574	5815	6055	57
	8.850057	0355	o654	0952	1250	1548	56	3	6295	6535	6775	7015	7255	7494	56
4	1846	2144	2441	2738	3035	3332	55	4	7734	7973	8212	8451	8690	8929	55
5		3925						5	9168 8.950597	9406	9644	9883	.121	.359	54
7		5699 7465							2021	2258	2405	2732	2068	3205	$\frac{55}{52}$
8	8932	9225	9517	9810	.102	.394	51	7 8	3441	3677	3913	4149	4385	4621	51 l
9	8.860686	0977	1269	156o	1851	2142	50	9	4856	5092	5327	5562	5797	6032	50
10		2723						10	6267	6502	6736	6971	7205	7439	49
11		4462 6194						11						8842 .240	
13	7632	7919	8206	8402	8770	9065	46		8.960473						
14	9351	9637	9923	.208	.494	.779	45	14	1866	2098	2329	2561	2792	3023	45
	8.871064							15						4408	
16	2770	3054 4752	3337 5036	53.7	3904	4187	43	16	4639	60.48	5099	5329	6036	5789 7165	43
17	6162	6444	6725	7006	7287	7568	42	17 18						8538	
19		8129						19	8766	8994	9222	9450	9678	9905	40
20	9529	9808	87	.366	.645	.924	39	20	8.970133	0360	o 5 88	0815	1042	1269	39
	8.881202							21	1496	1723	1949	2176	2402	2628	38
22	2809 4530	3147 4807	5083	5358	3977 563/	5010	36	22						3984 5335	
24	6185	6460	6735	7010	7285	7550	35	24						6682	
25	7833	8108	8382	8655	8929	9202	34	25	6906	7130	7354	7578	7801	8025	34
26	9476	9749	22	.295	.567	.840	33	26	8248	8472	8695	8918	9141	9364	33
27 28	8 891112	3013						27	9380 8.980921					.699	
29		4636						29						3356	
30		6253						3ó	3577	3798	4018	4238	4459	4679	29
31		7864						31	4899	5119	5339	5559	5778	5998	28
32		9470						3 ₂ 33						7313	
34	8.900803 2308	2663						34						8624 9931	
35		4251							8.990149	0366	0583	0801	1018	1235	24
36	5570	5833	6096	6359	6622	6885	23	36	1451	1668	1885	2101	2318	2534	23
37	7147	7410	7672	7934	8196	8457	22	37						3830	
38	8719 8.910285	8980	0806	1066	9704	1586	21	38 39						5122 6410	
40		2106						40						7694	
41	3401	3660	3918	4177	4435	4693	18	41	7908	8122	8335	8549	8762	8975	18
42	4951	5209	5466	5724	5981	6238	17	42	9188	9401	9614	9827	40	.252	17
43	8036	6752 8290	7009	7205	7522	7778	15		9.000465					2795	
44	0568	9823	78	.332	587	.841	14	44						4061	
	8.921096	1350	1604	1858	2112	2365	13	46	4272	4483	4693	4904	5114	5324	13
47	2619	2872	3125	3378	3631	3884	12	47	5534	5744	5954	6164	6373	6583	12
48		4389						48	6792	7002	7211	7420	7629	7838	II
49	7156	5900	765	7008	8158	8/108	9	49	0047	0200	0715	0073	131	9090	10
51	8658	8908	9158	9407	9657	9906	8	51	9298 9.010546	0754	0961	1160	1376	1583	8
52	8.930155	0404	0653	0902	1150	1399	7	52	1790	1997	2204	2411	2618	2824	7 1
53		1895						53	3031	3237	3444	3650	3856	4062	6
54		338 I 4862	5100	5355	1560	14369	5 4	54 55						5297 6528	
56	6093	6339	6582	683c	7075	7320	3	56	6732	6937	7142	7346	7551	7755	3
57	57 7565 7810 8055 8299 8544 8788 2 57 7959 8164 8368 8572 8776 8979													2	
	58 9032 9276 9520 9764 7 .251 1 58 9183 9387 9590 9794 9997 .200 1													1	
1 29							0	59							0
							Min		Co-ta	150" anger	40"	30' 84 D	egree	10" s.	Min.
P.	Co-tangent of 85 Degrees. \(\overline{\pi}\) Co-tangent of 84 Degrees. \(\overline{\pi}\) P.Part \(\begin{cases} 1'' 2'' 3'' 4'' 5'' 6'' 7'' 8'' 9'' \\ 27 54 81 108 135 162 188 215 242 \end{cases} P.Part \(\begin{cases} 1'' 2'' 3'' 4'' 5'' 6'' 7'' 8'' 9'' \\ 22 44 66 88 110 132 154 177 199 \end{cases} \)														
L	. (1	(~~				101		

ੜੀ ਹੈ	S	ine o	f 6 D)egree	es.			ä	S	ine o	f 7 I	egre	es.			
Min	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	1	
0	9.019235	9435	9635	9835	35	.235	59	0	9.085894	6066	6237	6400	658o	6751	50	
	9.020435							1	6922							
2			2030					2	7947	8118	8288	8459	8629	8800	5	
3			3223					3	8970	9140	9310	9480	9651	9820	56	
4			4412					4	9990							
5			5598						9.091008	1178	1347	1516	1685	1855	54	
6	6386	6583	6780	6977	7174	7370	53	6	2024	2193	2362	2530	2699	2868	53	
7	7507	7703	7960	8130	8352	8548	52	7						3879		
8	8744	8940	9136	9332	9327	9723	51	8	4047							
9	9910	1114	.309	.504	- 099	.094	40	9						5894		
	9.031089		2645					10	6062							
I			3809					II	7065 8066	7232	7399	8566	7733	7900	4	
3	4582	6015	4060	5,60	5355	55.48	46	13	8066	0233	0399	0564	0732	0099	4	
4			6126						9065 9.100062	0227	9393	0550	9730	9890	4	
5			7280					15						1883		
6	8048							16						2873		
7			9579					17	3037	3202	3367	353T	3606	386o	14	
	9.040342							18	4025							
9			1865					19	5010	5174	5337	5501	5665	5820	140	
0	2625							20						6810		
ı			4140					21	6973							
2	4895							22	7951	8114	8277	8439	8602	8765	3	
3	6026	6214	6402	6590	6778	6966	36	23	8927 9901	9090	9252	9414	9577	9739	30	
4	7154	7342	7529	7717	7904	8091	35	24	9901	63	.225	.387	.549	.711	3	
5	8279	8466	8653	8840	9027	9214	34	25	9.110873	1034	1196	1358	1519	1681	3	
6	9400	9587	9774	9960	.147	.333	33	26	1842	2003	2165	2326	2487	2648	3	
7	5.050519							27	2809							
8	1635	1821	2007	2192	2378	2563	31	28	3774							
9	2749							29	4737	4897	5057	5218	5378	5538	30	
이	3859							30	5698	5858	6017	6177	6337	6497	20	
I	4966							31	6656							
2	6071							32	7613							
3	7172							33	8567	0720	0004	9043	9202	9300	20	
4	8271	0404	0037	0020	9002	9100	25	34	9519 9.120469	9677	9030	9994	.132	1050	20	
5	9367 9.060460	9550	9732	9914	68	1360	03	36	1417							
7			1914					37	2362	2520	2677	2835	2047	31/0	25	
8			3001					38	3306	3/63	3620	3777	303/	4001	2	
9	3724							39	4248	4404	4561	4718	4874	5031	20	
0	4806							40	5187							
I	5885							41	6125							
2	6962							42	7060							
3	8036	8215	8393	8572	8751	8929	16	43	7993	8149	8304	8459	8614	8770	16	
4	9107	9286	9464	9642	9820	9998	15	44	8925	9080	9235	9390	9544	9699	1	
5	9.070176	o354	0532	0709	0887	1065	14	45	9854	9	.163	.318	.472	.627	14	
6	1242	1420	1597	1774	1951	2128	13	46	9.136781	0936	1090	1244	1398	1552	1	
7	2306	2482	2659	2836	3013	3190	12	47	1706	1860	2014	2168	2322	2476	1:	
8	3366	3543	3719	3896	4072	4248	II	48	2630	2783	2937	3091	3244	3398	I	
9	4424	4600	4777	4952	5128	5304	10	49	3551	3704	3858	4011	4164	4317	I	
0	5480	5656	5831	6007	6182	6358	9	50	4470	4623	4776	4929	5082	5235	1	
I	6533	6708	6883	7058	7233	7408	8	51	5387	5540	5693	5845	5998	0130		
2	7583	7758	7933	8107	8282	8457	7	52	6303	260	0007	0700	0912	7004	1	
3	8631 9676	8805	8980	9154	9328	9502	6	53	7216							
4	9676	9850	24	.198	.372	.545	5 4	54 55	8128 9037							
	9.080719	0892	1000	1239	1413	1080	3		9037	9100	9340	308	5/8	600		
6	1759	1932	2105	2278	2401	365	2	56	9944 9.140850	1007	. 247	1300	1/53	1603		
78			3142				1 1	58	9.140050	1001	2055	2205	2355	2505		
9			4176 5208				I	59	2655	2806	2056	3106	3256	3405		
1							-	19	60"	50"	40"	30"	20"	10"		
	60"	50"	40"	30"	20"	10"	Min.				L		<u>'</u>	1 10	N.	
1	Co-	sine	of 83	Degr			9"					$\frac{\text{Deg}}{5'' - 6''}$			9	
			4" 5		7"	8'			D (1" S	2" 3"			7"	8"		

	Tangent of 6 Degrees. E Tangent of 7 Degrees.														3
Min.	Tai					Eo#		Min.	0"	ngent	20"	Deg	rees.	50"	
	9.021620	1803	20"	30"	2/30	0630	50		9.089144						50
0		3036							9.090187						
2		4245						2					1920		
3	5251	5452	5653	5853	6054	6254	56	3					2957		
4	6465	6655	6855	7055	7255	7455	55	4					3991		
5		7855						5	4336	4508	4680	4851	5023	5195	54
6	9.030046	9052	9251	9450	9049	9848	50	6					6053 7080		
8		1435						7 8					8105		
9		2623						9	8446	8616	8787	8957	9127	9298	5o
10		3806						10					. 148		
11		4987						11	9.100487						
12		6165						12					2181		
13	7144	7339	7535	7730	7925	8121	46	13					3194		
15		8511 9679						14					4205 5214		
	9. 04 0651							16					6221		
17		2007						17					7225		
18	2973	3166	3359	3552	3745	3937	41	18	7559	7726	7893	8060	8227	8394	41
19	4130	4322	4515	4707	4899	5002	40	19	8560	8727	8894	9060	9227	9393	40
20	5284	5476	5668	5859	6051	6243	39	20	9559	9726	9892	58	.224	.390	39
21	0434	6626	0817	7009	7200	7391	36		9.110556						
23	7302	7773 8917	7904	0100	0340	0650	36	22 23					2213 3204		
24		59						24	3533	3608	3863	1028	4192	4357	35
	9.051008	1107	1387	1576	1766	1055	34	25					5179		
26	2144	2333	2522	2711	2900	3688	33	26	5507	5671	5835	5999	6163	6327	33
27	3277	3466	3654	3843	4031	4219	32	27	6491	6655	6818	6982	7145	7309	32
28	4407	4596	4784	4972	5159	5347	3 r	28	7472	7636	7799	7962	8126	8289	31
29		5723						29					9104		
30 31	0009	6847	7034	7221	7408	7594	29	30					••79		
32		7 9 68 9086						32	9.120404				2025		
	9.060016	0202	0388	0573	0750	0044	26	33	2348	2510	2671	2833	2994	3156	26
34	1130	1315	1500	1685	1870	2055	25	34					3962		
35	2240	2425	2610	2795	2979	3164	24	35					4927		
36	3348	3533	3717	3901	4085	4269	23	36					5891		
37	4453	4637	4821	5005	5188	5372	22	37					6852		
38	6655	5739	5922	0100	0289	6472	21	38					7811		
39 40	7752	6838 7935	8117	8300	8/82	8664	20	39 40					8768 9723		
41		9029							9.130041	0200	0350	0518	0676	0835	18
42	9938	.120	.301	.483	.664	.846	17	42	0994	1152	1311	1469	1628	1786	17
43	9.071027	1208	1389	1570	1751	1932	16	43	1944	2102	2261	2419	2577	2735	16
44	2113	2294	2475	2655	2836	3016	15	44	2893	3050	3208	3366	3524	3681	15
45	3197	3377	3558	3738	3918	4098	14	45		3997	4154	4312	4469	4626	14
46 47	4278 5356	4458 5536	4038	4317	4997	6052	13	46					5412 6353		
47	6/32	6611	6700	6060	71/8	7327	12	47 48					7292		
49		7684						49		7761	7018	807/	8230	8386	10
50	8576	8754	8932	9110	9288	9466	9	50	8542	8608	8854	9009	9165	9321	9
51	9644	9822		1.177	.355	.532	8	51	9476	9632	9788	9943	98	.254	8
	9.080710	0887	1064	1241	1419	1596	7		9.140409	0564	0720	0875	1030	1185	7 6
53		1950						53					1959		
54 55		3010						54					2887		5
56	. ,	4067 5122						55					3813 4737		3
57		6175						57	50//	5108	535 T	5505	5659	5810	2
58		7225						58	5066	6110	6272	6425	6579	6732	ī
59	8098	8273	8447	8621	8795	8970	0	59		7038	7191	7344	7497	7650	0
	60"	50"	40"	30"	20"	10"		-	60"	50"	40"	30"	20"	10"	
	Co-ta	ingen	t of 8	83 D	egree	s.	Min.		Co-ta	ingen	t of	82 D	egree	s.	Mir.
p	Part \ 1"	2" 3"					9"	n	(1"		4"			8"	9"
1.	rart { 19 ;	3 7 56	75 9	94 119	2 131			r.					114	130	
								'							

., 2				-			Sine of 9 Degrees.								
Min	- S	ine o	# 8 I	egree 30"	40"	50'		Min.	S 0"	ine o	f 9 I ┌ 20″			T Four	
-	9.143555						50	lL	9.194332			30" 4731	4864	4005	50
I	4453	46o3	4752	4902	5051	5200	58	I	5129	5262	5395	5527	566o	5792	58
2				5797				2	5925	6057	6189	6322	6454	6586	57
3				6690 7581				3	6719	6851	6983	7115	7247	7379	56
5				8471				4 5	8302	8/3/	8565	8607	8828	8170 8960	33 5/
6				9358				6	9091	9223	9354	9486	9617	9748	53
7				.244				7	9879	11	. 142	.273	.404	.535	52
1	9.150686								9.200666						
10				2010 2891				9						2104 2886	
111	3330	3476	3623	3769	3915	4061	48	11	3017	3147	3277	3407	3537	3667	48
12	4208	4354	4500	4646	4792	4938	47	12						4447	
13				5521				13						5225	
14	5957 6830	6075	0248	6394 7265	0539	D555	45	14	5354	5484	5613	5743	5872	6002 67 7 7	45
16	7700	7845	7000	8135	8270	8424	44	15 16	6006	7035	7164	7203	7422	7551	44
17	8569	8713	8858	9002	9147	9291	42	17	7679	7808	7937	8066	8194	8323	42
18	9435	9580	9724	9868	12	.156	41	18	8452	858o	8709	8837	8966	9094	41
	9.160301	0445	0589	0732 1595	0876	1020	40	1,0	9222	9351	9479	9607	9735	9864 .632	40
20				2456				20	9992 9.210760	0888	1015	.370 11/3	1271	1300	38
22				3315				22	1526	1654	1781	1909	2037	2164	37
23	3743	3886	4029	4172	4314	4457	36	23	2291	2419	2546	2674	2801	2928	36
24	4600							24						3691	
25 26	6307			5881				25 26	4579	3945	4071	4198	4325	4452	34
27				7584				27	5338	5465	55aı	5718	5844	5970	32
28				8432				28	6097	6223	6349	6475	6601	6728	31
29	<i>6</i> 856	8997	9138	9279	9420	9561	3о	29	6854	6980	7106	7232	7358	7483	30
30	9702	9843	9984	.125	.265	.406	29	30	7609	7735	7861	7987	8866	8238	29
32	9.170547			1810				31 32	9116					8991	
33				2650				33	9868	9993	.118	.243	.368	.493	26
34	3070								9.220618						
35	3908							35						1990	
36 3 ₇	4744 5578							36 37						2737 3482	
38	641.							38						4226	
39	.7243	7381	7510	7657	7796	7934	20	39	4349	4473	4597	4721	4845	4968	20
40	8072							40						5709	
41	8900 9726	9038	9176	9313	9451	9589	18	41	5833 65=3	5956	6810	6040	0320	6449 7188	18
.12	9.180551							42	7311	7434	7557	7680	7803	7925	16
4.	1374	1511	1648	1785	1922	2059	15	44	8048	8171	8294	8416	8539	8661	15
45	2106	2333	2460	2606	2743	2879	14	45	8784	8906	9029	9151	9274	9396	14
46	3016	3152	3289	3425	3562	3698	13	46						.130	
47 48	3834 4651	3971 1987	4107	5050	4379 5105	533T	12	47	9.230252					1593	
49	5466	5602	5738	5874	6000	6145	10	49	1715	1836	1958	2079	2201	2323	
50	6280	6416	655ı	6686	6822	6957	9	50	2444						9
51	1092	7228	7363	7498	7633	7768	8	51	3172	3293	3415	3536	3657	3778	
52 53	903 9,12	884-	8087	03.08	0442	0385	7	52 53	3899 4625	4020	4141	4202	4303 5108	5220	7 6
54	e5.0	065/	0788	9110	57	.101	5	54	5349						5
55	9.190325	0460	0594	0728	0862	0996	4	55	6073	6193	6313	6434	6554	6674	4
56	1130	1264	1398	1532	1665	1799	3	56	6795	6915	7035	7155	7275	7395	3
57	1933	2066	2200	2334	2467	2601	2	57 58	7515 8235	7035	7755	7875 850/	7995	883/	2 I
58 59	2734 3534						I 0	59	8g53						0
	60"	50"	40"	30"	20"	10"		- 7	60"	50"	40"	30"	20"	10"	
				Degr			Min.		Co-	sine o	of 80	Degr	ees.		Min.
	(1" 0	11 911	A'I =	11 611	~//	8" 9	,,,	P		2" 3"	4"	5" 6"	7"		ð
Ρ.	f'art \ 14 2	8 42	56 7	0 85	99	13 19		r.	Part \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	25 38	50 6	3 75	88	101 1	13

	To	ngoni	ofs	Deg	rees				То	ngeni	t of 9	Dec	rees		7
Min	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	-
0	9.147803	7955	8108		8413	8566	59	0	9.199713	9849	9985	.121	.257	.393	59
1	8718	8871	9023	9175	9328	9480	58	I	9.200529					1209	58
2	9632	9784	9936	.88	.240	.392	57	2					1888		
3	9.150544							3	2159	2294	2430	2505	2701	2836	56
5				1909				5	2971	3018	1053	13377	3512 4322	3047	5.
6				2816 3722				6					5131		
				4626				7					5938		
8				5528				8					6744		
9	5978	6128	6278	6428	6578	6728	50	9					7549		
IO.	6877	7027	7177	7326	7476	7625	49	ΙÓ	7817	7950	8084	8218	8352	8485	49
11				8223				11					9153		
12				9118				12					9954		
13				11					9.210220						
15	9.160457							14					1550 2346		
16				1792 2680				16					3141		
17				3566				17					3934		
18	4008							18	4198						
19				5333				19	4989	5121	5253	5385	5516	5648	40
20				6214				20					63o5		
21	6654	6800	6947	7093	7240	7386	38	21	6568	6700	6831	6962	7093	7225	38
22	7532	7678	7825	7971	8117	8263	37	22	7356	7487	7618	7749	7880	8011	37
23 24	8409	8333	0701	8847	0992	9138	30	23	8142						
1	9284 9.170157	0303	0448	0503	9000	0884	3/	24 25	8926						
26				1464					9.220492				.231		
27				2333				27					1792		
28				3201				28					2571		
29	3634							29	2830	2959	3089	3218	3348	3477	30
30	4499	4643	4787	4931	5075	5218	29	30					4124		
31	5362							31	4382						
32 33	6224							32					5671		
34				7513 8371				33 34					6443		
35	8799							35	6700	7500	9997	7855	7983	8111	2/
36	9655							36	8230	8368	8406	8623	8751	8870	23
37	9.180508							37	9007						
38	1360	1502	1644	1786	1027	2069	21	38					.284		
39	2211	2352	2494	2635	2777	2918	20	39	9.230539						
40	3059							40					1811		
41	3907 4 7 52							41					2573		
43	5597							42 43					3333 4092		
44	6439	6570	6720	6860	7000	71/10	15	44	4345						
45	7280	7420	7560	7700	7840	7980	14	45	5103	5229	5355	5481	5607	5733	14
46	8120	8259	8399	8539	8678	8818	13	46	5859	5985	6111	6237	6362	6488	13
47	8958	9097	9236	9376	9515	9655	12	47	6614	6740	6865	6991	7117	7242	12
48	9794	9933	72	.212	.351	.490	11	48	7368	7493	7619	7744	7870	7995	11
	9.190629	0768	0907	1046	1184	1323	10	49	8120						10
50				1878			9	50	8872	8997	9122	9247	9372	9497	3
51 52	2294						8	51	9622 9.240371	9747	9072	9996	0860	.246	8
53	3124 3953	1001	/220	436	1505	1610	7 6	53	9.240371						7 6
54	4780	4018	5056	5103	533 t	5468	5	54	1865						5
55	5606	5743	588ı	6018	6156	6293	4	55	2€10						4
56	643o	6567	6705	6842	6979	7116	3	56	3354						3
57	7253	7390	7527	7664	7801	7938	2	57	4097	4221	4345	4468	4592	47i5	3
58	8074	8211	8348	8484	8621	8758	1	58	4839	4962	5086	5209	5333	5456	I
59	8894						0	59	5579	5703	5826	5949	6072	6196	0
	60"	50"	40"	30"	20"	10"	ri i		60"	50"	40"	30"	20"	10"	ä
-	Co-tar	igent	of 8	1 De	grees		Min.		Co-ta	ngent	of 8	0 De	grees.		Min.
P			4" 5	5" 6" 72 86			"	ъ	$\operatorname{Part} \left\{ egin{array}{ll} 1'' & \S \\ 13 & \S \end{array} ight.$!" 3"	4" 5	6" 6"	7"	8" 9)"

Min.			10 I					Min.		ne of	11	Degre	es.	
2	0"	10"	20/	30"	40"	50′		Ξ	0"	10"	20"	30"	40"	50"
0	9.239670	0700	0000	28	. 148	.267	50	0	9.280599	0707	0815	002/	1030	77/10
	9.240386								12/8	1356	T 465	1553	7687	1140
								I	- 0	1330	1405	1573	1001	1709
2			1339					2	1897	2005	2113	2220	2328	2436
3			2052					3	2544	2652	2760	2867	2975	3083
4	2526	2645	2763	2882	3001	3110	55	4	3190	3208	3406	3513	3621	3728
5			3474					5	3836	30/3	405 T	4158	1266	/373
6			4184					6	448o	1588	1605	4800	4000	5070
)									4400	4300	4095	4002	4909	3017
78			4892					7 8	5124	3231	5338	5445	5552	15659
8	5363	5481	5599	5717	5834	5952	51	8	5766	5873	5980	6087	6194	6301
9	6069	6187	63o5	6422	6540	6657	5o	9	6408	6514	6621	6728	6835	6041
10			7009					10	7048	7155	7261	7368	7/17/	7581
11			7713						7688					
- 1	7470	7090	01-5	0520	1941	0-66	40	II						
12			8415					12	8326					
13	8883	8999	9116	9233	9350	9466	46	13	8964	9070	9176	9282	9388	9494
14	9583	9700	9816	9933	49	.166	45	14	9600	9706	0812	9018	24	.130
15	9.250282	o3aa	0515	ó631	0748	0864	44		9.290236	03/12	0//17	6553	0650	0765
16			1213					16						
- 1								1 1	0870					
17	1077	1793	1909	2023	2141	2237	42	17	1304	1010	1713	1820	1920	2031
18	2373	2489	2605	2720	2836	2952	4 1	18	2137	2242	2347	2453	2558	2663
19	3067	3183	3299	3414	353o	3645	40	19	2768	2874	2979	3084	3189	3204
20	3761	3876	3992	4107	4223	4338	30	20	3399	350/	3600	371/	3816	302/
21	4453	4568	4684	%700	1011	5020	38	21	4029					
- 1	5-11	5050	52-4	4/99	56-1	5-29	2-							
22			5374					22	4658	4703	4007	4972	2077	2191
23	5834	5949	6064	6179	6294	6409	36	23	5286	5391	5495	5600	5704	580g
24	6523	6638	6753	6867	6982	7096	35	24	5913	6017	6122	6226	633o	6435
25	7211	7326	7440	7554	7660	7783	34	25	6539	6643	6747	6852	6056	7060
26			8126					26	7164					
- 1								1 1						
27	0303	0097	8811	0920	9040	9134	32	27	7788					
28	9268	9382	9495	9609	9723	9837	31	28	8412	8515	8619	8723	8827	8930
29	9951	65	. 178	.292	.406	.519	3o	29	9034	9138	9241	9345	9448	9552
30	9.260633	0747	0860	0074	1087	1201	20	3ó	9655	0750	0862	0066	60	.172
31			1541						9.300276	0370	0/82	0586	0680	0702
32			2220					32	0895	0000	7.7.00	1005	1308	7/92
- 1									0093	0999	1102	-0-3	1300	1411
33			2899					33	1514					
34			3576					34	2132	2235	2337	2440	2543	2646
35	4027	4140	4253	4365	4478	4590	24	35	2748	2851	2954	3057	3159	3262
36			4928					36	3364					
37			5602					37	3979					
38	0031	0103	6275	0307	0499	0011	21	38	4593					
39	6723	6835	6947	7059	7171	7283	20	39	5207					
40	7395	7506	7618	7730	7841	7953	19	40	5819	5921	6023	6125	6227	6328
41	8065	8176	8288	8300	8511	8622	18	41	643o	6532	6634	6736	6837	6030
42	873/	88/15	8957	ഹര്ള	0170	0201	17	42	7041					
43	0/04	25.3	2624	9000	9. /9	9292	-6		7650	7750	-853	7055	8056	8 - 58
			9624					43	7050	7752	7033	7933	0000	0130
1 4 1	9.270069							44	8259	8300	8402	8303	8004	8700
45	0735	0846	0957	1067	1178	1289	14	45	8867	8968	9069	9170	9272	9373
46	1400	1510	1621	1732	1842	1953	13	46	9474	9575	9676	9777	9878	9979
47			2285					177	9.310080	6181	0282	0382	0/83	0584
48			2947						0685	0486	0886	0085	1088	1180
. 1								48						
49	3300	3490	3608	3710	3029	3939	10	49	1289					
50	4049	4159	4269	4379	4489	4598	9	50	1893					
51	4708	48 i 81	4028	5038	5148	5257	8	51	2495	2595	2696	2796	2896	2997
52	5367	5/177	5586	5606	5805	5015	7	52	3097					
53	6005	6.34	6243	6353	6/60	65.70	6	53	3698					
									3090	1390	1/0-	1500	4690	4190
54			6900				5	54	4297	4397	4497	4397	4097	4797
55	7337	7446	7555	7664	7773	7882	4	55	4897	4996	5096	5196	5295	5395
56	7991	8100	8209	8318	8427	8536	3	56	5495	5594	5694	5793	5893	5993
57			8862				2	57	6092	6102	6201	6300	6/100	6580
58							- 11	58						
			9514				1	- 1	6689					
59	9948	57	. 165	.274	.382	.491	0	59	7284	7383	7482	7302	7001	
	60"	50"	40"	30"	20"	10"	۰		60"	50"	40"	30"	20"	10"
-	Co	sine d	of 79				Min.		Co	sine (f 78	Deg	rees	
	C0-1	otite (וו ווו	Degr	CCS.	- 1	~		C0-	onie (110	T CB		
		3"	4" :	5" 6"	7"	8" 9	"		D \ 1" S	2" 3"	4"	5″ €	3" 7"	8"

Min	Lan									Thon	mant	∧+ 11	1)00	DOOM		1
	0"	10"	20"	Deg	40"	50"		Min.	L	0"	10"	of 11	30"	40"	50"	
0	9.246319						50	0	9.	288652						59
1	7057	7180	7303	7426	7548	7671	58	I	1	9326	9438	955 r	9663	9775	9887	58
2	7794	7917	8039	8162	8285	8407	57	2				.223				
3	026/	038	0500	8897	9020	0876	55	3	9.	290671		1566				
5	9204	120	.242	9631 .364	.486	.608	54	5				2236				
- 1	9.250730							6		2682	2793	2905	3016	3127	3239	53
7 8				1826				7	j			3572				
				2556				8				4239				
9				3284 4011				10				4905 5571				
II	4374	4495	4616	4737	4858	4979	48	II				6235				
12	5100	5221	534 t	5462	5583	5703	47	12				6898				
13	5824	5945	6065	6186	6306	6427	46	13				7560				
14	7260	7380	0700	6908 7630	7029	7149	45	14				8221 8882				
16				835o				16				9541				
17	8710	8830	8950	9069	9189	9309	42	17				.200				
18	9429	9548	9668	9787	9907	27	41	18	9.	300638						
- 1	9.260146			0504				19				1514				
20 21				1935				20				2825				
22				2649				22				3479				
23	3005	3124	3243	3361	348o	3599	36	23		3914	4023	4132	4241	4349	4458	36
24				4073				24				4784				
25 26				4783 5493				25 26		5218 5860	5077	5435 6o86	5544	6300	6/10	33
27	5847	5065	6083	6201	6310	6437	32	27		6519	6627	6735	6843	6051	7050	32
28	-6555							28				7384				
29				7614				29				8031				
30	7967	8084	8202	8319	8437	8554	29	30				8678				
31 32	0375	0/02	0600	9023 9726	08/3	9235	27	31 32		9109	0862	9324 9969	9432	. 184	201	27
	g.270077	0194	0311	0428	0545	0662	20	1 1	9.	310399						
34				1129				34	ľ			1256				
35				1829				35				1899				
36	2178	2294	3100	2527 3225	2044	2700	23	36 3 ₇				2540 3181				
38				3921				38				3821				
39	4269	4385	4501	4617	4733	4849	20	39	İ	4247	4353	4460	4566	4672	4779	20
40	4964	5080	5196	5312	5427	5543	19	40				5098				
41				6005 6698				41				5735 6371				
43				7389				42				7007				
44	7734	7849	7964	8079	8194	8300	15	44		743o	7536	7641	7747	7853	7958	15
45	8424	8539	8654	8769	8884	8998	14	45				8275				
46	9113	9228	9342	9457	9572	9686	13	46		8697	8803	8908	9013	9119	9224	13
47 48	9.280488	0602	0717	0831	00/15	1050	12	47 48				9540				
49	1174	1288	1402	1516	1630	1744	10	40	9.	320592	0697	0802	0907	1012	1117	10
50	1858	1973	2087	2201	2314	2428	9	50		1222	1326	1431	1536	1641	1746	9
51		2656	2770	2884	2998	3111	8	51	1	1851	1955	2060	2165	2269	2374	8
52 53	3007	1021	3453	3566 4248	1360	3793	7 6	5 ₂		2479 3106	3211	2688 3315	3/20	3504	3628	7 6
54	4588	4701	4815	4928	5041	515/	5	54		3733	3837	3941	4046	4150	4254	5
55	5268	5381	5494	5607	5720	5833	4	55		4358	4463	4567	4671	4775	4879	4
56	5947	6060	6173	6286	6399	6512	3	56	1	4983	5087	5191	5295	5399	5503	3
57 58				6963				57		5507	6337	5815 6438	5919	6646	6127	2
59				7639 8315				58		6853	605	7060	716	7267	7371	0
7	60"	50"		30"	20"	10"		19	-	60″	50"	40"	30"	200	10"	-
	~			79 De	-	<u> </u>	Min.		\vdash			t of	1			Min
P	D- 1 1"	2" 3"	4"	5" 6'			9"	D	D.	(1//		" 4"		6" 7'		9"
	1art (12 9	23 35	47	59 70	82	94 1	06	F.	Pa		22 3	2 43	54	65 75	86	97

d	Si	ne of	12 1	Degre	es.				Si	ne of	13]	Deore	es.		Γ
Min.	07	10′		30"	40"	50"		Min.	0"	10"	20"		40"	507	
0	9.317879	7978	8077	8176	8275	8374	59	0	9.352088	2179	2270	2362	2453	2544	5
I				8769				1	2635	2726	2817	2908	2999	3000	5
2	9066	9165	9263	9362	9461	9559	57	2	3181	3272	3363	3454	3545	3636	5
3	9658	9757	9855	9954	52	.151	56	3	3726	3817	3908	3999	4000	4180	5
	9.320249	o348	0446	0545	0643	0742	55	4	4271	4362	4452	4543	4634	4724	15
5	0840	0938	1037	1135	1233	1332	54	5	4815	4906	4996	5087	5177	5268	5.
6				1724				6	5358	5449	5539	563o	5720	5810	5
78				2313				7	590I	5991	6081	6172	6262	6352	5
8	2607	2705	2802	2900	2998	3096	5 r	8	6443	6533	6623	6713	6803	6894	5
9				3487				9	6984	7074	7164	7254	7344	7434	5
	9.323780	3878	3975	4073	4171	4268	49		9.357524						
I	4366	4463	4561	4658	4756	4853	48	II	8064	8154	8243	8333	8423	8513	4
2	4950							12	8603	8692	8782	8872	8962	9051	4
3				5826				13	9141	9231	9320	9410	9499	9589	4
4				6409				14	9678	9768	9858	9947	36	.126	4
5	6700	6797	0894	6991	7087	7184	44		9.360215	0305	0394	0484	0573	0662	4
6	7281	7378	7475	7572	7668	7705	43	16						1198	
7				8152				17	1207	1370	1405	1004	1044	1733	4
8	8442							18	1822	1911	2000	2089	2178	2267	4
9	9021							19	2330	2445	2004	2023	2711	2800	4
0	9.329599	9090	9791	9000	9984	80	39		9.362889						
- 1	9.330176							21						3865	
2				1041				22	1105	4042	4131	4220	4300	43.97	3
3				1616				23	4400	4374	4002	4731	4839	4927	3
4				2191				24	5010	5104	2193	5281	2309	5457	3
5	2470	2070	2009	2764	2000	2930	22	25	5540	6-62	6722	2010	2099	5987	3
6	3031	3147	20-7	3337	3433	3328	33	26						6516	
7				3910				27						7044	
8	4195							28						7571	
9	4767							29	268185	8073	936+	9//8	8536	8604	0
31	9.335337							31	9.368185						
32				6191				32						9149	
3				6759				33	9250	0848	9411	9499	9300	9673 .197	2
34	7643	7137	7202	7326 7893	7421	9080	0.5		9.370285	0370	0450	05/6	0634	197	2
5	8176	8007	8365	8/50	8553	8648	0/1	35						1243	
6	8742							36						1765	
7	0307	0/01	0/05	0580	0683	9212	20	37						2287	
8	9 ³ 07 9 ⁸ 71	006/	58	750	2/6	3/1	21	38						2807	
	9.340434	0528	0621	0715	0800	0003	20	39						3327	
	9.340996								9.373414						
I				1839				41						4365	
2	2119							42	4452						
3	2679							43						5401	
4				3518				44	5/187	5573	5650	5745	5831	5917	I
5	3707	3800	3083	4076	4160	4262	14	45	6003	6080	6175	6261	6347	6433	I
6	4355	4448	4541	4634	4727	4820	13	46						6949	
7	4912							47						7464	
8	546a	5561	5654	5747	583a	5032	11	48	7540	7635	7721	7806	7802	7978	I
9				6302				49	8063	8149	8235	8320	8406	8491	I
	9.346579							50	9.378577	8662	8748	8833	8910	9004	
I	7134	7226	7318	7410	75o3	7505	8	51	9089	9175	9260	9346	9431	9516	1
2	7687	7770	7871	7963	8056	8148	7	52	9601	9687	9772	9857	9942	28	
3	8240	8332	8424	8516	8608	8700	6	53	9.386113	0198	0283	o368	0454	0539	1
4	8792	8884	8976	9067	9159	9251	5	54						1049	
5	9343	9435	9526	9618	9710	9802	4	55						1559	1
6	9893	9985	77	.168	.260	.352	3	56						2069	
7	9.350443	o535	0626	0718	0800	0001	2	57						2576	
8	0992	1084	1175	1266	1358	1449	1	58	2661	2745	2830	2914	2999	3084	:
9	1540	1632	1723	1814	1906	1907	0	59					3566		
-	60"	50"	40"	30"	20"	10"		-	60"	50"	40"	30"	20"	10"	+
				Degr			Min.				of 76	l			Min
		2" 3"			.ees.	8"	9"	-		2" 3		5"		8"	9/

Γ.	Ton	rent	of 19	Da~				Γ.	Тог	orent	of 15	The	grees.		
Min	0''	10"	20"	2 Deg 30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	
0								0	0.363364						
1 2				8405 9025				1 2					4324 4899		
3				9644				3	5090	5186	5282	5377	5473	5568	56
4	9953	56	.159	.262	.365	.468	55	4	5664	5760	5855	595 r	6046	6142	55
5 6	9.330570							5					6619		
7				1495 2111				6	7382	7477	7572	7668	7191 7763	7858	52
8	2418	2521	2623	2726	2828	2930	5 r	8	7953	8048	8143	8239	8334	8429	5 I
9	3033	3135	3237	3340	3442	3544	50	9					8904		
10	9.333646	3748 4361	4463	4565	4667	4137	49 48	11	9.369094	9189	0853	9378	9473	9208	49 48
12	4871	4973	5075	5177	5279	5380	47		9.370232						
13	5482	5584	5686	5788	5 889	5991	46	13	0799	0894	0989	1083	1178	1272	46
14	6093	6194	6296	6398	6499	6601	45	14					1744		
15 16				7007 7615				15 16					2311 2876		
17				8223				17					3441		
18				883o				18					4005		
19	9133 9.339739			9436				19	4193 9.374756				4569		
20	9.340344	0445	0546	0646	0747	0848	38	21					5694		
22				1250				22	5881	5975	6068	6162	6255	6349	37
23				1853				23	6442	6536	6629	6723	6816	6910	36
24 25				2456 3057				24					7376		
26				3658				25 26					7936 8495		
27				4258				27					9053		
28	4558	4658	4758	4858	4957	5057	3 r	28	9239	9332	9425	9518	9611	9704	3 r
29	9.345755			5456				29	9797 9.38o354	9890	9983	0630	.168	.201	30
31				6651				3r					1280		
32	6949	7049	7148	7248	7347	7446	27	32	1466	1558	1651	1743	1836	1928	27
33	7545	7645	7744	7843	7942	8042	26	33					2390		
34 35				8438 9032				34					2944 3497		
36	9329	9428	9527	9626	9724	9823	23	36					4050		
37	9922	21	.120	.218	.317	.416	22	37	4234	4326	4418	4510	4602	4694	22
	9.350514							38	4786	4878	4970	5062	5153	5245	21
39	9.351697			1401				39 40		5070	6071	6163	5704 6254	5790 6376	20
41	2287	2385	2483	2582	2680	2778	18	41	6438	6529	6621	6712	6804	6895	18
42	2876	2974	3073	3171	3269	3367	17	42	6987	7078	7170	7261	7353	7444	17
43				3759				43					7901		
44 45				4347 4934				44					8449 8996		
46				5520				46					9542		
47	5813	5910	60 0 8	6105	6203	6300	12	47	9724	9815	9906	9997	88	.179	12
48	6398	6495	6593	6690	6787	6885	II		9.390270	0361	0452	0543	0633	0724	II
49 50	9.35 7 566	7663	7177 7760	7274 7857	7054	7409 8052	9	49 50	9.391360				1178		9
51	8149	8246	8343	8440	8537	8634	8	51	1903	1994	2085	2175	2266	2356	8
52	8731	8828	8925	9022	9119	9216	7	52	2447	2537	2628	2718	2808	2899	7
53 54	9313 9893	9409	9506	9603	9700	9797	6 5	53 54					3351 3892		6 5
	9.360474	0570	0667	0763	0860	0057	4	55					4433		4
56	1053	1150	1246	r343	1439	r 535	3	56	4614	4704	4794	4884	4974	5064	3
57				1921			2	57	5154	5244	5334	5424	5514	56o4	2
58 59				2499 3076			I	58 59					6053 6592		I
9	60"	50"	40"	30"	20"	10"			60"	50"	40"	30"	20"	10"	0
	Co-ta				1		Min.		Co-ta						Min.
10		2" 3"			" 7"	- 1	9"		(1//	2" 3"			6" 7"		9"
		20 30	40	50 E	0 70		90	P.		19 28	3 37	46	56 65		8 3

<u>.</u>	s	ine of	14	Degre			T		SIN	Sine of	15]	Dogw			
Min	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	
0									9.41299	6 3075	3153	3232	3310	3389	59
1 2	4182	4200	4856	4435 4940	5024	5108	57	1 2	393	7 3546 8 4016	4005	4173	4252	3860 4330	58
3	5192	5277	5361	5445	5529	5613	56	3	440	8 4486	4565	4643	4721	4800	56
5				5949 6452				5	487	8 4956 7 5425	55034	5112	5190	5269	55
6	6704	6788	6872	6955	7030	7123	53	6	581	5 5893	5071	6040	6127	6205	53
7	7207	7290	7374	7458	7541	7625	52	7	628	3 6361	6439	6517	6595	6673	52
8	7709	7792	7876	7959 8461	8643 8544	8607	50	8	675	1 6828 7 7295	6906	6984	7062	7140	51
10	9.388711	8794	8878	8961	9044	9128	49	9	9.41768	4 7761	7839	7917	7994	8072	44
11	9211	9294	9378	9461	9544	9627	48	11	815	0 8227	8305	8382	8460	8537	48
13	9711 9.390210			9960				13	007	5 8692 9 9 1 5 7	8770	0312	0380	9002	47
14				0957				14	954	49621	9698	9776	9853	9930	45
15	1206	1289	1371	1454	1537	1620	44		9.42000	7 0085	0162	0239	0316	0393	44
16	1703 2100	2282	2365	1951 2447	2034 2530	2117 2613	43	16	047	0548 3 1010	1082	116/	0779	1318	43
18	2695	2778	286o	2943	3025	3108	41	18	139	5 1472	1549	1626	1703	1780	41
19				3438				19	185	7 1933	2010	2087	2164	2241	40
20	9.393685			4426				20	9.42231	3 2394 3 2855	2471	3008	3085	3161	38
22	4673	4755	4837	4919	5002	5084	37	22		3315					
23	5166	5248	533o	5412	5494	5576	36	23	369	7 3774	385o	3927	4003	4080	36
24 25				5904 6395				24	413	6 4233 5 4691	4309	4844	4402	4006	34
26	6641	6723	68o5	6886	6968	7050	33	26	507	3 5149	5225	5301	5378	5454	33
27	7132	7213	7295	7377	7458	7540	32	27		5606					
28 29	7021	7703	7700 8274	7866 8355	7940 8437	8518	30	28 29		7 6063 3 6519					
30	9.398600	868ı	8762	8844	8925	9007	29	30	9.42689	6975	705 I	7127	7202	7278	29
31	9088	9169	9250	9332	9413	9494	28	31 32	735	7430	7506	7582	7657	7733	28
	9.400062	0144	0225	9819 0306	0387	0468	26	33		7885 8339					
34	0549	o63o	0711	0792	0873	0954	25	34	871	8792	8868	8944	9019	9095	25
35 36				1277 1762				35 36	917	9246 9698	9321	9397	9472	9547	24
37				2247				1 1	9.43007	0150	0226	0301	0376	0451	22
38	2489	2570	265 0	2731	2811	2892	21	38	052	0602	0677	0752	0828	0903	21
39	297 2 9.403455	3053	3133 3616	3607	3294	3375	20	39	0978 9.43142	1053					
41	3938	4018	4098	4179	4259	4339	18	41	187	1954	2029	2104	2179	2254	18
42	4420	4500	458o	466o	4741	4821	17	42	232	2403	2478	2553	2628	2703	17
43				5141 5622				43 44		3 2853 3 3301					
45	5862	5942	6022	6102	6181	6261	14	45	367	3749	3824	3898	3973	4048	14
46	6341	6421	6501	6581	6661	6740	13	46		4197					
47	7200	7378	7458	7060 7538	7139	7219	12	47 48	501	4644 5091	4718 5165	4793 5230	5314	4942 5388	11
49	7777	7856	7936	8015	8095	8174	10	49	546:	5537	5611	5685	5760	5834	10
50 51	9.408254						9	50 51	9.435908	3 5982 3 6427	6556	6526	6650	6279	9
52	8731 9207	9286	9365	9445	9524	g6o3	7	52	6798	8 6872	6946	7020	7094	7168	
53	9682	9762	9841	9920	9999	78	6	53	724:	2 7316	7390	7464	7538	7612	6
54 55	9.410157 0632						5	54 55		7760 8203					7 6 5 4
56	1106						3	56		8646					3
57	1579	1658	1737	1816	1895	1973	2	57	9014	19088	9162	9235	9309	9382	2
58 59	2052 252/	2603	2210 2682	2288 2760	2367 2830	2446	0	58 59	9450	9530 9971	9603	9077	9750	265	0
- 9	60"	50"	40"	30"	20"	10"		- 9	60"	50"	40"	30"	20"	10"	
	Co-	sine o		Degr			Min.		Co	-sine			rees.		Min.
P.	Part 5 1" S	2" 3"	4"	5" 6	″ 7″		9"	P.	$\operatorname{Part} \left\{ \begin{array}{l} 1'' \\ 8 \end{array} \right.$	2" 3"			3" 7"	~	9"
	8	16 24	33	41 4	9 57	65	73		8 (***	15 23	3 30	38 4	6 53	61	99

Γ.	Tan	runt		Deg		тн			Tan			Deg	rees		
Min	- 0 "	10"	20"	30"	40"	50″		Min	0"	10"	20"	30"	40"	50"	i
0	9.396771	6861	6950	7040	7130	7219	59	0	9.428052	8137	8221	8305	8389	8473	59
I	7309	7399	7488	7578	7667	7757	58	I	8558						
1 3				8115 8651				3	9062 0566					9482	
4				9187					9.430070						
5	9455	9544	9633	9722	9811	9900	54	5	0573	0657	0740	0824	0908	0992	54
6	9990	79	. 168	.257	.346	.435	53	6	1075	1159	1243	1326	1410	1494	53
8	9.400524			1325				8						1995 2496	
9				1857				9						2997	
10	9.402124								9.433080						
11	2656	2744	2833	2922	3010	3099	48	ΙΙ						3997	
12				3453 3983				13	4080 4579					4496	
14				4514				14						5493	
15				5043				15	5576	5659	5742	5825	5907	5990	44
16				5572				16	6073						
17				6608				17	6570						
19				6628 7155				18	7563	7646	7728	7811	7804	7480 7976	40
20	9.407419							20	9.438059	8141	8224	8306	8389	8471	39
21	7945	8033	8121	8208	8296	8384	38	21	8554	8636	8719	8801	8884	8966	38
22				8734				22	9048						
23				9259 9783				23	9543 9.440036	9023	9707	0283	0365	04/17	35
	9.410045							25						0940	
26				0831				26	1022	1104	1186	1268	1350	1432	33
27				1353				27						1924	
28 29				1876 2397				28 29	2000	2570	2661	2232	2825	2416 2907	30
	9.412658								9.442988						
31	3179	3266	3352	3439	3526	3613	28	31	3479	356o	3642	3724	3805	3887	28
32	3699	3786	3873	3959	4046	4132	27	32						4376	
33 34	4219 4 2 38	4805	4392	4479 4998	4565	4652	20	33 34	4458	4539	5110	4702	5272	4865 5354	25
35				5516				35						5842	
36				6034				36	5923	6005	6086	6167	6248	633o	23
37	6293	6379	6465	6551	6638	6724	22	37						6817	
38	7326	7/13	7/00	7068 7585	7134	7240	21	38 39	9384 9384	0979 7465	7000	7141	7222	73o3 7789	21
	9.417842	7928	8014	8100	8186	8272	10	40	9.447870	7951	8032	8113	8194	8275	10
41	\$358	8444	853o	8616	8701	8787	18	41	8356	8437	8518	8599	868o	8760	18
42				9130				42	8841	8922	9003	9084	9164	9245	17
43		9473	9009	9644 . 158	9730	9810	15	43 44	9320	9407	9487	951.5	9049	9730	15
	9.420415	0500	0586	0671	0757	0842	14	45	9.450294	0375	0455	0536	0610	0697	14
46	. 0927	1013	1098	1184	1269	1354	13	46	0777	0858	0938	1019	1099	1180	13
47				1696				47						1662	
48		25/8	2633	2207 2718	2292	2378	II	48	1743	2305	2385	2/65	25/6	2144 2626	10
	9.422974	3059	3144	3229	3314	3399	9	50	9.452706						
51	3484	3569	3654	3739	3824	3909	8	51	3187	3267	3347	3428	3508	3588	8
52	3993	4078	4163	4248	4333	4418	7	52						4068	
53	4003 5077	5006	4072 5181	4757 5265	5350	4927	6 5	53	4148	4228	4508	4388	4408	4548 5027	6 5
55	5519	5604	5689	5773	5858	5042	4	55	5107	5187	5267	5346	5426	5506	4
56	6027	6112	6196	6281	6365	6450	3	56	5586	5655	5745	5825	5905	5984	3
57	6534	6619	6703	6788	6872	6956	2	57						6462	
58	7041	7125	7210	7294 7800	7378	7463	I	58						6940	
1-09	60"	50"	40"	30"	20"	10"		59	60"	50"	40"	30"	20"	10"	-
1		1		75 D	<u>'</u>	-	Min.		Co-ta			. I	٠		M.n.
1		2" 3			3" 7"		9"	-	(1//				6" 7'		9.
1'.	Pa * \{ \frac{1''}{9}	17 20	_		52 61	-	78	P.	Part / -	16 2		-	49 57	-	74
-								и							

1			ina c	f 16	Dogra					Q:	ina of	177	Doome			-
1 2	1	0"	10"	of 16	30"	40"	50"		Min	0"	10"	20"	Degre 30"	es.	50"	
-	0	9.440338						50		9.465935						50
	1			2 0925					I	6348	6417	6486	6555	6623	6602	58
	2	1218	129	2 1365	1438	1511	1584	57	2	6761	683o	6898	6967	7036	7104	57
	3			1804					3	7173	7242	7310	7379	7448	7516	56
	4 5			2243					4	7585	7653	7722	7790	7859	7928	55
	6			8 2681 6 3119					5	7990 8407	8/45	8544	8670	868	8338 8749	54
	7			3556					7	8817	8886	805/	0012	0001	9159	52
	8	3847	392	3993	4066	4138	4211	5 I	8	9227	9296	9364	0432	0500	9569	51
	9	4284	435	6 4429	4502	4574	4647	5o	9	9637	9705	9773	9842	9910	9978	50
1	o	9 . 444720							10	9.470046	0114	0182	0251	0319	0357	49
,	I			3 5300					11						0795	
	3			3 5735 7 6170		(·		12						1203	
1	4			6604					13						1611 2018	
	5			7037					15						2424	
4	6			3 7470					16						2831	
I	7	7759	783	1 7903	7975	8047	8119	42	17	2898	2966	3034	3101	3160	3237	42
I	8			8335					18	3304	3372	3439	3507	3575	3642	41
I	9	8623	869	8767	8838	8910	8982	40	19						4047	
	0	9.449054	912	9198 79628	9209	9341	9413	39		9.474115	4182	4250	4317	4384	4452 4856	39
1	2	0015	008	7 59	. 13o	202	27/	37	2 I 2 2	4023	4001	5058	5125	5103	5260	37
	- 1	9.450345							23						5663	
ı	4			0918					24	5730	5798	5865	5932	5999	6066	35
2	5			5 1347					25	6133	6200	6268	6335	6402	6469	34
1	6			4 1775					26						6871	
	7			2203					27	6938	7005	7072	7139	7206	7273	32
1	8			9 2630 6 3057					28	7340	7407	7473	7340	8008	7674 8075	30
	9	9.453342								9.478142						
	I	3768	383	3910	3981	4052	4123	28	31	8542	8609	8676	8742	8800	8876	28
3	2			5¦4336					32						9275	
1	3			4761					33						9675	
	4			5 5 1 8 6					34						74	
	5			5610 3 6034					36	9.480140					0472	
	7			6457					37						1268	
	8	6739	681	6880	6951	7021	7001	21	38						1665	
	9	7162	723	2 7303	7373	7443	7514	20	39	1731	1798	1864	1930	1996	2062	20
4	o	9.457584								9.482128						
	I			8146					41						2855	
	3			7 8567 8 8988					42						3251 3646	
	4	0268	033	3 9408	0478	0548	0618	15	44	3712	3778	3843	3000	3075	4041	15
	5			9828					45	4107	4172	4238	4304	4370	4435	14
		9.460108	017	8 0248	0317	0387	0457	13	46	4501	4567	4632	4698	4764	4829	13
	7			0667					47	4895	4961	5026	5092	5158	5223	12
	8			1085					48	5289	5-10	58-2	58-0	5044	5617	II
	9			1503					49	9.486075					6/02	
	ı	9.461782	226	2338	2/07	2/177	25/16	8	51	6467	6533	6508	6664	6720	6794	8
	2	2616	268	5 2755	2824	2804	2963	7	52	6860	6925	6990	7055	7121	7186	7
5	3	3032	310	2 3171	3240	3310	3379	6	53	7251	7316	7382	7447	7512	7577	6
	4	3448	351	8 3587	3656	3725	3795	5	54	7643	7708	7773	7838	7903	7968	
	5			3 4002				4	55				8229			3
	6			8 4417 3 4832				3	56	881/	8870	8044	9009	0004	8749	2
	8	5±08	517	7 5246	5315	538/	5453	I	58	020/	0260	033/	9300	9464	9528	1
	9			5660				o	59	9593	9658	9723	9788	9853	9918	0
-	<u> </u>	60%	50"	40"	30"		10"	\vdash	ŕ	60"	50"	40"	30"	20"	10"	
		Co-	sine	of 73	Deg	rees.		Min.		Co-	sine	of 72	Deg	rees.		Min.
1		Part § 1"	2 / 3	4"	5" 6	7"	8"	9"	n	Post § 1"	2" 3'	4"	5" (5" 7 "	8"	9"
1	۲.	Part 7	14 9	21 28	36 4	13 50		64	r.		13 20	27	33 4	0 47	53	60

	Tan	cont	of 16	5 Deg	raag				Tar	cent	of 17	7 Dec	rrees		Г
Min.	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	
o	9.457496							0	9.485339						
2				8211				1 2						6167 6618	
3				9163				3						7068	
4	9400	9479	9558	9638	9717	9796	55	4	7143	7218	7293	7368	7443	7518	55
5				.112				5	7593 8043	7668	7743	7818	7893 8373	7968 8418	53
7	9.460349 0823	0002	0081	1060	1130	1218	52	7	8492	8567	8642	8717	8792	8866	52
8	1297	1376	1454	1533	1612	1691	51	8	8941	9016	9091	9166	9240	9315	51
9	1770 9.462242	1849	1927	2006	2085	2164	50	9	9390	9465	9539	9614	9689	9763	50
11				2950					9.489838 9.490286						
12	3186	3265	3343	3422	35oi	3579	47	12						1106	
13				3893				13	1180	1255	1329	1404	1478	1552	46
14				4364 4834				14						1999 2445	
16	5060	5147	5226	5304	5382	546o	43	16						2890	
17	5539	5617	5695	5773	5851	5930	42	17	2965	3039	3113	3187	3261	3336	42
18				6242				18						3780	
20	9.466945			6711				20	3834 9.494299					4225 4669	
21	7413	7491	7569	7647	7724	7802	38	21	4743	4817	4891	4965	5039	5113	38
22	7880	7958	8036	8114	8192	8269	37	22						5556	
23				8581 9047				23 24	5030 6073	5704 61/6	6220	6204	0920 6368	5999 6441	36 35
25				9513				25						6884	
26	9746	9823	9901	9979	56	. 134	53	26	6957	703í	7105	7178	7252	7326	33
	9.470211							27	7399	7473	7546	7620	7693	7767	32
28				0909 1373				28 29						8208 8649	
	9.471605								9.498722						
31				2300				31						9529	
32 33	2032	3072	31/0	2763 3226	2840 3303	2918 3380	27	32	9603 9.500042					9969	
34	3457	3534	3611	3688	3765	3842	25	34						0847	
35	3919	3996	4073	4150	4227	4304	24	35	0920	0993	1066	1140	1213	1286	24
36 37	4381	4458	4535	4612 5073	4688	4765	23	36	1359	1432	1505	1578	1651	1724 2162	23
38				5533				37 38						2599	
39	5763	584o	5917	5993	6070	6147	20	39						3036	
	9.476223	6300	6377	6453	653o	6606	19	1 : 1	9.503109						
41	71/2	7210	7205	6913 7372	0989 7448	7524	18	41						3910 4346	
43				7830				43						4781	
44				8288				44	4854	4926	4999	5072	5144	5217	15
45 46				8746 9203				45 46	5289 5724	5706	5860	50/1	5579 601/	5652 6086	14
47	9432	9508	9584	9660	9237	9813	12	47						6520	
48	9889	9965	41	.117	.193	.269	II	48	6593	6665	6737	6810	6882	6954	11
49	9.480345	0421	0497	0573	0649	0725	10	49	7027	7099	7171	7243	7316	7388	10
5 I	9.480801	1333	1408	1484	1560	1636	8	51	9.507460 7803	7065	7003 8038	7077	7749 8182	7521 8254	8
52	1712	1788	1863	1939	2015	2091	7	52	8326	8308	8470	8542	8614	8687	7
5 3	2167	2242	2318	2394	2470	2545	6	53	8759	883 ı	8903	8975	9047	9119	6
54 55	3075	2097 3151	3226	2848 3302	2924 3355	2999 3/53	5 4	54 55	9191	9263	9335	9407	9479	9551 9982	5 4
56	3520	3604	368o	3755	3831	3906	3		9022 9.510054	0126	9700	0260	0341	0413	3
57	3982	4057	4133	4208	4284	4359	2	57	0485	0557	0629	0700	0772	0844	2
58	4435						1	58	0916	0987	1059	1131	1203	1274	1
59	4887	4902 50"	40"	30"	20"	10"	0	59	1346	50"	1489	30"	20"	1704	0
+	Co-ta						Min.		Co-ta						Min.
		2" 3'			7''		9"			2" 3"			3" 7"		9"
				_ 0	•	-			Font / "		-				-

			110					17.		SINI						
Min.	0"	ne of	20"	Degre	es.	50"		Min.	L	<u>0''</u>	ne of	19]	Jegre 30"	es.	5011	
0	9.489982				-		59	0	9	512642	2703	2764	2825	2886	2048	50
I	9.490371							1		3009	3070	3131	3192	3253	3314	58
3				0953 1341				3	1	3375	3800	3497	3558	3619 3985	3680	57
4	1535	1599	1664	1728	1793	1857	55	4	1	4107	4168	4229	4289	4350	4411	55
5	1922	1986	2051	2115	2179	2244	54	5	,	4472	4533	4594	4655	4715	4776	54
6				2502 2888				6	!	4837	4898	4959	5019	5080 5445	5141	53
8				3273				8		5566	5627	5687	5748	5809	586a	5r
9	3466	353o	3595	3659	3723	3787	50	9		5930	5991	6051	6112	6172	6233	50
1 1	9.493851							10		516294	6354	6415	6475	6536	6596	49
11	4230	4685	4740	4428 4813	4492	4041	40	11		7020	7080	71/1	7201	6899 7262	7322	48
13	5005	5069	5133	5196	5260	5324	46	13	1	7382	7443	7503	7564	7624	7684	46
14	5388	5452	5516	558o	5644	5708	45	14		7745	7805	7865	7926	7986	8046	45
15	5772 6154	5835	5899	5963 6346	6410	6473	44	15 16	1	8/68	8508	8580	8640	8348 8709	8408	44
17				6728				17	1	8829	8890	8050	9010	9070	0130	43
18	6919	6983	7047	7110	7174	7237	41	18		9190	9250	9311	9371	9431	9491	41
19	7301	7365	7428	7492	7555	7619	40	19	1	9551	9611	9671	9731	9791	9851	40
20	9.497682 8064			7073 8254						519911						
22				8634				22	3.					0870		
23	8825	8888	8951	9015	9078	9141	36	23	l	0990	1050	1110	1169	1229	1289	36
24	9204	9268	9331	9394	9458	9521	35	24						1588		
26	0063	26	00	9774 .153	,216	.270	33	25 26	•					1946 2304		
	9.500342							27						2662		
28				0910				28						3019		
30	1099	1530	1602	1288	1331	1414	30	30		523495	3555	361/	3317	3376	3436	30
31				2042				31	9.	3852	3911	3971	4030	4089	4149	28
32	2231	2294	2356	2419	2482	2545	27	32		4208	4267	4327	4386	4445	4505	27
33				2796				33		4564	4623	4683	4742	4801	4860	26
35				3172 3548				34		4920 5275						
36				3923				36						5866		
37	4110	4173	4235	4298	436o	4423	22	37						6221		
38	4485 4860	4548	4610	4673 5047	4735	4797	21	38		6339 6693	6398	6457	6850	6575	6634	21
	9.505234	5206	5350	5421	5483	5545	10		٥.	527046						
41				5794				41	_	7400	7459	7517	7576	7635	7694	18
42				6168				42		7753	7811	7870	7929	7988	8047	17
43	6727	6780	685 t	6541	6075	7037	10	43 44		8105 8458						
45	7099							45		8810						
46	7471	7533	7595	7657	7719	7781	13	46		9161	9220	9279	9337	9396	9454	13
47	7843	7905	7967	8028	8090	8152	12	47		9513	9571	9630	9688	9747	9805	12
48	8214 8585	86/17	0338 8700	8770	0401 8830	880/	11	48	0 -	9864 530215	9922	0331	0300	04/8	0507	10
	9.508956	9017	9079	9141	9202	9264	9			530565	0623	0682	0740	0798	0857	9
51	9326	9387	9449	9511	9572	9634	8	51		0915	0973	1032	1090	1148	1207	8
52	9696	9757	9819	9880	9942	4	7	52 53		1265 1614						7 6
54	9.510065 0434						6 5	54		1963						5
55	o8o3	o865	0926	0987	1049	1110	4	55		2312	2370	2428	2487	2545	2603	4
56	1172	1233	1294	1356	1417	1478	3	56		2661	2719	2777	2835	2893	2951	3
57	1540						2	57		3009						2
59	1907 2275						I O	58 59		335 ₇ 3 ₇₀ 4						1 0
	60"	50"	40"	30"	20"	10"		- 7		60"	50"	40"	30"	20"	10"	-
	Co-s	sine o	f 71	Degr	ees.		Min.			Co-s	sine c	f 70	Degr	ees.		Min.
P. 1	Part /	2" 3"		_	" 7"		9"	Р.	Par		2" 3"			7"		9"
	6 1	13 19	25	31 3	8 44	50 5	57	- • •	_ 14		12 18	24	30 3	6 42	48	54

				LOG			, -	. د	LANGE	11 1 1	•				4
Min		gent						Min.		gent					
- 2	0"	10"	20"	30"	40"	50"	_		0"	10"	20"	30"	40"	50**	_
0	9.511776							1	9.536972	7040	7109	7177	7245	7314	59
1 2		2277 2707						1 2	7702	7450 7860	7020	7007	8065	8133	57
3		3136						3		8270					
4	3493	3564	3636	3707	3778	385o	55	4		8679					
5		3992						5	9020	9088	9156	9224	9293	9361	54
6		4420 4848						6		9497 9905					
8	5204	5275	5346	5417	5489	5560	51	8	9.540245						
9	5631	5702	5773	5844	5915	5986	5о	9		0721					
10	9.516057	6129	6200	6271	6342	6413	49	11 1	9.541061	1					
11	6484	6555	0020	6697	6768	6839	48	II		1536					
13	7335	6981 7406	7652	7548	7610	7600	47	12	2281	1943 2349	2417	2485	2552	2620	47
14	7761	7831	7902	7973	8044	8115	45	14		2755					
15	8186	8256	8327	8398	8469	8539	44	15	3094	3161	3229	3297	3364	3432	44
16		8681						16		3567					
17 18	9034	9105	9170	9240	9317	9388	42	17	3905	3972 4377	4040	45107	4170	4242	42
19	0882	9529 9953	23	9070	.164	.235	40	19	4310	4782	4850	4017	4085	5052	40
	9.520305							20	9.545119	5187	5254	5322	5389	5456	39
21	0728	0799	0869	0939	1010	1080	38	21	5524	5591	5658	5726	5793	586o	38
22		1221						22	5928	5995	6062	6129	6197	6264	37
23 24		1643 2065						23	6731	6398 6802	6860	6036	0000	0007	35
25		2487						24		7205					
26		2908						26	7540	7608	7675	7742	7809	7876	33
27	3259	3329	3399	3469	3539	3609	32	27	7943	8010	8077	8144	8211	8278	32
28		3750						28	8345	8412	8479	8546	8613	8680	31
29	4100 9. 52 4520	4170						29		8814					
31	4040	5009	5070	51/0	5210	5280	28	31	9.549149	9617	0684	0751	0817	088/	28
32		5429						32	9951	18	85	.152	.218	.285	27
33	5778	5848	5918	5987	6057	6127	26		9.550352						
34	6197	6266	6336	6406	6476	6545	25	34		0819					
35 36	7033	6685 7103	7734	72/2	7312	7381	24	35 36		1619					
37	7451	7520	7500	7660	7729	7700	22	37		2019					
38	7868	7938	8007	8077	8146	8216	21	38	2351	2418	2484	2551	2617	2684	21
39	8285	8355	8424	8494	8563	8633	20	39		2817					
	9.528702	8772	8841	8910	8980	9049	19	11 .	9.553149						
41	0535	9188 9604	9237	9327	0812	0881	10	41 42		3614 4012					
43	9951	20	89	.158	.228	.207	16	43		4410					
44	9.536366	0435	0504	0574	o643	0712	15	44		4808					
45	0781	0850	0920	0989	1058	1127	14	45		5205					
46		1265						46		5602					
47 48		1680 2094						47 48		5999 6395					
49		2508						49	6725	6791	6857	6923	6989	7055	10
50	9.532853	2921	2990	3059	3128	3197	9	50	9.557121	7187	7253	7319	7385	7451	9
51	3266	3335	3404	3472	3541	3610	8	51	7517	7583	7649	7715	7781	7847	8
5 ₂ 53	3079	3748 4160	3816	3885	13954	4023	7	52 53	7913	7978	8/30	8505	85-	863-	7
54	4504	4573	4641	4290	4770	4433	5	54	8703	8768	883/	8000	8066	0037	5
55	4916	4985	5053	5122	5191	5250	4	55	9097	9163	9229	9294	9360	9426	4
56	5328	5396	5465	5534	5602	5671	3	56	9491	9557	9623	9688	9754	9820	3
57		5808						57	9885	9951	17	82	. 148	.214	2
58 59		6630	1	1	1 - 1 - 1		1		9.560270						
L-39	60"	663o	40"	30"	20"	10"		59	60"	50"	40"	30"	20"	1000	-
		ingen			<u>'</u>		Min			inger			1		Min.
-	4 4 4 4	2" 3'			3" 7"		9"	-	·		" 4"		6" 7'		9"
P.	Part	14 21	_		12 49	_	63	P.	Part $\begin{cases} 1'' \\ 7 \end{cases}$	13 2			40 47		60
L								11							

Min.				Degre				Min.			ine of	21]	Degre	ees.		
Ξ	0"	10"	20"	30"	40"	50"				D''	10"	20"	30"	40"	50"	1
0	9.534052	4110	4167	4225	4283	4341	50	0	9.55	4320	4384	4430	4404	4540	4603	50
7				4572				1	1	4658	4713	1768	1822	1877	1032	158
2	1015	1803	186-	4918	1076	503/	5.7	2		1087	5042	5006	5.5-	5206	5060	5
3	5000	5 - 40	5007	5065	5300	5380	56	3								
1	5092	5149	5207	5265	5660	56	50			5619	5370	5425	3479	500	5509	130
4				5610				4		2043	5698	2723	3007	2002	3916	153
5				5956				5		5971	6026	6080	6135	6190	6244	5
6	6129	6186	6244	63o1	6359	6416	53	6		6299	6353	6408	6462	6517	6571	5:
7	6474	653ı	6580	6646	6704	6761	52	7			668o					
8				6991				8			7007					
- 1	7163	7070	7078	7335	7300	7/50	50	1 1								
9	7105	7220	12/0	7333	7592	7430	10	9		7200	7334	7300	7443	7497	7552	13
	9.537507	7304	7022	7079	7730	7794	49		9.50		7660					
1				8023				11		7932	7986	8041	8095	8149	8204	4
2	8194	8252	8309	8366	8423	848o	47	12		8258	8312	8366	8421	8475	8529	4
3	8538	8505	8652	8709	8766	8823	46	13		8583	8638	8602	8746	8800	8855	4
4				9052				14			8963					
5	0003	0080	0334	0306	0/51	0508	1.1	1 - 1		0934	9288	93/9	9376	0/50	2504	17
	9223	9200	9557	9394	9431	9300	44	15		9234	9200	9342	9390	9450	9304	14
6	9505	9022	9079	9730	9793	9000	43	16		9000	9613	9007	9721	9779	19029	14
7	9907	9964	21	9736 ••78	.135	.192	42	17		9883	9937	9991	45	99	1.153	4
8	9.540249	0306	o363	0420	0477	0533	4 1	18	9.56	0207	0261	0315	0369	0423	0477	4
9				0761				19		o531	o585	0639	0693	0747	0801	4
	9.540931							20	0.56	io855	0908	0062	1016	1070	112/	3
1				1442				21	,	1178	1232	1286	1330	1303	1/1/1	3
- 1								1 1		150-	1555	1600	1660	1093	1.447	2
22				1783				22								
:3				2123				23			1878					
:4	2293	2349	2406	2462	2519	2576	35	24			2200					
5	2632	2689	2745	2802	2858	2915	34	25		2468	2522	2576	2629	2683	2737	3.
6				3141				26			2844					
27	3310	3367	3/23	348o	3536	3503	32	27			3166					
	3640	3705	3-60	3818	38-5	3037	3				3487					
8								28	_							
29	3987	4044	4100	4156	4213	4209	30	29	٠.		3808					
30	9 544325	4382	4438	4494	4550	4607	29	30	9.56		4129					
31	4663	4719	4776	4832	4888	4944	28	31		4396	4449	45o3	4556	4610	4663	2
32	5000	5057	5113	5169	5225	5281	27	32		4716	4770	4823	4876	4030	4083	2
33	5338	530/	5/50	55o6	5562	5618	26	33		5636	5090	51/13	5106	5250	5303	2
34	56=4	5731	5080	5843	5800	5055	25	34			5409					
	5074	6-6-	6707	6	6-25	6933	20				5729					
35				6179				35								
36				6515				36			6048					
37	6683	6739	6795	6851	6907	6963	22	37			6367					
88	7019	7075	7131	7187	7242	7298	21	38		6632	6685	6739	6792	6845	6898	2
39	7354	7410	7466	7522	7578	7633	20	39			7004					
	9.547689								0.56		7322					
i				8191				41	,		764o					
								1 : 1		100/	7957	2040	8062	1779	8160	1
12				8526				42								
3				8860				43		0222	8275	0327	0300	0433	0400	11
14	9027	9082	9138	9193	9249	9305	15	44		8539	8592	8644	8097	8750	8803	I
15	9360	9416	9471	9527	9582	9638	14	45		8856	8908	8961	9014	9067	9119	I.
6	9693	9740	9805	9860	9916	9971	13	46		9172	9225	9277	9330	9383	9436	1
	9.550026	0082	0137	0103	0248	0304	12	47		0488	9541	0504	0646	0600	9752	1
8	0350	0/15	0/170	0525	0581	0636	111	48		080/	9857	0010	0062	1. 15	. 67	I
	0600	07/-	0800	0858	0012	0068	1	100	0 5-	7007	0173	0225	0278	0330	0383	T
19								49	9.57	0120	0488	051-	0500	06 16	0600	
	9.551024								9.57	/0433	-0-0	-050	0093	0040	0090	1
1	1356	1411	1466	1521	1277	1032	8	51			0803					
2	1687	1742	1798	1853	1908	1963	7	52			1118					
53	2018	2074	2120	2184	2235	2294	6	53			1433					
54				2515			5	54		1605	1747	1790	1852	1904	1956	
55				2845			4	55			2061					1
56	2000	3065	3790	3176	303-	3086		56			2375					
	3010	3000	312I	3176	050	26-1				2020	20/0	2427	479	0015	0805	
27				3506			2	57			2688					
58	3670	3725	3780	3835	3890	3945	1	58			3002					
.9	4000	4055	4110	4165	4210	4274	0	59		3263	3315	3367	3419	3471	3523	1
-	60"	50"	40"	30"	20"	10"	-	<u> </u>	- 6	3011	50"	40"	30"	20"	10"	-
				Degr			Min.	1	`		sine					Š
																<u>_</u>
D	Part /	2" 3"			" 7"		9"	TO	Part	, -	2" 3"	_	-		-	9'
	Part 6	11 17	23	28 3	4 39	45	51	; I.	1 all	5 5	11 16	3 21	27 3	2 37	43	48

Min	Tan	gent	of 20) Deg	rees.			Min.		gent	of 2	1 Deg	grees.		Γ
Z	0"	10"	20"	30"	40"	50"		M	0"	10"	20"	30"	40"	500	
0	9.561066	1131	1197	1262	1328	1393	59	0	9.584177	4240	4303	4366	4429	4492	59
1	1459	1524	1590	1655	1721	1786	58	I	4555	4618	4681	4744	4806	4869	58
2	1851	1917	1982	2048	2113	2178	57	2						5246	
3	2244	2309	2375	2440	2505	2571	56	3	5309	5372	5435	5498	5500	5623	50
4	2636	2701	2767	2832	2897	2963	50	4						6000	
5				3224				5						6376	
6				3615				6						6752	
7				4006				7						7128	
8				4397				8	7190	7200	7510	7370	7441	7503 7879	5
9	4393 9.564983			4788				9	7566 9.587941						
I				5568				1 1						8629	
2				5958				11						9003	
3				6348				13	0091	0754	0101	0253	0375	9378	14
4				6737				14	0//0	0502	0565	0627	0600	9752	1
5				7126				15	081/	0877	0030	9027	63	.126	1
6				7515					9.590188	0250	0313	0375	0/37	0/100	43
7	7700	777/	7830	7903	7068	8033	12	17						0873	
8	8008	8162	8227	8292	8356	8/121	41	18	0035	0007	1060	1122	1184	1246	4
9				8680				19						1619	
	9.568873	8938	9003	9067	9132	9197	39		9.591681						
1	0261	0326	9390	9455	9519	0584	38	21	2054	2116	2178	2240	2302	2364	38
2	6648	9713	9777	9842	9906	9971	37	22						2737	
	9.570035	0100	0164	0220	0203	o358	36	23						3109	
:4	0422	0487	o551	0616	o68o	0744	3.5	24						3480	
5				1002				25						3852	
6	1195	1250	1324	1388	1452	1517	33	26						4223	
27				1774				27	4285	4347	4409	4471	4532	4594	3:
8				2160				28	4656	4718	4780	4842	4903	4965	3
29	2352	2417	2481	2545	2609	2673	3о	29	5027	5089	5150	5212	5274	5336	3
30	9.572738	2802	2866	2930	2994	3059	29	30	9.595398						
31				3315				31						6076	
32				3700				32						6446	
33				4084				33	6508	6570	6631	6693	6754	6816	21
34				4468				34						7185	
35				4852				35						7555	
36				5236				36						7924	
37				5619				37	7985	8047	8108	8170	8231	8293	2
38				6002				38	8354	8415	8477	8538	8600	8661	2
39	6193	0257	6321	6385	6449	0512	20	39	8722	8784	8845	8907	8968	9029	20
	9.576576								9.599091	9152	9213	9275	9336	9398	I
I				7150				41	9459	9520	9281	9643	9704	9765	I
12				7532				42						.133	
13	7723	7700	7000	7914	7977	0041	10		9.600194						
14 15				8295 8676				44						0868	
16								45 46						1235 1601	
17	0007	0317	5375	9057 9438	0500	0565	10	47						1968	
18	0620	9911	0755	9819	0880	9000	17	47 48						2334	
٠,	9.580009	3092	9736	9019	0260	0326	10	49						2700	
3	9.580389	0/153	0516	0570	06/10	0706	0	149	9.602761	2800	2883	2014	3005	3066	- 1
ί	0760	0830	0806	0959	1022	1086	8	51	3127	3188	32/10	3310	3371	3432	
52				1339				52	3/03	3554	3615	3675	3736	3797	1
3				1718				53						4162	
54				2097				54						4527	
55	2286	2350	2413	2476	2530	2602		55						4892	
56	2665	2728	2701	2854	2017	2080	3	56	∠ 053	501/	507/	5135	5106	5257	
57				3233				57	5317	5378	5430	5500	5560	5621	
8	3422	3485	3548	3611	3674	3737	I	58						5985	
59	3800	3863	3026	3989	4052	4114		59						6349	
-1	60"	50"	40"	30"	20"	10"		-	60"	50"	40"	30"	20"	10"	-
	Co-ta					l	Min.		Co-ta				1		1
							9"	_							J
D	$Part \begin{cases} 1'' \\ 6 \end{cases}$	2'' - 3'	4"	5" 6	5" 7"	8"	9.,	p	Part \ 1"	z 3	" 4"	5"	6" 7"	′ 8″	9'

_								11							
Min.				Degre]	Min.				Degre			
	0"	10"	20"	30"	40"	50"	_		0"	10"	20"	30"	40"	50"	
0	9.573575					4148		0		1928	1977	2027	2076 2374	2126	59
2						4460		2	2473	2522	2572	2621	2671	2720	57
3						4772		3	2770	2819	2869	2918	2068	3017	56
4						5084		4	3067	3116	3165	3215	3264	3314	55
5						5395		5	3363	3412	3462	3511	3561	3610	54
6						5706 6017		6	3059	3709	3758	3807	3857	3906	53
8						6327		7 8	4251	430t	4350	//300	4153 4448	4408	5 T
9						6638		9	4547	4506	4645	4605	4744	4703	50
	9.576689	6741	6793	6844	6896	6948	49	10	9.594842	4891	4941	4990	5039	5088	49
11	6999	7051	7102	7154	7206	7257	48	11	5137	5186	5236	5285	5334	5383	48
12	7309	7360	7412	7464	7515	7567	47	12	5432	5481	5530	5580	5629	5678	47
13	7010	7070	7721 8030	8082	7024	7876 8185	45	13 14	6027	6070	5825	574	5923 6217	5972	46
15	8236	7979 8288	8330	8301	8/1/2	8494	43	15	6315	6364	6/13	6/62	6511	6560	43
16	8545							16	6600	6658	6707	6756	6805	6854	43
1.7	8853	8905	8956	9008	9059	9110	42	17	6903	6952	7001	7050	7099	7148	42
18	9162	9213	9264	9316	9367	9418	41	18	7196	7245	7294	7343	7392	7441	41
19	9470	9521	9572	9023	9075	9726	40	19	7490	7539	7587	7636	7685	7734	40
20	9.579777 9.580085	9020	9000	9931	9902	03/1	38	21	9.597783	7001 810/	7000	7929	7978 8270	837	39
22	0392							22					8563		
23	0699	0750	0801	0852	0903	0954	36	23					8855		
24	1005	1056	1107	1158	1209	1261	35	24	8952	9001	9050	9098	9147	9195	35
25						1567		25	9244	9293	9341	9390	9438	9487	34
26						1873		26	95 3 6	9584	9633	9681	9730	9778	33
27	2220					2178		27	9827 9.600118						
29	2535							20					0603		
	9.582840							30	9.600700						
31	3145	3195	3246	3297	3348	3398	28	31	0990	1038	1087	1135	1184	1232	28
32	3449	3500	3551	3601	3652	3703	27	32					1474		
33	3754							33					1763		
34	4058 4361							34 35	1860 2150						
36	4665							36					2632		
37	4968							37					2920		
38	5272	5322	5373	5423	5474	5524	21	38	3017						
39	5574	5625	5675	5726	5776	5827	20	39					3497		
	9.585877								9.603594				4074		
41 42	6179 6482							41 42	4170						
43	6783							43	4457						
44	7085	7135	7186	7236	7286	7336	15	44	4745	4793	4841	4888	4936	4984	15
45	7386	7437	7487	7537	7587	7637	14	45					5223		
46	7688							46	5319						
47 48	79 ⁸ 9 8 2 89							47 48	5606 5892						
49	8590	8640	86aa	8740	8700	8840	10	49	6179						
50	9.588890	8940	8990	9040	9090	9140	9	50	9.606465	6512	656o	6608	6655	6703	9
51	9190	9240	9290	9340	9389	9439	8	51	6751	6798	6846	6893	6941	6989	8
52	9489	9539	9589	9639	9689	9739	7	52	7036	7084	7131	7179	7227	7274	7
53	9789	9839	9889	9938	9988	38	6 5	53 54	7322	7309	7417	7404	7012	7339	6 5
55	9.590088 0387						4	55	7607 7892	7034	7087	7749 803/	7797 8082	8120	4
56	0686						3	56	8177	8224	8271	8310	8366	8414	3
57	0984						2	57	8461	8508	8556	86o3	8651	8698	
58	1282	1332	1382	1431	1481	1531	1	58	8745	8793	8840	8887	8935	8982	1
59	1580						0	59	9029						0
	60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
				Degr			- 1					Degr		0''	
P. 1	Part / - "	2″ 3″ 10 15	_	5" 6 25 3	7" 7" 1 36		9" 46	Ρ.	Port / "	2" 3" 10 15		-	3" 7" 29 34	-	9" 44
·		. 0 10	· ~0	~ 0		JI ,	10		() ,		1.7	~			

			-£ 00	D			1 1		_	Ton		of 92	Doo			
Min.	0"	gent	OI 22	Deg	rees.	50"		Min	L	0"	10"	of 23	30"	40"	50"	
0	9.606410						50	0	0	627852						50
1		6834						1	1	8203	8262	8320	8379	8437	8496	58
2	7137	7197	7258	7318	7379	7439	57	2		8554	8612	8671	8729	8788	8846	57
3	7500	7560	7621	7681	7742	7802	56	3		8905	8963	9022	9080	9138	9197	55
4 5	7003 8225	7923 8286	7904 83/6	8/07	8/67	8528	5/1	5		0606	0664	9372	0781	0830	9547 9897	54
6	8588	8648	8709	8769	8830	8890	53	6		9956	14	73	.131	.189	.247	53
7	8950	9011	9071	9131	9192	9252	52		9.	636366						
8	9312	9373	9433	9493	9554	9614	51	8							0947	
9	9.610036	9735	9795	9000	9913	0337	30	9	_	631355					16/6	
11		0458						11	9	1704	1762	1820	1878	1936	1995	48
12		0819						12		2053	2111	2169	2227	2285	2343	47
13	1120	1180	1240	1300	1360	1420	46	13							2692	
14 15		1540 1901						14		2700 3000	3157	3215	3273	2902 3331	3040 3389	45
16		2261						16							3737	
17	2561	2621	2681	2741	2801	2861	42	17		3795	385 3	3911	3969	4027	4085	42
18		2981						18							4432	
19	3281 9.613641	3341						19		4490 634838 .					4780 5127	
21		4060						21	9						5474	
22		4419						22		5532	5590	5648	5706	5763	5821	37
23	4718	4778	4838	4897	4957	5017	36	23							6168	
24 25	5077	5136 5495	5555	5256	5316	5375	35	24		65=0	6630	6688	6399	6863	6514 6861	35
26	5703	5853	5013	5072	6032	6002	33	25 26							7207	
27	6151	6211	6271	633o	6390	6450	32	27							7553	
28	6509	6569	6628	6688	6748	6807	31	28		7611	7668	7726	7783	7841	7899	3 1
29	6867	6926	6986	7046	7105	7165	30	29							8244	
3o 31		7641	7343	7760	7820	7322	29	31	9	.638302 8647					8935	
.32		7998						32		8992	9050	9107	9165	9222	9280	27
33		8355						33		9337	9395	9452	9510	9567	9625	26
34		8711						34							9969	
35 36	036/	9068 9424	0/83	05/3	0602	0661	24	36		.640027 .0371					0658	
37	9720	9780	9839	9898	9958	17	22	37							1002	
	9.020070	0136	0195	0254	0313	0373	21	38							1346	
39		0491						39							1690	
40	9.620787	1201						40		.641747	21/8	2205	2263	2320	2377	18
42		1556						42	1						2720	
43	1852	1911	1970	2029	2088	2147	16	43		2777	2834	2892	2949	3006	3063	16
44		2266						44							3406	
45 46		2620 2974						45 46							3749 4091	
47	3269	3328	3387	3446	3505	3564	12	47		4148	4205	4262	4319	4376	4433	12
48	3623	3682	3741	38oc	3858	3917	11	48		4490	4547	4604	4661	4718	4775	II
49	3976	4035	4094	4153	4212	4271		49		4832	4889	4946	5003	5060	5117	}
51	9.62433c	4388	4447	4850	4005	4024	8	50 51		.645174	5573	15288 15630	568	57/1/	5801	8
52	5036	5094	5153	5212	5271	5330		52	ı	5857	5914	5971	6028	6085	6142	7
53	5388	5447	5506	5565	5623	5682	6	53		6199	6256	6313	6369	6426	6483	6
54	5741	5800	5858	5917	5976	6035	5	54							6824	
55		6152 6504						55		0881	10938	7335	7303	7108	7165	3
57	6707	6856						57	1	7562	7610	7676	7733	7780	7846	2
58	7149	7208	7266	7325	7383	7442	1	58		7903	7960	8016	8073	8130	8186	I
59		7559					0	59	_						8526	0
	60"	50"	40"	30"	20"	10"	Min.		L	60"	50"		30"	20"	10"	Min.
	1	angen 2" 3			egree		9"		L			it of		egree		9"
Ρ.	Part 6	12 1	_	_	36 42	_	54	Ρ.	. P	art \ 6	12 1		-	35 40	_	52

		Si	ne of	24 1	Degre	es.			ير	S	ine of	25.1	Derro	900		Т
Min.		$-\frac{1}{0'}$	10"	20"	30"	40"	50"		Min	0"	10"	20"	Jegre 30"	40"	50"	-
О	9	609313				9502	9550	5g	0	9.625948						5
1	′	9597	9644	0601	9739	9786	9833	58	1	6219	6254	6309	6354	6400	16445	15
2		9880	9928	9975	22	69	.116	57	2	6490	6535	658o	6625	6670	6715	5
3	9.	610164	0211	0258	0305	0352	0399	56	3	6760	68o5	685o	6895	6940	6985	5
4							0682		4	. 7030	7075	7120	7165	7210	7255	5
5							0965		5	7300	7345	7390	7435	7480	7525	5
6							1247		6	7570	7615	7660	7705	7750	7795	5
7							1529		7	7840	7885	7929	7974	8019	8064	5
- 1							1811 2093		8	83-8	8154 8423	0199	0244	0550	8333	5
9	Λ.	612140							9	9.628647						
11	у.						2655		11	8916						
12							2936		12	9185	0220	0274	0310	0363	0/108	14
13		2983	3030	3077	3124	3171	3217	46	13	9453	9498	9542	9587	9632	9676	1/4
14							3498		14	9721	9766	9810	9855	9900	9944	. 4
25							3778		15	9989	34	78	.123	.168	.212	4
16							4058		16	9.630257						
7							4338		17	0524						
18							4618		18	0792	0836	0881	0925	0970	1014	-14
19	_						4898		19	1009	1103	1148	1192	1237	1281	14
- 1	9.	614944	4991	53.6	5363	5/00	5456	39		9.631326						
21							5735		2 I 2 2	1393	1637 1904	1001	1720	1770	1013	0
23							6013		23	2125	2170	221/	2250	2303	2001	3
24							6292		24		2436					
25		6338	6385	6431	6477	6524	6570	34	25		2702					
26		6616	6663	6700	6755	6802	6848	33	26		2968					
27		6894	6941	6987	7033	7080	7126	32	27		3233					
28		. 7172	7218	7265	7311	7357	7403	3 ı	28	3454						
29		7450	7496	7542	7588	7635	768 I	3о	29		3764					
	9.	617727	7773	7819	7866	7912	7958	29		9.633984	4028	4073	4117	4161	4205	12
31		8004	8050	8096	8143	8189	8235	28	31	4249	4293	4337	4381	4426	4470	2
32		8281	8327	8373	8419	8465	8512	27	32	4514	4558	4602	4646	4690	4734	2
33							8788		33	4778	4822	4800	4910	4934	4998	2
34							9064		34 35	5042 5306	535o					
36		0386	0/32	0/178	052/	0570	9340 9616	23	36		5614					
37		0662	0708	075/	0800	08/16	9892	22	37	5834						
88		0038	0084	30	76	.121	.167	21	38	6097	6141	6185	6220	6272	6316	2
	9.	620213	0250	0305	o351	0397	0443	20	39	6360						
ío.	ģ.	625488	o534	o58o	0626	0672	0718	19		9.636623	6667	6711	6754	6798	6842	1
11	•						0992		41	6886	6930	6973	7017	7061	7105	I
12							1267		42	7148	7192	7236	7280	7323	7367	I
43							1541		43	7411	7455	7498	7542	7586	7629	I
44		1587	1633	1678	1724	1770	1816	15	44	7673	7717	7760	7804	7848	7891	I
15							2089		45	7935	7979	8022	8000	8110	8153	I
16							2363 2637		46	8197 8458						
17 18							2910		47 48	8720	8763	8807	885 t	8804	8038	T
19		2056	3001	30/17	3002	3138	3183	10	49	8981	0025	0068	0112	0155	0100	I
10	ο.	623229	3274	3320	3365	3411	3456	9	50	0.630242	0286	0320	0373	0416	0460	1
1	,	3502	3547	3503	3638	3683	3720	8	51	9.639242 9503	9546	0500	6633	9677	9720	
52		3774	3820	38 6 5	3911	3956	4001	7	52	9764	9807	9851	9894	9937	9981	
53		4047	4092	4138	4183	4228	4274	6	53	9.640024	0068	0111	o 154	0198	0241	
54		4319	4364	4410	4455	4500	4546	5	54	0284	0328	0371	0414	o458	0501	
55		4591						4	55	0544						
56		4863	4908	4954	4999	5044	5089	3	56	0804						
57		5135	5180	5225	5270	5316	5361	2	57	1064						
58		5406	5451	5496	5542	2587	5632	I	58		1367					
59		5677						0	59		1626					-
1		60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"		10"	N.
			sine (Degr						sine o					1
_				4"	5" 6	" 7"	8"	9"		$\operatorname{Part}\left\{egin{array}{l} 1'' & 3' \\ 4' & 4'' \end{array}\right\}$	2" 3"	4"	5" 6	" 7"	8"	9

-	773			Log	Tangent of 24 Degrees. Tangent of 25 Degrees.													
Min.						50"		Min.						500				
o	9.648583	-	-	-		8866	59	0	9.668673	8728	8782			8947	59			
1				9093				1	9002	9057	9112	9167	9222	9277	58			
3	9263	9319	9376	9433 9772	9489	0885	56	3				9497 9826						
4	9002	9998	55	.111	.168	.224	55	4				.155						
5	9.650281	0337	0394	0450	0507	0563	54	5	9.670320	0375	0429	0484	0539	0594	54			
6				0789				6				0813						
7				1128				8				1142 1470						
9	1636	1692	1749	1805	1861	1918	50	9	1635	1689	1744	1799	1853	1908	50			
- 1	9.651974								9.671963									
II I2				2481 2819				11	2291 2619	2540	2728	2455 2783	2010 2838	2802	48			
13				3157				13				3111						
14	3326	3382	3438	3494	3551	3607	45	14				3438						
15				3832				15	3602									
17				4169 4506				16	3929 4257									
18				4843				18	4584									
19	5011	5067	5123	5179	5236	5292	40	19	4911	4965	5019	5074	5128	5183	40			
20	5684			5852				20 21	9.675237	56.8	5673	5401 5727	5455	5509	39			
22				6188				22	5890									
23	6356	6412	6468	6524	658o	6636	36	23	6217	6271	6325	638o	6434	6488	36			
24	6692	6748	6804	686o	6916	6972	35	24	6543									
25 26	7028	7084	7140	7196 7531	7252	7308	34	25 26	6869	5923	0977	7032 7357	7086	7140	34			
27	7600	7755	7811	7837	7022	7978	32	27	7520	7249 7574	7620	7683	7737	7701	$\frac{33}{32}$			
28	8034	8090	8146	8262	8258	8313	3т	28	7846	7900	7954	8008	8062	8117	31			
29	8369							29	8171									
30	9.658704	0005	0150	9206	0262	@318	28	30 31	9.678496 8821									
32	9373	9429	9485	9540	9596	9652	27	32	9146	0200	9254	9308	9363	9417	27			
33	9708	9763	9819	9875	9930	9986	26	33	9471	9525	9579	9633	9687	9741	26			
	9.660042							34				9958						
35 36	0376			0543				35	9.680120			0282 0606						
37	1043	1000	1155	1210	1266	1321	22	37				0930						
38	1377	1432	1488	1544	1599	1655	21	38	1092	1146	1200	1254	1308	1362	21			
39	1710	1766	1821	1877	1932	1988	20	39				1578						
41	9.662043	2099	2134	2543	2200 2508	2021 2654	19 18	40	9.681740			1901 2225						
42	2709	2765	2820	2876	2931	2987	17	42				2548						
43	3042	3097	3153	3208	3264	3319	16	43	2710	2764	2817	2871	2925	2979	16			
44				3541				44				3194						
46	4039	4004	4150	3873 4205	4260	4316	13	45 46				3517 3840						
47	4371	4426	4482	4537	4592	4648	12	47	4001	4055	4109	4162	4216	4270	12			
48	4703	4758	4814	4869	4924	4979	II	48	4324	4377	4431	4485	4539	4592	11			
49	5035 9.665366			5200				49	4646 9.684968	4700	4753 5075	4807	4861 5183	4914 5236				
51				5863				51	5200	5344	5307	5451	5505	5558	8			
52	6029	6084	6139	6194	6249	6305	7	52	5612	5666	5719	5773	5827	588o	7			
53				6525			6	53	5934	5987	6041	6095	6148	6202	6			
54				6856 7187			5 4	54 55	6255 6577	6630	6684	6416 6737	0470 6707	6845	5			
56	7352	7407	7462	7517	7572	7627	3	56	6898						3			
57	7682 8013	7737	7792	7847	7903	7958	2	57	7219	7273	7326	7380	7433	7487	2			
58	8013	8068	8123	8178	8233	8288	I	58	7540	7594	7647	7701	7754	7808	1			
59	8343						0	59				8021			0			
-	Co-tai	50"	40"	5 Do	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.			
		ngent 2" 3"			grees		9"	\square	$\frac{\text{Co-tar}}{\text{Part}\left\{\frac{1''}{5}\right\}}$	ngen 2″ 3′			grees		9"			

Min.				D. gre				Min.		ne of					
	0"	10"		:0"	40"	30"	<u>.</u>		0"	101	20"	30"	40"	50"	_
1	9.641842			1971 2230				1	9.657047	7336	7129	7171	7212 7460	7233	59
2				2489				2	7542	758.1	7625	7666	7707	77/10	57
3				2747				3	7790	7831	7872	7913	7955	7006	56
4				3006				4	8037	8078	8119	8161	8202	8243	55
5	3135	3178	3221	3264	3307	3350	54	5	8284	8325	8367	8408	8449	8490	54
6	3393	3436	3479	3522	3565	3607	53	6					8696		
7	365o	3693	3736	3779	3822	3865	52	7					8942		
8				4037				8					9189		
9				4294				9	9271	9312	9353	9394	9435	9476	50
	9.644423	4403	4500	4808	4294	4037	49	11	9.659517	9336	9399	9040	9927	9722	49
11	4036	4722	5000	5065	5108	5150	40	1 1	9.660009						
13	5103	5236	5270	5321	5364	5/07	46	13	0255	0206	0337	0378	0419	0//60	46
14				5578				14					0664		
15				5834				15					0909		
16				6090				16					1154		
17	6218	6260	63o3	6346	6388	6431	42	17	1236	1277	1318	1359	1399	1440	42
18	6474	6516	6559	6601	6644	6686	41	18	1481	1522	1563	1603	1644	1685	41
19	6729	6772	6814	6857	6899	6942	40	19	1726	1766	1807	1848	1889	1929	40
20	9.646984	7027	7069	7112	7154	7197	39	1 1	9.661970						
21	7240	7282	7325	7367	7409	7452	38	21					2377		
22	7494	7537	7579	7622	7664	7707	37	22	2459	2499	2540	2581	2621	2002	37
23				7877				23					2865		
24				8131				24					3109		
25 26				8385				25 26					3352 3596		
- I				8639 8893				27					3839		
27 28	0700	0063	0001	9147	0180	0970	31	28					4082		
29	027/	0316	0358	9401	0///3	0/85	30	29					4325		
30	9.649527	0570	0612	0654	0606	0730	20		9.664406						
3 r	9781	9823	9865	9907	9949	9992	28	31	• 4648						
	9.650034							32					5052		
33¦	0287	0329	0371	0413	0455	0497	26	33	5133	5173	5214	5254	5294	5335	26
34	0539	0582	0624	0666	0708	0750	25	34					5536		
35				0918				35					5778		
36				1171				36					6020		
37				1423				37					6561		
38				1675				38					6502		
39				1926				39	9.666824				6743		
	9.652052			2429				41					7225		
41 42				2680				42					7466		
43	2806	2848	2800	2931	2073	3015	16	43					7706		
44				3182				44	7786	7826	7866	7906	7946	7986	15
45	3308	3340	3301	3433	3475	3516	14	45	8027	8067	8107	8147	8187	8227	12
46	3558	3600	3642	3683	3725	3767	13	46	8267	8307	8347	8386	8426	8466	13
47	3808	385o	3892	3934	3975	4017	12	47					8666		
48				4184				48					8906		
49	4309	4350	4392	4434	4475	4517		49	8986	9026	9065	9105	9145	9185	10
	9.654558						9	50	9.669 2 25 9464	9265	9305	9345	9384	9424	1
51	4808	4850	4591	4933	4974	5055		5.0	9404	9504	9344	9304	0860	9003	`
52	5058	52/0	52-	5182	5/-2	55-7	7	52 53	9703	9743	9703	9023	9862	7/1	1
53				5680			5		9942 9.670181	9902	0260	0300	03/0	0370	1
54 55	5000 5865	5846	5888	5680 5929	5057	6010	4	55					0578		
50,				6178			3	56	0658	0607	0737	0777	0816	0856	
57				6426			2	57	0 806	0035	0075	1015	1054	1004	
58	655r	6502	6633	6675	6716	6757		58					1292		
59				6923				59	1372	1411	1451	1400	1530	1570	
7	60"	50"	40"	30"	20"	10"			60"	50"	40"	30"	20"	10"	-
				Degr		10	Min.			sine					Min
	(1//	2" 3"			6" 7"	8'	9"		(1"	2" 3			6" 7'	/ 8//	9'
	Part 🕽 🔒	~ 3	4		v (**	O	J	P	Part $\frac{1}{4}$	8 1			24 28		36

-	m			- T					m		. C or	- D			
Min.				Deg		F0#		Min.	Tan 0"	gent				F0#	
	9.688182	2035	20"	30"	40"	50"	50			70.18	20"	30"	40"	50"	50
1				8663				1	9.707166 7478				7686		
2				8983				2					7998		
3	9143	9196	9250	9303	9356	9410	56	3					8310		
4	9463	9516	9570	9623	9676	9730	55	4					8622		
5 6	9,690103	9830	9890	9943	19990	0360	53	5					8934 9245		
7				0582				7	9349	9401	0453	0504	9556	9608	52
8				0902				8	9660	9712	9764	9816	9868	9919	5 I
9				1221				9					.179		
	9.691381	1434	1487	1540	1594	1647	49		9.710282						
11				1859 2178				11					1111		
13				2497				13					1422		
14				2816				14					1732		
15				3134				15					2043		
16	3673	3665	3400	3453 3 771	3506	3559	43	16					2353 2663		
17	3030	3083	4036	4089	11/12	4105	42 /r	17					2973		
19	4248	43o1	4354	4407	446o	4513	40	19	3076	3128	3179	3231	3283	3334	40
20	9.694566	4619	4672	4724	4777	483o	39		9.713386	3438	3489	3541	3592	3644	39
21	4883	4936	4989	5042	5095	5148	38	21					3902		
22 23				5360 5677				22					4211		
24				5994				23					4521 4830		
25	6153	6206	6258	6311	6364	6417	34	25					5139		
26	6470	6522	6575	6628	668 r	6734	33	26	5242	5293	5345	5396	5448	5499	33
27	6787	6839	6892	6945	6998	7050	32	27					5757		
28	7103	7156	7209	7262	7314	7367	31	28					6065		
29 30	9.697736			7578				30	9.716477				6374		
31	8053	8105	8158	8211	8263	8316	29 28	31					6991		
32	8369	8421	8474	8527	8579	8632	27	32	7093	7145	7196	7247	7299	7350	27
33	8685	8737	8790	8843	8895	8948	26	33					7607		
34 35	9001	9053	9106	9159	9211	9264	25	34					7915		
36	0632	9309 9685	9422	9474 9790	08/2	0805	24	35					8223 8530		
37	9947		53	.105	.158	.210	22	37					8838		
38	9.700263	0315	o368	0420	0473	0525	21	38					9145		
39	0578	o63o	0683	0736	0788	0841	20	39	9248	9299	9350	9401	9452	9504	20
40 41	9.700893	0940	0998	1001	1103	1155	19		9.719555	9000	9057	9708	9760	9811	19
42	1523	1575	1628	1365 1680	1733	1470	17	41	9.720169						
43				1995				43					0680		
44	2152	2204	2257	2309	2362	2414	15	44	0783	o834	o885	0936	9987	1038	15
45	2466	2519	2571	2623	2676	2728	14	45					1294		
46				2938				46					1600		
47 48				3252 3566				47 48					1906 2213		
49	3722	3775	3827	3879	3932	3984		49	0 6				2519		
50	9.704036	4088	4141	4193	4245	4297	9	50	9.722621	2672	2723	2774	2825	2876	9
5 r	435o	4402	4454	4506	455g	4611	8	51	2927	2978	3029	3080	3130	3181	8
52 53	4663	4715	4768	4820	4872	4924	7	52					3436		7 6
54	5200	53/2	530/	5133 5446	5/08	555 r	6	53 54					3742 4047		5
55	5603	5655	5707	5759	5811	5863	4	55	4149	4200	4251	4302	4353	4403	4
56	5916	5968	6020	6072	6124	6176	3	56	4454	4505	4556	4607	4658	4709	3
57	6228	6280	6333	6385	6437	6489	2	57	4760	4810	4861	4912	4963	5014	
58	6541	6593	6645	6697	6749	6801	I	58					5268		I
59	60"	50"	40"	7010	7002	-	0	59	60"	50"		30"	5573 20"	10"	0
-	Co-ta					10"	Min.		Co-ta						Min.
		ngen			grees		9"						egrees		9"
P.	Port / - '	2" 3" 11 16	_		2 37		47	Ρ.		10 15			5" 7" 81 36		46
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5 ~				L	06	ARIT	r H	мі	SINE	s.	1				
l d	Si	ine of	28]	Degre	es.			i	Si	ine of	29]	Degre	ees.		T
Min	0"	10"	20"	30"	40"	50"	1	Min.	0".	10"	20"		40"	50"	
0	9.671609	1649	1688	1728	1768	1807	59	0	9.685571	5609	5647	5685	5723	5761	59
1	1847	1886	1926	1965	2005	2045	58	1	5799	5837	5875	5913	5951	5989	58
3						2282 2519		3	6027	6000	6330	6369	6178 6406	6216	57
						2756		4					6633		
5	2795					2992		5					686o		
6		3071	3111	3150	3190	3229	53	6	6936	6974	7012	7049	7087	7125	53
7	3268	3308	3347	3387	3426	3465	52	7	7163	7201	7238	7276	7314	7352	52
8						3702		8					7541		
9						3938		9	7616	7654	7692	7729	7767	7805	50
1 1	9.673977					4409			9.687843	7000	7918	7930	7993 8220	8051	49
11						4645		11					8446		
13						488o		13					8671		
14	4919	4959	4998	5037	5076	5115	45	14	8747	8784	8822	8860	8897	8935	45
15	5155	5194	5233	5272	5311	535o	44	15	8972	9010	9048	9085	9123	9160	44
16						5585		16					9348		
17						5820		17					9573		
18						6055		18					9798		
19	9.676328					6289 6523		19	9.60098	9911	9940	9900	02/8	0286	30
21						6757		21					0473		
22						6991		22					0697		
23	7030	7069	7108	7147	7186	7225	36	23					0922		
24	7264	7303	7342	7381	7420	7459	35	24	0996	1034	1071	1108	1146	1183	35
25	7498	7536	7575	7614	7653	7692	34	25					1370		
26						7925		26					1594		
27						8158 8391		27					1817		
20						8624		28 29					2264		
	9.678663								9.692339						
31						9089		31					2711		
32						9321		32	2785	2822	2859	2897	2934	2971	27
33	9360	9399	9438	9476	9515	9554	26	33					3157		
34	9592	9631	9670	9708	9747	9786	25	34	3231	3268	3305	3342	3379	3416	25
35	9824	9863	9902	9940	9979	17	24	35	3433 36=6	3490	3028	3202	3602 3824	3867	24
37	9.680056					0249		36 37	3808	3035	3072	4000	4046	1083	23
38						0712		38					4268		
39						0943		39	4342	4379	4416	4453	4490	4527	20
	9.680982								9.694564	4601	4638	4675	47-2	4749	19
41						1405		41	4786	4823	486o	4897	4934	4971	18
42						1636		42	5007	5044	5081	5118	5155	5192	17
43						1866		43					5376		
44						2097 2327		44					5598 5819		١ -
45						2557		45 46	5802	5020	5066	6003	6039	6076	13
47						2787		47	6113	6150	6187	6223	6260	6207	12
48	2825	2863	2002	2940	2978	3016	11	48					6481		
49	3055	3093	3131	3170	3208	3246	10	49	6554	6591	6628	6664	6701	6738	10
50	9.683284	3323	3361	3399	3437	3475	9		9.696775	6811	6848	6885	6921	6958	9
51	3514	3552	3590	3628	3667	3705		51	6995	7031	7068	7105	7141	7178	8
52	3743	3781	3819	3858	3896	3934	7	52	7213	7231	7288	7520	7361	7390	6
53	3972	4010	4048	4315	4120	4163	5	53 54	7433	7601	7708	7764	7581 7801	7838	
55	4/30	4468	4506	4544	4582	4620	4	55	787/	7011	7047	7984	8020	8057	4
56				4773			3	56	8004	8130	8167	8203	8240	8276	3
57				5001			2	57	8313	8349	8386	8423	8459	8496	2
58	5115	5153	5191	5229	5267	5305	1	58	8532	8569	8605	8642	8678	8715	I
59	5343	5381	5419	5457	5495	5533	0	59					8897		0
	60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
				Deg			1 1			sine o					
P.	Part J	2" 3"		-	7"		9"	P.	Part /	2" 3"			6" 7"		9"
1 -	4	8 19	2 16	19 2	3 27	31	35		4	7 11	15	19 5	22 26	30	33

0	ر ع	Тат	ngent	of 25	8 Dec	rrees			-:	Τ	Tai	ngent	of 29) De	rrees		1
0	Min						50"		Min.	-							1
1	0	F.C.			_			59	0	9	.743752	-		3901			50
2 6284 6334 6385 6336 6469 7040 6791 6844 856 3 4 6892 6431 8094 7045 7095 7146 55 4 4 4043 4992 5042 5092 5141 519155 55 7197 7247 7298 7340 7309 7450 54 5 5 240 5200 533 538 538 538 548 544 65 20 533 548 54 6 7501 7551 7602 7653 7703 7755 133 6 7501 7551 7602 7653 7703 7755 133 6 7 7805 7855 1962 7965 7705 7755 133 6 7 7805 7855 1962 7965 797 8058 52 7 8833 5884 5934 5933 6033 0882 51 8 8109 8159 8210 8861 8311 8362 51 8 6 133 6182 623 16 82 623 16 82 623 36 682 62 60 9 - 2287 68 876 887 88 8868 8918 8868 51 8 1506 40 9 1 0 0 9 7 20 7 20 7 20 7 20 7 20 7 20 7 2	_	1	1.	1	1 "	1 - 1	1-1		Н	1-							
3 6588 6639 6690 6740 6791 6842 56	2	6284	6334	6385	6436	6487	6537	57	2								
5	3	6588							3		4645	4695	4744	4794	4844	4893	56
66		6892	6943	6994	7045	7095	7146	55			4943	4992	5042	5092	5141	5191	55
7 7605 7855 7906 7957 8007 8058 52		7197	7247	7298	7349	7399	7450	54	II.	1							
8 \$ 10, 8 15, 9 850 826 1837 8366 55 5 6439 6479, 6529 6538 6577 6825 6874 6924 6973 49 111 9020 9070 121 1)71 9222 9272 48 111 7022 9279 48 7369 7927 7122 717 7221 7270 48 7468 7764 78 78 78 78 78 78 78 7	6								6								
9 841½ 8464 8564 8564 8665 8 0 9 6 49 6429 6479 6528 6577 6627 6676 650 9 79.78716 8876 981 8858 818 885 896 49 10 9 9 9 9 9 9 9 9 9 9 9 9 9 11 9 17 1 9 22 2 9 27 2 48 11 2 9 3 23 3 3 7 4 9 4 2 4 9 4 7 5 5 6 5 2 5 3 6 6 6 7 9 1 7 9 7 7 8 8 8 8 9 8 7 9 46 1 1 7 7 3 1 7 3 6 7 6 6 7 7 1 7 7 7 7 5 6 8 1 8 6 6 1 8 1 1 7 7 3 1 7 3 6 6 6 6 6 7 7 1 5 7 7 7 5 6 8 2 6 8 7 7 6 8 2 7 1 7 7 7 7 5 6 8 3 6 8 6 1 8 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1																	
10 9, 748716 8767 8817 8868 8918 8969 49 10 9, 746726 6775 6825 6874 6924 6973 6921 6971 7921	8	8109	8159	8210	8261	8311	8362	51	8								
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32										9.	0035	2091	3035	308/	3+33	3180	29
334											3037	3080	3330	3350	3/08	3/47	20
34											3526	3575	3604	3673	3722	3771	26
35																	
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38											4703	4752	1801	485a	4800	10/8	20
39											4007	50/6	5005	5 t // /	5103	52/2	21
40 9.737771 7821 7871 7921 7971 8021 19 40 9.755585 5634 5682 5731 5780 5829 19 8071 8121 8171 8221 8271 8321 18 41 5871 8421 8471 8521 8571 8621 17 43 8671 8721 8771 8821 8871 8921 16 43 6465 6514 6563 6612 6661 6710 16 44 8971 9021 9071 9121 9171 9221 15 44 6759 6808 6857 6905 6954 7003 15 9271 9321 9371 9420 9470 9520 14 45 7052 71101 7150 7199 7247 7296 14 7052 7101 7150 7199 7247 7296 14	- 1										5201	53/0	5380	5/38	5/87	5536	20
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42										7	5878	5027	5076	6025	6074	6r23	18
43											6172	6221	6270	6310	6368	6416	17
44		8671	8721	8771	8821	8871	8021	16									
45	1 -1																
46			- 1			· . · 1	1	. 11									
47	46										7345	7304	7443	7402	7541	7580	13
48 9.740169 0219 0265 0319 0368 0418 11 48 49 8224 8273 8322 8371 8419 8468 050 0.740767 0817 0867 0917 0967 1016 9 50 0.740767 0817 0867 0917 0967 1016 9 50 0.758517 8566 8615 8663 8712 8761 9 51 1066 1116 1166 1216 1265 1315 8 51 8810 8858 8907 8956 0905 0953 8 1365 1415 1465 1514 1564 1614 7 52 0102 0151 0200 0248 0297 0346 7 53 0644 0714 0763 0813 0863 0913 0 0877 0978 098	47								- 1		7638	7687	7736	7785	7834	7882	12
49											7031	7980	8020	8078	8127	8175	11
50 9.7407670817 0867 0917 0967 1016 9 50 9.758517 8566 8615 8663 8712 8761 9 51 1066 1116 1166 1216 1265 1315 8 51 8810 8858 8907 8956 9005 9053 8 8 1664 1714 1763 1813 1863 1913 6 53 9395 9443 9492 9541 9590 9638 6 54 1962 2012 2062 2112 2161 2211 5 54 9687 9736 9785 9833 9882 9931 5 55 2261 2311 2360 2410 2460 2510 4 55 99792877 . 126 . 174223 4 6 2559 2609 2659 2709 2758 2808 3 156 2257 2659 2709 2758 2808 3 156 3206 3255 3305 3355 3404 1 58 3156 3206 3255 3305 3355 3404 1 58 3156 3206 3255 3305 3355 3404 1 58 3156 3206 3255 3306 33653 3702 0 59 1148 1196 1245 1293 1342 1391 0 60° 50° 40° 30° 20° 10° 59 148 1196 1245 1293 1342 1391 0 60° 50° 40° 30° 20° 10° 59 10° 50° 40° 30° 20° 10° 50° 40° 30° 20° 10° 50° 40° 30° 20° 10° 50° 40° 30° 20° 10° 50° 40									- 1		8224	8273	8322	8371	8410	8468	10
51		9.740767	0817	0867	0917	0967	1016	- 11	50	9.	758517	8566	8615	8663	8712	8761	
52	51	1066	1116	1166	1216	1265	1315			′	8810	8858	8907	8956	9005	9053	8
53	- 1	1365	1415	1465	1514	1564	1614	7			9102	9151	9200	9248	9207	9346	7
54 1962 2012 2062 2112 2161 2211 5 54 9687 9736 9785 9833 9882 9931 5 55 2261 2311 2360 2410 2460 2510 4 55 9799		1664	1714	1763	1813	1863	1913	- 1	- 1		9395	9443	9492	9541	9590	9638	6
55 2261 2311 2360 2410 2460 2510 4 55 9979 28 77 .126 .174 .223 4 2559 2609 2659 2709 2758 2808 3 56 2.063 2659 2709 2758 2808 297 2957 3056 3106 2 57 0564 0612 0661 0710 0758 0807 258 3156 3266 325 3305 3355 3404 1 58 0856 0904 0953 1002 1050 1099 1 1148 1196 1245 1293 1342 1391 0 000	54							5			9687	9736	9785	9833	9882	993 r	5
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57	56	2550	2600	2650	2700	2758	2808	3	56	9.	760272	0320	0369	0418	0466	o515	3
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60" 57" 40" 30" 20" 10" E 60" 50" 40" 30" 20" 10" E Co-tangent of 61 Degrees. E Co-tangent of 60 Degrees. E P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2} \cdot 2" 3" 4" 5" 6" 7" 8" 9" P. Port \$\frac{1}{2}	59							0	- 1								
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0									9.711839	1874	1909	1944	1979	2014	59
2				9298 9517				1 2	2000	2085	2120	2155	2190	2225 2434	58
3	0626	0662	9600	9735	9771	9808	56	3	2460	2504	2530	257/	2600	2644	56
4	1			9953				4	2679	2714	2749	2784	2819	2854	55
5	9.700062	0099	0135	0171	0208	0244	54	5	2889	2924	2959	2994	3029	3063	54
6				0389				6	3098	3133	3168	3203	3238	3273	53
8	0498	0534	0071	0607 0825	0043	0680	52	8	3308	3343	3377	3412	3447	3482	52
9	0033	0070	1006	1042	1078	1115	50	9	3726	3761	3706	3830	3865	3691 3900	50
	9.701151	1187	1223	1250	1206	1332	40	10	9.713935	3070	4005	4030	107/	4100	10
11	1368	1404	1440	1477	1513	1549	48	11						4318	
12	1585	1621	1658	1694	1730	1766	47	12	4352	4387	4422	4457	4491	4526	47
13	1802	1838	1874	1911	1947	1983	46	13	4561	4596	463o	4665	4700	4735	46
14				2127				14						4943	
16				2344 2561				15	4970 5186	5012	5055	5000	530/	5151 5359	44
17								17						5567	
18				2993				18	5602	5636	5671	5705	5740	5775	4 r
19	3101	3137	3173	3209	3245	3281	40	19	5809	5844	5878	5913	5948	5982	40
1	9.703317	3353	3389	3425	3461	3497	39		9.716017						
21	3533	3509	3005	3641	3677	3713	38	21	6/24	6259	6293	6328	6362	6397	38
22				3856				22	6630	6673	6708	67/2	6770	6604 6811	36
24								24	6846	688o	6015	6040	6084	7018	35
25				4502				25	7053	7087	7122	7156	7191	7225	34
26	4610	4646	4682	4717	4753	4789	33	26	7259	7294	7328	7363	7397	7432	33
27	4825	4861	4896	4932	4968	5004	32	27						7638	
28	5040	5075	5111	5147	5183	5219	31	28						7844	
29	5254 9.705469	5505	55/0	5576	5610	56/8	30	29	7079 9.718085					8051	
31	5683	5710	5755	5700	5826	5862	29 28	31	8291						
32	5898	5933	5969	6005	6040	6076	27	32	8497						
33	6112	6147	6183	6219	6254	6290	26	33	8703	8737	8772	8806	884o	8874	26
34	6326							34	8909	8943	8977	9011	9046	9080	25
35	6539	6575	6804	6060	6005	6718	24	35	9114	9148	9183	9217	9251	9285	24
36	6753 6967	7002	7038	7073	7100	71/5	20	36 3 ₇	9320 9525	0550	0503	0627	0662	0606	23
38	7180							38	9730	9764	9708	0833	0867	9090	21
39	7393							39	9935	9969	3	38	72	.106	20
	9.707606	7642	7677	7713	7748	7784	19	40	9.720140						
41	7819							41	0345						
42								42	0549						
43	0.000	8/03	8528	856/	8500	8635	15	43	0754 0958						
45	8670	8705	8741	8776	8811	8847	14	45						1332	
46	8882	8918	8953	8988	9024	9059	13	46	1366	1400	1434	1468	1502	1536	13
47	9094	9130	9165	9200	9236	9271	12	47	1570	1604	1638	1672	1706	1740	12
48	9306	9342	9377	9412	9448	94831	II	48	1774	1808	1842	1876	1910	1944	II
49	9518	9553	9589	9024	9059	9095		49	1978 9.722181	2012	2046	2080	2114	2148	
51	9.709730 9941						8	51	2385	2/10	2/153	2487	2520	255/	9
52	9.710153	0188	0223	0250	0204	0320	7	52	2588						7
53	0364						6	53	2791	2825	2859	2893	2927	2960	6
54	0575	0611	0646	0681	0716	0751	5	54	2994	3028	3062	3096	3130	3163	5
55	0786						4	55	3197						4
56	0997						3	56	3400 3603						3
57	1208 1419						2	57 58	3805						2 I
59	1629						0	59	4007						0
- 7	60"	50"	40"	30"	20"	10"		- 7	60"	50"	40"	30"	20"		
				Degr			Min.				of 58				Min.
				5" 6		8"	9"			2" 3"			3" 7"	8"	9"
P.	Part /	7 11					32	Р.					1 24		31
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Min.	Tan.	gent	of 30	Deg	rees.			Min.		gent	of 31	Deg	rees.		-
	0′′	10"	20"	30"	40"	50"			0"	10"	20"	30"	40"	50"	L
U	9.761439							0	9.778774	8821	$ 886_{9} $	8917	8964	9012	5
I			1828					I	9060	9108	9155	9203	9251	9298	15
2			2120					2						9584	
3			2411					3		9679	9727	9775	9822	9870	5
4			2703					4						. 156	
5			2994						9.780203						
6			3285					6						0727	
7			3576					7						1013	
8			3867					8						1298	
9	4001	4110	4158	4207	4255	4304	20	9						1583	
	9.764352							14 1	9.781631						
H			4740					II	1910	1904	2011	03//	2307	2154 2439	14
12 13			5030					12	2201	2249	2587	2544	2591	2724	14
			5321 5611					13	2400	2334	0866	2029	2070	3009	14
14 15			5901					14	3056	310/	3,5,	3100	30/6	3294	14
16			6192					15						3578	
17			6482					17						3863	
18			6772					18						4148	
19			7062					19						4432	
20	9.767255	7303	7352	7/100	7/1/8	7/106	30	20	9.784479						
21	7545	7503	7641	7600	7738	7786	38	21						5001	
22	7834	7883	7931	7070	8027	8076	37	22	5048	5005	5143	5100	5238	5285	3
23	8124	8172	8221	8260	8317.	8365	36	23	5332	5380	5427	5474	5522	5569	3
24			8510					24	5616	5664	5711	5758	5806	5853	3
25			8799					25						6137	
26			9089					26						6421	
27	9281	9330	9378	9426	9474	9522	32	27						6705	
28	9571	9619	9667	9715	9763	9811	3 r	28						6988	
29	986o							29	7036	7083	7130	7178	7225	7272	3
3ó									9.787319	7367	7414	7461	7508	7556	2
31	0437	o485	o534	o582	o63o	0678	28	31	7603	7650	7697	7745	7792	7839	2
32	0726	0774	0822	0870	0919	0967	27	32	7886	7934	7981	8028	8075	8122	2
33	1015	1063	IIII	1159	1207	1255	26	33						8406	
34	1303	1351	1399	1448	1496	1544	25	34	8453	8500	8547	8595	8642	8689	2
35			1688					35						8972	
36	1880	1928	1976	2024	2072	2120	23	36						9255	
37	2168	2216	2264	2312	2361	2409	22	37	9302	9349	9397	9444	9491	9538	2
38			2553					38	9585	9532	9679	9727	9774	9821	2
39	2745	2793	2841	2889	2937	2985	20	39	9868	9915	9962	•••9	57	.104	2
40	9.773033	3081	3129	3177	3225	3273	19		9.790151	0198	0245	0292	0339	0386	I
41	3321	3369	3417	3405	3512	3560	18	41						0669	
42			3704					42						0952	
43			3992					43	0999	1040	1002	1140	1107	1234	I
44 45			456					44	1201	1528	1659	1422	1409	1516	1
45 46			4567					45						2081	
47	50/6	500/	4855 5142	5100	5038	5086	10	46 47						2363	
48			5429					47						2645	
49	5621	5668	5716	576/	5812	5860	10		2602	2730	2786	2833	2880	2927	I
	9.775908						9	49 50	9.792974	3021	3068	3115	3162	3200	٦
51			6290				8	51	3256	3303	3350	3307	3444	3491	1
52	6482	6529	6577	6625	6673	6721	7	52	3538	3585	3632	3670	3726	3773	
53	6768	6816	6864	6912	6960	7007	6	53	3810	3866	3913	3960	4007	4054	1
54	7055	7103	7151	7199	7246	7294	5	54						4336	
55	7342	7390	7437	7485	7533	758ı	4	55						4617	
56	7628	7676	7724	7772	7810	7867	3	56						4899	
57	7915	7963	8010	8058	8106	8154	2	57	4946	4992	5039	5086	5133	5180	
58	8201	8249	8297	8344	8392	8440		58	5227	5274	5321	5367	5414	5461	1
59	8488	8535	8583	8631	8678	8726	0	59	5508	5555	5602	5649	5696	5742	
ŕ	60"	50"	40"		20"	10"	نے	⊩	60"	50"		30"		10"	1
	Co-ta		·				Min.		Co-ta	·					-
							9"		l						_
	Part \ \ \frac{1''}{\pi} \ \ \frac{1}{\pi}	2" 3"	4"	5" (3" 7"	8′′	0//	{	Part $\begin{cases} 1'' \\ 5 \end{cases}$	2'' - 3	// A//	5"	6" 7'	′′ 8′′	9

	1							~						-
Min.	S	ine of 3					Min.		ne of					1
	0'	10" 20		40"	50"			0"	10"	20"	30"	40"	50"	
1 0	9.724210						0	9.736109						
I	4412	4445 44	79 4513	4540	4580	58	1						6465	
1 2	4014	4647 46 4849 48	83 4015	4740	4702	56	3						6659	
3	5017	5051 50	85 5118	5,50	5185	55	4						6854 7048	
5	5210	5253 52					5	7080	7112	71/5	7177	7200	7241	54
6		5454 54					6	7274	7306	7338	7371	7403	7435	53
7		5655 56					7	7467	7500	7532	7564	7597	7629	52
8	5823	5856 58	90 5923	5957	5990	51	8	7661	7693	7726	7758	7790	7822	51
. 9	C 1	6057 60					9	7855	7887	7919	7951	7983	8016	50
10	9 726225	6258 62					10	9 .73 8048	8080	8112	8145	8177	8209	49
11		6459 64					II						8402	
12		666o 66	·	1 - ' - 1			12						8595	
13		6860 68					13	8027	8039	8092	8724	8756	8788	46
14		7061 70					14	0020	0032	0004	0917	0949	8981	43
16		7261 72					15 16	9013	0238	9077	0302	0334	9173 9366	44
17		7661 76					17						9558	
18		7861 78					18	9590	9622	9654	9687	0710	0751	41
19		8061 80					19	9783	9815	9847	9870	9911	9943	40
	9.728227	8260 82	94 8327	836o	8393	39	20	9.739975	7	39	71	.103	.135	39
21	8427	8460 84	93 8526	856o	8593	38	21	9.740167	0199	0231	0263	0295	0327	38
22		8659 86					22						0519	
23		8858 88					23						0710	
24		9058 90					24						0902	
25	9223	9257 92	90 9323	9330	9389	34	25						1093	
26	9422	9455 94	109 9522	9555	9300	30	26						1284 1476	
27		9853 98					27 28						1667	
	9.730018	0051 00	8/ 0117	0150	0183	30	29						1858	
	9.730217						30	9.741889	1921	1953	1985	2017	2049	29
31		0448 04					31						2239	
32	0613	0646 06	79 0712	0745	0778	27	32	2271	2303	2335	2366	2398	2430	27
33	0811	0844 08	377 0910	0943	0976	26	33						2620	
34		1042 10					34						2811	
35		1239 12					35						3001	
36	1 1	1437 14					36						3191 3381	
37		1634 16					37 38						3571	
39	1799	2029 20	62 2005	2127	2160	20	39						3761	
1 /6	9.732193	2226 22	50 2202	2325	2357	10	40	9.743792						
41		2423 24					41	3982	4013	4045	4077	4108	4140	18
42		2620 26					42	4171	4203	4234	4266	4297	4329	17
43	2784	2816 28	349 2882	2915	2948	16	43	4361	4392	4424	4455	4487	4518	16
44	2980	3013 30	46 3.079	3111	3144	15	44						4707	
45	3177	3210 32	242 3275	3308	3340	14	45						4896	
46		3406 34					46						5085 5274	
47	3765	3602 36 3798 38	735 3007 33	3806	3020	12	47						5463	
48	3761	3994 40	27 /050	4002	4125	10	49	5404	5526	5557	5580	5620	5651	10
50	9.734157	4100/42	222 4255	4288	4320	9	50	9.745683	5714	5746	5777	5808	5840	9
51	4353	4386 44	118 4451	4483	4516	8	51	5871	5903	5934	5965	5997	6028	8
52	4540	4581 46	514 4646	4679	4711	7	52	6060	6091	6122	6154	6185	6216	7
53	3 4744	14777 48	300 4842	4874	4907	6	53	6248	6279	6310	6342	6373	6404	6
54	4939	4972 50	004 5037	5069	5102	5	54						6592	
55	5135	5 5 1 6 7 5 2	200 5232	5265	5297	4	55						6780	
56	5330	5362 53	395 5427	5460	5492	3	56						6968	
5.5	5525	5557 55	90 3022	5840	5882	2 I	57 58	0999	7031	7002	7281	7319	7156 7343	I
50		5752 57 5947 59	70413017	6044	6076	0	59		7/106	7/37	7468	7400	7530	0
1	60"		30"	20"	10"		1	60"	50"	40"	30"		10"	-
		-sine of			1. 10	Min.			sine	1				Min.
-	7 (1"			3" 7"	8"	9"			$\frac{2''}{3}$		5"		' 8"	9"
P	. Part \ \ \ \ \ \ \ 3			20 23		30	Ρ.	Part $\begin{cases} 1'' \\ 3 \end{cases}$	-	0 13		19 2:		29
1	()		'	~0			11	(-						

				Log	AR	ТН	M I	O .	IANGE	NTS	·				5
Min.	Tan	gent	of 32	2 Deg	rees.			Min.	Tar	igent	of 33	3 Deg	rees.		
Z	0"	10"	l	30"	40"	50"		Z	0"	10"	20"	30"	40"	טטיי	<u> </u>
0	9.795789							0	9.812517						
I 2				6211 6492				1 2	2794 3070	3116	2886 3163	3200	3255	3301	57
3				6773				3	3347	3393	3439	3485	3531	3577	56
4	6913	6960	7007	7053	7100	7147	55	4	3623	3669	3715	3761	3807	3853	55
5	7194	7241	7287	7334	7381	7428	54	5	3899	3945	3991	4037	4083	4129	54
6	7474	7521	7568	7615 7895	7002	7708	50	6	4170	4222	4268 4544	4514	4636	4682	50
78	8036	8082	8120	8176	8223	8260	51	8			4820				
9	8316	8363	8409	8456	8503	8550	50	9	5004	5050	5096	5142	5188	5234	50
	9.798596	8643	8690	8737	8783	883o	49	1 1	9.815280						
II				9017				II			5647				
13	0437	0484	0530	9297 9577	0624	0670	47	13	6107	6153	5923 6199	6245	6201	6336	47
14				9857				14			6474				
15	9997	44	90	.137	. 184	.230	44	15	6658	6704	6750	6796	6842	6888	44
	9.800277	0324	0370	0417	0463	0510	43	16	6933	6979	7025	7071	7117	7163	43
17	0337	0883	0030	0697 0976	1023	10790	42	17	7209	7200	7301 7576	7622	7592	771/	42
19				1256				19			7851				
20	9.801396	1442	1489	1535	1582	1629	39		9.818035						
2 I	1675	1722	1768	1815	1862	1908	38	21	8310	8356	8402	8447	8493	8539	38
22 23				2094				22	8585	8631	8677	8722	8768	8814	37
24	2513	2560	2527	2374 2653	2600	27/16	35	23 24	0135	0181	8952 9226	0272	0318	0364	35
25	2792	2839	2886	2932	2979	3025	34	25	9410	9455	9501	9547	9593	9639	34
26				3211				26	9684	9730	9776	9822	9868	9913	33
27	3351	3397	3444	3490	3537	3583	32	27	9959	5	51	96	. 142	.188	32
28 29				3769 4048				1 1	9.820234		0525				
	5.804187	4234	4280	4327	4373	4420	20	29 30	9.820783						
31	4466	4513	4559	4605	4652	4698	28	31	1057	1103	1149	1195	1240	1286	28
32	4745	4791	4838	4884	493o	4977	27	32	1332	1377	1423	1469	1515	1560	27
33				5163				33			1697				
34 35				5441 5719				34 35			1972 2246				
36				5998				36	2420	2474	2520	2566	2611	2657	23
37	6137	6183	6230	6276	6322	6369	22	37	2703	2748	2794	2840	2885	2931	22
38				6554				38	2977	3022	3068	3114	3159	3205	21
39				6832				39	3251 9.823524	3570	3342	3667	3433	3479	20
40 41	72/0	7206	73/12	7388	7435	7481	18	41			3889				
42	7527	7574	7620	7666	7713	7759	17	42	4072	4117	4163	4209	4254	4300	17
43	7805	7851	7898	7944	7990	8037	16	43			4437				
44				8222				44			4710				
45 46				8499 8777				45	4093 5166	5212	4984 5257	5303	5348	5304	13
47	8916	8962	9008	9055	9101	9147	12	47	5439	5485	5531	5576	5622	5667	12
48	9193	9240	9286	9332	9378	9424	II	48	5713	5758	5804	5849	5895	5940	II
49	9471	9517	9563	9609	9656	9702	10	49	5986	6032	6077	6123	6168	6214	10
	9.809748 9.810025							50 51	9.826259		6350				
52				0441				52	6805	685 T	6896	6042	6087	7033	7
53	o58o	0626	0672	0718	0764	0810	6	53	7078	7124	7169	7215	7260	7306	6
54	0857	0903	0949	0995	1041	1087	5	54	7351	7397	7442	17488	7533	7579	5
55				1272				55	7624	7670	7715	7761	7806	7851	4
56 57	1687	1437	1780	1549 :826	1872	1041	2	56	7097	7942	7988 8261	8306	8351	8307	3
58	1964	2010	2056	2102	2149	2195	I	58			8533				
59	2241	2287	2333	2379	2425	2471	0	59	8715	8760	8806	8851	8897	8942	0
	60"	50"	40"	30"	20"	10"	ď		60"	50"	40"	20"	20"	10"	-
	Co-ta	ngen	t of 5	7.De	0		Min.		Co-ta			56 De	egrees	3.	Min.
P.	Part /	2" 3'	-		3" 7"		9"	р	Part { 1"			-	5" 7"	_	9"
- •	1 and 5	9 1	4 - 19	23 9	2 8 33	37	42	1.	1 411 5	9 1	4 18	23	2 7 32	2 37	41

.5		ne of	34 T	Degre	es			ندا	1	Si	ne of	35 1	Degre	02		
Min.	0"	10"	20"	30"	40"	50"		Min		0"	10"	20"	30"	40"	50"	
	9.747562								9.	758591	8621	8651	8681	8712	8742	59
2	7749	7780	7811	7842 8030	7874 8061	7905	58 57	1 2		8052	8082	0012	00/2	0072	8922 9102	58
3	8123	8154	8185	8216	8248	8279	56	3		9132	9162	9192	9222	9252	9282	56
4				8403				4		9312	9342	9372	9402	9432	9462	55
5 6	8497	8528	8559 85/5	8590 8777	8808	8830	54	5 6		9492 9672	9522	9552	9582	9612	9642	54
7	8870	8901	8932	8963	8994	9025	52	7		9852	9881	9911	9941	9792	9022	52
8	9056	9087	9118	9149	9180	9212	5 ı	8	9.	76003 I	0061	0091	0121	0151	0181	51
9				9336				9							0360	
11	9.749429	9400 06/16	0677	9708	9555	9270	49 48	10	9.	760390 0560	_				0339	1 : /
12	9801	9832	9863	9894	9925	9956	47	12							0898	
13	9987	18	48	79	.110	.141	46	13	ı						1076	
	9.750172							14	ı						1255 1434	
15				0451 0636				16	1						1613	
17				0821				17	l	1642	1672	1702	1732	1761	1791	42
18				1007				18		1821	1851	1880	1910	1940	1969	41
19				1192				19		1999 762177	2029	2059	2088	2118	2148	40
20 21	9.751284			1561				21							2504	
22	1654	1685	1715	1746	1777	1808	37	22	I	2534	2563	2593	2623	2652	2682	37
23	1839	1869	1900	1931	1962	1992	36	23	ł	2712	2741	2771	2801	2830	2860	36
24				2115				24 25		2889	2919	2949	2978	3008	3038	35
25 26				2300 2484				26							3215 3393	
27				2668				27	1	3422	3452	3481	3511	3540	3570	32
28	2760	2791	2822	2852	2883	2914	31	28		3600	3629	3659	3688	3718	3747	31
29	2944	2975	3005	3036	3067	3097	30	29							3925	
31	7.753128	33/2	3373	3404	3/3/	3/65	29 28	31	9.	763954 /131					4279	
32				3587				32		4308	4338	4367	4396	4426	4455	27
33	3679	3710	3740	3771	3801	3832	26	33	i	4485	4514	4544	4573	4603	4632	26
34				3954				34							4809	
35 36				4137 4320				35 36	1						4985 5162	
37				4503				37	1	5191	5221	5250	5279	5309	5338	22
38	4595	4625	4656	4686	4717	4747	21	38		5367	5397	5426	5456	5485	5514	21
39	4778	4808	4839	4869	4900	4930	20	39							5690	
40	9.754960 5143	4991	520/	5234	5265	5205	18	41		765720 5806	5025	505/	5084	6013	6042	18
42				5417				42	1	6072	6101	6130	6159	6189	6218	17
43	5508	5538	5569	5599	5629	566o	16	43							6394	
44	5690	5721	5751	5781	5812	5842	15	44							6569 6745	
45 46				5963 6145				45 46							6920	
47	6236	6267	6297	6327	6358	6388	12	47	1						7095	
48	6418	6448	6479	6509	6539	6570	11	48		7124	7154	7183	7212	7241	7270	II
49				6691				49							7445	
50 51	9.756782	6003	5842	7054	708/	0933	8	51		767475					7795	
52	7144	7175	7205	7235	7265	7205	7	52	ł	7824	7853	7882	7912	7941	7970	1
53	7326	7356	7386	7416	7446	7477	6	53	1	7999	8028	8057	8086	8115	8144	6
54	7507	7537	7567	7597	7627	7658	5	54		8173	8203	8232	8261	8290	8319	5
55 56	7688	7718	7748	7778 7959	7808	7839	3	55		8522	8551	8580	8600	8638	8493 8668	3
57				7939 8140			2	57		8697	8726	8755	8784	8813	8842	2
59	8230	8260	8290	8321	8351	8381	I	58		8871	8900	8929	8958	8987	9016	I
59	8411	8441	8471	8501	8531	8561	0	59		9045	9074	9103	9132	9161	9190	0
	60″	50"	40"	30"	20"	10"	Min.			60"	50"	40"	30″	20"	10"	Min.
	Co-	sine o	of 55	Degr	rees.		×			Co-	sine		Deg			9"
	n . (1"	2" 3"	4"	5" (5" 7"	8"	9"		Pa	. (1"	2" 3	" 4"	5"	6" 7"	/ 8"	

Tangent of 34 Degrees.						LOG	AK	1 1 11 .			ANGE		·				
0 9.888987 9033 978 9134 9169 915 59 1 960 9345 927 5346 5355 5406 5456 555 546 5355 546 5355 546 5456 5555 546 5355 546 5456 5456 5555 546 5456		ji,		gent	of 34	l Deg	rees.			j.	t	gent	of 35	Deg	rees.		
1 9860 305 331 306 6442 9487 58 1 5496 5346 538 53636 575 5720 53 3 9505 985 985 985 985 985 985 985 585 589 985 545 589 5445 585 55 55 55 55 55 56 56 56 56 56 56 56 56														-	<u> </u>		
2 \$\sigma_0^3 \sigma_0^3 \sig			9.828987	9033	9078	9124	9169	9215	59	11							
3			0532	9303	9331	9390	9442	9487	55	1							
A 0, 830077 6122 6168 6213 6258 6304 655 6304 6304 6345 6310 6367 6716 6365 6364 6365	1		9805	0850	0805	0041	0086	32	56								
G		4								1 .	6302	6347	6391	6436	6481	6526	55
7										1							
S	١		0021	0007	0712	0757	0803	0848	53								
10 38170 1755 1806 1845 1801 1936 49	1	8	1165	1211	1256	1301	1347	1302	5 t		7376	7421	7/197	7510	7555	7600	51
10 0.831700 1755 1800 1845 1891 1936 49 11 1931 206 2072 2117 216 2208 48 12 2525 2570 2613 2606 2706 2751 46 13 2525 2570 2613 2606 2706 2751 46 14 2790 2842 2887 2932 2977 3033 45 15 3068 3113 3158 3204 3349 3324 4479 47 16 3339 3385 3433 3475 3520 3566 43 17 3611 3656 3701 3747 3792 3837 42 18 3888 3927 3973 4618 4638 4108 41 19 4154 4199 4244 4289 4334 4380 40 20 9.834425 4470 4513 4566 4651 30 21 4069 4741 4787 4832 4877 4823 8876 8857 8857 8857 8858 8673 47 22 4967 5012 5058 5103 5148 5103 37 22 4967 5012 5058 5103 5148 5103 37 23 5238 5288 5320 5374 5415 6606 634 25 5780 5826 5871 5076 561 6006 34 26 6051 6066 6144 6187 606 634 27 37 47 47 57 67 78 78 78 28 6530 3633 6868 6868 6868 6788 6773 7802 31 7405 7480 7481 7856 7901 7912 7902 7912 7912 7902 7912 7902 791	1																
12		10	9.831709	1755	1800	1845	1891	1936	49		9.847913	7957	8002	8047	8092	8136	49
13	1		1981	2026	2072	2117	2162	2208	48	1	8181	8226	8270	8315	8360	8405	48
14 2796 8842 887 2032 2077 3003 45 14 8986 0030 0075 0120 10f40 2009 45 15 3068 3113 3158 3204 3240 324 4 15 9254 928 0343 388 0432 077 44 16 3339 3385 3430 3475 3520 3566 43 16 9752 9566 961 0656 9700 9745 43 18 3882 3927 373 4018 4063 4108 41 17 9790 9834 987 9924 9968 .113 42 19 4154 4199 4244 489 4334 4380 40	1		2233	2570	2545	2589	2434	2479	47	1 - 1	8717	8762	8807	885 ₁	8806	80/1	47
15	1		2796	2842	2887	2032	2077	3023	45	1 -1							
166	1		3068	3113	3158	3204	3249	3294	44	1	9254	9298	9343	9388	9432	9477	44
18	١		3339	3385	3430	3475	3520	3566	43	16	9522	9566	9611	9656	9700	9745	43
19																	
20 0,834455 4470 4515 4561 4606 4651 39										i 1							
22	1	20	9.834425	4470	4515	4561	4606	4651	30								
23	1		4696	4741	4787	4832	4877	4922	38								
24	1	- 1	4967	5012	5058	5103	5148	5193	37	1 1							
25			5500	5555	5600	56/5	5600	5404	36	۱ . ۱							
266 6051 6096 6142 6187 632 6277 33 27 2466 2511 2555 2600 2644 2689 32 28 6593 6638 6683 67928 6773 6819 31 28 2733 2778 2823 2887 322 379 2423 33 30 9.837134 7179 7225 7270 7315 7360 29 30 9.837134 7179 7225 7270 7315 7360 29 30 9.837134 7179 7225 7270 7315 7360 29 30 9.837134 7179 7225 7270 7315 7360 29 30 9.83733 357 3402 3446 3491 29 2705 7455 7450 7455 7450 7585 7450 29 30 9.835368 3373 3357 3402 3446 3491 29 32 32 30 9.835368 3373 3357 3402 3446 3491 29 32 32 30 9.835368 3373 3357 3402 3446 3491 29 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 20 32 32 30 9.835368 3373 3402 3446 3491 29 22 32 32 32 32 32 32 32 32 32 32 32 32	1	1	5780	5826	5871	5016	5061	6006	3/1	1 - 1	1031	1076	2020	2065	2110	2154	34
28 632e 6367 6412 6458 6503 6348 32 27 2466 2511 2555 2600 2644 2686 32 296 6864 6999 6954 6999 7044 7089 30 3001 3045 3090 3134 3179 3223 330 309 837134 7179 7225 7270 7315 7360 29 31 3351 3357 3402 3446 3491 29 32 7405 7450 7450 75450 75450 7585 7630 28 31 3351 3357 3402 3446 3491 29 32 7075 7721 7766 7811 7866 7811 7866 7811 7866 7811 7966 7811 7866 7811 7966 7818 7966 7812 7966 7812 7966 7811 7966 7961			6051	6096	6142	6187	6232	6277	33	[
29 6864 6909 6954 6999 7044 7089 30 3001 3045 3009 3134 3179 3223 30 309 837134 7179 7225 7270 7315 7360 28 31 3535 3588 3313 3357 3402 3466 3461 3405 7450 745			6322	6367	6412	6458	65o3	6548	32	1 1	2466	2511	2555	2600	2644	2689	32
36 9.837134 7176 7225 7270 7315 7360 29 30 9.853268 3313 3357 3402 3446 3491 29 32 7405 7450 7455 7450 7585 7630 28 311 3535 3580 3624 3669 3713 3758 28 37946 7991 8036 8081 8126 8171 26 33 4069 4114 4158 4203 4247 4292 26 27 4781 4826 24 4366 4364 4669 4747 4781 4826 24 4366 4364 4669 4748 7481 4455 25 25 4481 4485 4470 4514 4559 25 4481 4485 4470 4514 4559 25 4481 4485 4470 4514 4559 25 4481 4485 4485 4470 4481 4485 4470 4481 4485 4470 4481 4485 4481 4485 4481 4485 4481 4485 4481 4485 4481 4485 4481 4485 4481 4485 4481 4485 4481 4	l	- 1								l i							
31			0.83713/	7170	7225	7270	7044	7009	30								
32																	
34	1		7675	7721	7766	7811	7856	7901	27	32	3802	3847	3891	3936	398o	4025	27
35			7946	7991	8036	8081	8126	8171	26		4069	4114	4158	4203	4247	4292	26
36	1	35	8/87	8532	85mm	8600	8667	8710	25								
37			8757	8802	8847	8802	8037	8082	23								
38	١		9027	9072	9117	9162	9207	9252	22								
40 9.839838 9883 9928 9973 18 63 19 . 46 9.855938 5982 6026 6071 6115 6160 19 . 4840108 0153 0168 0243 0248 0333 18 . 41 . 6204 6249 6293 6338 6382 6426 18 . 42 . 0378 0423 0468 0513 0558 0603 17 . 42 . 6471 6515 6560 6604 6649 6693 17 . 43 . 0648 0693 0737 0782 0827 0872 16 . 43 . 6737 6782 6826 6871 6915 6959 16 . 44 . 0917 0962 1007 1052 1097 1142 15 . 44 . 7004 7048 7093 7137 7182 7226 15 . 187 1232 1277 1322 1367 1412 14 . 45 . 7270 7315 7359 7404 7448 7492 14 . 46 . 1457 1502 1547 1592 1637 1682 13 . 46 . 7537 7581 7626 7670 7714 7759 13 . 47 . 1727 1771 1816 1861 1906 1951 12 . 47 . 7803 7848 7892 7936 7981 8025 12 . 48 . 1996 2041 2086 2131 2176 2221 11 . 48 . 8069 8114 8158 8203 8247 8291 11 . 48 . 8069 8114 8158 8203 8247 8291 11 . 48 . 8069 8114 8158 8203 8247 8291 11 . 48 . 8069 8114 8158 8203 8247 8291 11 . 48 . 8069 8114 8158 8203 8247 8291 11 . 805 2849 2894 2039 2984 3029 8 . 51 . 8860 8046 8691 8735 8779 8824 9 . 8860 8046 8091 8735 8779 8824 9 . 8860 8046 8091 8735 8779 8824 9 . 8860 8046 8091 8040 9040 9044 9049 9040	Ì		9297	9343	9 388	9433	9478	9523	21								
41 9.840108 0153 0108 0243 0288 0333 18	1	39	9568	9013	9658	9703	9748	9793	20								
42	l	40	0.8/0108	0153	0108	02/3	0288	0333	19								
43	1		0378	0423	0468	0513	0558	0603	17	1 : 1							
45	1	43	0648	0693	0737	0782	0827	0872	16		6737	6782	6826	6871	6915	6959	16 l
46	1										7004	7048	7093	7137	7182	7226	15
47		1 -1									7270	7313	7359	7404	7448	7492	14
48	1	- 1								1 : (7337 7803	7848	7802	7036	7081	8025	12
49			1996	2041	2086	2131	2176	2221	11		8069	8114	8158	8203	8247	8291	11
51	1	49	2266	2311	2355	2400	2445	2490	10	49	8336	838o	8424	8469	8513	8558	10
52	-										9.858602	8646	8691	8735	8779	8824	
53	-	1	307/	3110	2094 316/	3200	3253	3208	- 1	1 .	0134	0178	0937	9001	9045	9090	0
54			3343	3388	3433	3478	3523	3568	6		9400	9444	9480	0533	9577	9622	6
55		54	3612	3657	3702	3747	3792	3837	5	1	9666	9710	9755	9799	9843	9888	5
57			3882	3927	3971	4016	4061	4106	4		9932	9976	21	65	.109	. 154	
58			4101	4196	4241	4285	4530	4677	- 1		9.860198	0242	0287	0331	0375	0420	3
59 4958 5003 5048 5092 5137 5182 0 59 0995 1040 1084 1128 1172 1217 0 60" 50" 40" 30" 20" 10" 5			4420 4680	4734	4770	4823	4868	4044			0730	077/	0818	0869	0041	0051	
Co-tangent of 55 Degrees. E									- 1	1 1	0995	1040	1084	1128	1172	1217	
P. Part 1" 2" 3" 4" 5" 6" 7" 8" 9" P. Part 1" 2" 3" 4" 5" 6" 7" 8" 9"	-										60"	50"	40"	30"	20"	10"	
P. Part \ 1" 2" 3" 4" 5" 6" 7" 8" 9" P. Part \ 1" 2" 3" 4" 5" 6" 7" 8" 9"	-		Co-ta	ngent	t of E	$55~\mathrm{De}$	grees	s.	Mi		Co-ta	ngen	t of a	54 De	egrees	3.	Min
(5 9 14 18 23 27 32 36 41 11 11 11 (4 9 13 18 52 27 31 36 40	,	Р.			_			-	- 1	Р	Part /	-	_		-		
	L		₹ 5	9 14	18	23 2	7 32	36	41	Ľ.	4	9 13	18	22 2	27 31	36	40

Min.				Degre				Min.				f 37	Degr	ees.		I
	0"	10"	20"	30 ′	40"	50"				0"	10"	20"	30"	40"	50"	
0	9.769219	9248	9277	9306	9335	9364	59	C	9.	779463	9491	9519	9547	9575	9603	50
1	9393	9421	9450	9479	9568	9537	58	1		9631	9659	9686	9714	9742	0770	158
2	9566	9595	9624	9653	9682	9711	57	2		9798	9826	9854	9882	9910	0038	5
3				9827				3		9966	0003	21	40	77	. 105	151
4	,0013	9942	9971		20	58	55	4	9.	. 7 86 i 33	6161	0180	0216	0244	0272	5
5	9.770087	0116	0145	0173	0202	0231	54	5		0300	0328	0356	038/	0411	0/30	5
6				0347				6						0578		
7				0520				7	ŀ	063/	0662	0600	0718	0745	0773	5.
8	0606	0635	0664	0693	0722	0750	5 T	8		* 0801	0820	0857	0884	0010	00/0	5
9				0866				11	1	0068	0006	1003	7.057	1079	0940	5
10	9.770952							9		781134	7760	1020	1031	10/9	1107	1
11				1211					9.							
- 1				1384				11						1412		
12 13								12						1578		
				1556				13	•	1034	1002	1009	1717	1745	1772	40
4				1729				14	1	1000	1828	1856	1883	1911	1939	43
5				1901				15		1900	1994	2022	2049	2077	2105	44
t 6				2073				16		2132	2100	2188	2215	2243	2271	43
7				2245				17						2409		
8				2417				18						2575		
9	2503	2532	2561	2589	2018	2046	40	19	1					2741		
	9.772675							20	9.	782796						
1				2933				21		2961	2989	3017	3044	3072	3099	38
22	3018	3047	3076	3104	3133	3161	37	22		3127	3154	3182	3210	3237	3265	37
3	3190	3219	3247	3276	33o4	3333	36	23						3402		
4				3447				24		3458	3485	3513	3540	3568	3595	35
5	3533	3561	3590	3618	3647	3675	34	25		3623	365o	3678	3705	3733	3760	32
6	3704	3732	3761	3789	3818	3846	33	26		3788	3815	3843	3870	3898	3025	33
7				3960				27		3053	3080	4008	4035	4063	4000	32
8				4131				28						4228		
29				4302				29						4392		
	9.774388							30	٥.	784447	1/175	4502	1520	4557	4584	20
I	4558	4587	46±5	4644	4672	4700	28	31	,					4721		
2	4720	1757	4786	4814	18/12	1871	27	32						4886		
3				4985				33						5050		
4	5070	5008	5106	5155	5.83	5212	25	34		5105	5,30	5160	5185	5214	50/0	0.5
5	50/0	5268	5005	5325	5353	5380	04	35						5378		
6	5/10	5/38	5/67	5495	5503	5550	03	36						5543		
7	5580	5608	5637	5665	5603	5700	20							5706		
8	5=50	58	5807	5835	5863	5800	22	37 38								
- 1	5730	5770	5007	6005	6-22	6-6-	21							5870		
9	3920	60	0977	6005	0033	6-2-	20	39		-96-9-	3932	2979	6	6034	0001	20
	9.776090								9.	786089						
I	6259							41						6361		
2	6429							42						6525		
3				6683				43						6688		
4				6852				44						6851		
5				7021				45		6906	0933	0960	0987	7014	7042	14
6	7106	7134	7162	7191	7219	7247	13	46		7069	7096	7123	7150	7177	7205	13
7	7275	7303	7331	7359	7388	7416	12	47		7232	7259	7286	7313	7340	7367	12
8	7444	7472	7500	7528	7556	7585	11	48		7395	7422	7449	7476	7503	7530	ΙI
9	7613	7641	7669	7697	7725	7753	10	49		7557	7585	7612	7639	7666	7693	10
0	9.777781	7810¦	7838	7866	7894	7922	9	50	9.	787720	7747	7774	7801	7829	7856	9
I	7950	7978	8006	8034	8062	8091	8	51		7883 8045	7910	7937	7964	7991	8018	8
2	8119						7	52		8045	8072	8099	8127	8154	8181	7
3	8287						6	53		8208	8235	8262	8289	8316	8343	6
4	8455						5	54		8370	8397	8424	8451	8478	8505	5
5	8624						4	55		8532	8559	8586	8613	8640	8667	4
6	8792	8820	8848l	8876	8904	8032	3	56		8604	8721	8748	8775	8802	8829	3
7	8060	8988	0016	9044	0072	0100	2	57						8964		2
8	8960 9128	0156	0183	0211	230	0267	ī	58		8100	0045	0072	0000	9126	o i 53	1
9	9295	0323	35T	0370	0407	0435	0	59		9180						o
4		50"			20"			- 7				40"		20"	10//	
-						10.	Min.								10	Min.
				Degr		,	11					f 52	- 0			
7 1		" 3"		5" 6')"	Ρ.	 Рач	§ 1" S	2" 3"		5" 6			911
	art 3 3 (6 9	11	14 17	20	23 2	26		r al	"\3	5 8	11	14 1	6 19	.22 2	25

	,			100	21 10		147 1	1	IANGE						
Min.		• ,		3 Deg				Min.				`	grees.		
	07	10"	20"	30"	40"	50"	_	II	0"	10"	20"	30"	40"	50"	-
	9.861261							11	9.877114	7158	7202	7246	7290	7333	59
2				1659				1 2	7577	7421	7403	7309	7552 7815	7850	57
3				2191				3	7003	7047	7000	8034	8078	8122	56
4				2456				4	8165	8200	8253	8297	8341	8384	55
5				2721				5					8603		
6	2854	2898	2943	2987	3031	3075	53	6					8866		
7				3252				7					9128		
8				3517				8					9391		
9	9.863915			3783				9	9.879741	0784	0828	0872	9653	0050	10
11				4313					9.880003						
12	4445	4490	4534	4578	4622	4666	47	12					0440		
13	4710	4755	4799	4843	4887	4931	46	13	0528	0571	0615	0659	0703	0746	46
14				5108				14					0965		
15				5373				15					1227		
16				5638 5903				16					1489		
17				6167				17					1751 2013		
19				6432				19					2275		
	9.866564							20	9.882363	2406	2450	2494	2537	2581	39
21				6961				21	2625	2668	2712	2756	2799	2843	38
22	7094	7138	7182	7226	7270	7314	37	22	2887	2930	2974	3018	3061	3105	37
23				7491				23	3148	3192	3236	3279	3323	3367	36
24	7623	7007	7711	7755	7799	7843	35	24					3585		
25 26				8019 8284				25 26					3847 4108		
27				8548				27					4370		
28				8813				28					4632		
29				9077				29					4893		
	9.869 20 9	9253	9297	9341	9385	9429	29		9.884986						
31	9473	9517	9561	9605	9649	9693	28	31					5416		
32				9869				32					5678		
34	9.870001			0397				33	5705	5809	677	5890	5939 6201	5983	20
35				0661				34	6288	6337	6375	6/10	6462	6506	2/
36				0925				36					6723		
37				1189				37	6811	6854	6898	6941	6985	7028	22
38				1453				38	7072	7115	7159	7202	7246	7289	21
39				1717				39	7333	7377	7420	7464	7507	7551	20
	9.871849								9.887594						
41				2244 2508				41					8029		
42 43				2771				42					8291 8552		
44	2003	2947	2001	3035	3070	3123	15	44					8813		
45	3167	3211	3255	3299	3342	3386	14	45					9074		
46	343o	3474	3518	3562	3606	365o	13	46	9161	9204	9248	9291	9334	9378	13
47	3694	3738	3781	3825	3869	3913	12	47	9421	9465	9508	9552	9595	9639	12
48	3957	4001	4045	4089	4133	4177	II	48	9682	9726	9769	9813	9856	9900	11
49				4352			í	49					.117		
51	9.874484	4020	4072 1835	4879	4039	4703	8	51	9.890204				0639		8
52	5010	5054	5008	5142	5186	5230	7	52	0725	0760	0812	0856	0899	00/3	
53				5405			6	53	c 986	1030	1073	1116	1160	1203	7 6
54	5537	558o	5624	5668	5712	5756	5	54	1247	1290	1334	1377	1421	1464	5
55	5800	5843	5887	5931	5975	6019	4	55	1507	1551	1594	1638	1681	1725	4
56	6063	6107	6150	6194	6238	6282	3	56	1768	1811	1855	1898	1942	1985	3
57	6326	6370	6413	6457	6501	6545	2	57					2202		2
58	6589						I	58	2289	2332	2376	2419	2463	2506	I
59	6852						0	59					2723		0
-	Go to	50"	40"	30"]	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
	Co-tai				J				Co-ta						
P . 1	Port / "	9'' 3''	-		" 7" 6 31		9" 40	Р.	$\operatorname{Part} \left\{ egin{array}{l} 1'' \\ 4 \end{array} \right.$	2" 3' 9 1:	_		3″ 7″ 26 31		9″ 39
	('	U 10	. 10	~~ ~	0 01	,00,	10		('1	0 10	, 11	* * *	-U UI	0.0	<i></i>

.5	51	ine of	38.1	Degre	es.			l a	Si	ne of	39]	Degre	es.		
Min	Ü	10"	20"	30"	40"	50"		Min	0′′	10"	20"	30"	40"	50"	-
0	9.789342							0	9.798872	8898	8924	8950	8976	9002	5
1	9504	9531	9557	9584	9611	9638	58	1	9028	9054	9080	9106	9132	9158	5
2	9665	9692	9719	9746	9773	9800	57	2	9184	9210	9236	9262	9287	9313	5
3						9961		3	9339	9305	9391	9417	9443	9469	5
4						.122		5	9495	9521	9347	9373	9599	9025	0
6	9.790149					0445		6	0806	0832	0858	9720	9754	9780	5
7	0/71	0/108	0525	0552	0570	0606	52	7		0087	9030	30	9910	9930	5
8	0632	0650	0686	0713	07/10	0767	5 T		9.800117	01/13	0160	0105	0220	02/6	5
9						0927		9	0272	0208	0324	0350	0376	0/101	5
	9.790954								9.800427	o453	0479	0505	0531	0556	1
11						1249		11	0582	0608	0634	0660	0686	0711	4
12	1275	1302	1329	1356	1382	1409	47	12	0737	0763	0789	0815	0840	0866	4
13	1436	1463	1489	1516	1543	1570	46	13	0892	0918	0944	0969	0995	1021	4
14						1730		14	1047	1073	1098	1124	1150	1176	4
15						1890		15	1201	1227	1253	1279	1305	1330	4.
16						2050		16	1356	1382	1408	1433	1459	1485	4
17						2210		17	1511	1536	1562	1588	1613	1639	4
18						2370		18	1665	1691	1716	1742	1768	1794	4
19	2397	2423	2450	2477	2503	2530	40	19	1819	1845	1871	1896	1922	1948	4
	9.792557	2383	2010	2030	2003	2090	39		9.801973						
21	2710	2743	2770	2790	2823	2849	38	21	2120	2100	2179	2200	2230	2230	3
22	2070 3035	3060	3080	3775	31/0	3009 3168	36	22 23	2202	2307	2333	2559	2384 2538	2410	3
24						3328		24					2692		
25						3487		25					2846		
26						3646		26					2999		
27	3673	3600	3726	3752	3770	3805	32	27	3050	3076	3102	3127	3153	3178	3
28	3832	3858	3885	3011	3038	3964	31	28					3306		
29	3001	4017	4044	4070	4007	4123	30	29					3459		
	9.794150	4176	4203	4229	4255	4282	20	30	9.803511	3 53 6	3562	3587	3613	3638	2
31						4441		31	3664	3689	3715	3740	3766	3791	2
32						4599		32	3817	3842	3868	3893	3919	3944	2
33	4626	4652	4678	4705	4731	4758	26	33	3970	3995	4021	4046	4072	4097	2
34						4916		34	4123	4148	4174	4199	4225	4250	2
35						5074		35					4377		
36	5101	5127	5154	5180	5206	5233	23	36					453o		
37	5259	5285	5312	5338	5364	5391	22	37					4683		
38						5549		38					4835		
39	5575	2001	5028	5054	5080	5707	20	39	4880	4912	4937	4902	4988	2013	2
	9.795733							1	9.805039	5004	5009	5115	5292	2100	I
41						6022		41					5444		
42						6180		42 43	5/05	5500	55/6	5577	5597	5600	1
43 44						6338 6495		44					5748		
45						6652		45					5900		
46						6810		46					6052		
47	6836	6862	6888	6014	6941	6067	12	47	6103	6128	6153	6170	6204	6220	I
48	6993	7019	7045	7072	7098	7124	II	48	6254	6280	63o5	633ó	6355	6381	I
49	7150	7176	7202	7220	7255	7281	10	49					6507		
	9.797307	7333	7359	7386	7412	7438	9	50	9.806557						
51	7464	7490	7516	7542	7569	7595	8	51					6810		
52	7621	7647	7673	7699	7725	7751	7	52					6961		
53	7777	7804	7830	7856	7882	7908	6	53	7011	7037	7062	7087	7112	7137	'
54	7934						5	54	7163	7188	7213	7238	7263	7288	1
55	8091	8117	8143	8169	8195	8221	4	55	7314	7339	7364	7389	7414	7439	1
56	8247						3	56					7565		
57	8403						2	57					7716		
	8716	85/0	2 60	8038	8822	8690	I	58	7700	7/91	1010	7000	7867 8017	80/0	
59	60"	50"				-	0	59	60"	50"	40"	30"	20"	10"	1
-			40"		20"	10"	Min.							10.	Min
\perp		sine o									of 50				1
	$\operatorname{Part} \left\{ \begin{array}{l} 1'' \\ 3 \end{array} \right\}$	2" 3"	4"	5″ €	" 7"	8"	9"	р	$\operatorname{Part} \left\{ \begin{array}{l} 1'' \\ 3 \end{array} \right.$	2" 3°	4"	5" (5" 7"	8"	9

Tangent of 3B Degrees.					11 O G	AR.	LIH	MII		LANGE	NIA					-0
1 3070 3114 3157 3200 3233 3027 304 2983 3027 504 1 8628 8971 8714 8528 8971 8714 8715	ď.	Tan	gent	of 38	B Deg	rees.			j.	Tan	gent	of 39	Deg	rees.	,	
1	Mi	0"	10"	20"	30"	40"	50"									
2 3331 33743417 3461 3564 3547 577 2 8886 8929 8972 9015 9058 101 157 3 351 3364 3678 3972 3 9673 3972 30 9273 3016 9359 564 4 3851 3364 3368 3981 4025 4068 55 4 4 4020 4455 4488 521 4526 4468 521 4526 452 4526 452 4526 452 4526 452 4526 452 4526 452 4526 452 452 452 452 452 452 452 452 452 452	O	9.892810	2853	2897	2940	2983	3027	59	0	9.908369	8412	8455	8498	8541	8584	59 .
3 3591 3634 368 3721 3764 3808 56 3		3070	3114	3157	3200	3244	3287	58	16							
3351 3364 3338 361 4625 4668 55 4 4668 56 471 475 4708 476 476 4868 4868 4675 4718 476 4865 4848 52 476 476 4865 4848 52 476 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4848 52 476 4865 4868 52 486 476 4865 4868 4868 4868 4968 523 5865 5869 49 10 9, 90, 50, 73 575 575 5862 5845 5889 48 11 120 1252 1205 1338 1381 1424 48 48 48 48 48 48 48										8886	8929	8972	9013	9008	9101	57
56 4312 4415 4458 4524 4251 4258 438 54 85 43 86 46 970 3974 69 789 189 18 145 458 458 458 458 458 458 458 458 458 4										9144	0445	0488	9273 0531	057/	0617	55
6 4372 4415 4458 4502 4454 5488 503	5									0660	0703	0746	9789	9832	9875	54
7		4372	4415	4458	4502	4545	4588	53	6	9918	9961	5	48	91	. 134	53
9	7	4632	4675	4718	4762	48o5	4848	52		9.910177	0220	0263	0306	0349	0392	52
10 9, 8,95412 5455 5499 5542 5588 5682 649 10 9, 910551 0994 1037 1080 1123 1166 49 125 125 5725 5725 56019 6662 6165 6149 47 12 1467 1510 1553 1596 1639 1682 47 13 6162 6235 6278 6322 6365 6468 45 14 1282 2205 2368 23111 214 2197 45 15 6712 6755 6798 6842 6885 6682 6684 45 2240 2283 2366 23111 214 2197 45 15 6712 6755 6798 6842 6885 6928 44 15 2240 2283 2366 23111 214 2197 45 16 6971 7015 7058 7017 7145 7707 41 18 7411 7334 7578 7621 7644 7707 41 18 7411 7334 7578 7621 7644 7707 41 18 7751 7794 7837 7881 7924 7907 40 18 7751 7794 7837 7881 7924 7907 40 18 22 2353 8573 8568 8659 8746 877 22 2404 2833 8373 3316 3359 3484 4846 32 22 2353 8573 8568 8659 8746 877 22 2404 2404 2405 3318 3375 3408 3443 3486 38 21 2408 2331 8357 8408 8443 8486 38 21 2408	8	4892	4935	4979	5022	5065	5109	51	8							
11	9	5152	5195	5239	55/2	5325	5369	50								
12		5672	5715	5750	5802	5845	5880	49								
13																
15		6192	6235	6278	6322	6365	6408	46) - 1	1725	1768	1810	1853	1896	1939	46
16 6971 7015 7058 87101 7145 7188 433 16 2498 2541 2584 2627 2670 2713 43 17 7231 7275 7318 7361 7404 7448 42 17 2566 2790 2842 2855 2928 2971 42 2766 2790 2842 2855 2928 2971 42 2766 2790 2842 2855 2928 2971 42 2766 2790 2842 2855 2928 2971 42 2756 2790 2842 2855 2928 2925 2855 2928 2855 2858 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2928 2855 2855		6452	6495	6538	6582	6625	6668	45								
17		6712	6755	6798	6842	6885	6928	44								
18	1	6971	7015	7058	7101	7145	7188	43	1 1	2498	2541	2584	2027	2670	2713	43
9		7231	7273	7578	7501	7404	7440	42 // T		301/	2799 3055	3100	31/3	2920 3185	3228	42
20	- 1	7491	770/	7837	7881	702/	7067	40	1	3271	331/	3357	3400	3443	3486	40
22 8530 8573 8616 8659 8703 8746 37 22 23 8876 8619 8659 8703 8746 37 22 24 404 4087 4130 4173 4216 4259 37 23 84 9049 19052 9135 9178 9222 9265 35 24 4560 4603 4645 4688 4731 4774 455 736 26 9568 9611 9654 9697 9741 9784 33 26 9568 9611 9654 9697 9741 9784 33 26 9568 9611 9654 9697 9741 9784 33 26 900087 0130 0173 0216 0259 0303 31 28 900087 0130 0173 0216 0259 0303 31 28 900085 0648 0692 0735 0778 0821 29 0346 0389 0432 0476 0519 0562 30 30 9.90665 0648 0692 0735 0778 0821 29 30 0346 0389 0432 0476 0519 0562 30 31 0864 0908 0951 0994 1037 1081 28 31 1383 1426 1469 1513 1556 1599 26 33 1383 1426 1469 1513 1556 1599 26 33 1383 1426 1469 1513 1556 1599 26 33 1383 1426 1469 1513 1556 1599 26 33 1383 1426 1469 1513 1556 1599 26 33 1397 1734 277 22 2765 2808 2851 2894 21 38 269 2722 2765 2808 2851 2894 21 38 269 2722 2765 2808 2851 2894 21 38 269 2722 2765 2808 2851 2894 21 38 313 453 434 387 346 3493 3542 3585 3628 3671 18 41 3453 4577 4620 4663 4707 44 4 4 4232 4275 239 3587 5408 4405 4448 15 44 4232 4275 4318 4362 4465 4448 15 44 4232 4275 4318 4362 4465 4448 15 44 4232 4275 4318 4362 4465 4448 15 44 4232 4275 4318 4362 4465 4448 15 44 4232 4275 4318 4362 4465 4448 15 44 526 5656 5659 5138 5181 5224 12 47 5008 5052 5055 5138 5181 5224	20	9.898010	8054	8097	8140	8183	8227	39	20	9.913520	3572	3615	3658	3701	3744	39
33		8270	8313	8357	8400	8443	8486	38	1 1	3787	383o	3873	3916	3959	4001	38
24 9049 9092 9135 9178 9222 2655 35 24 4560 4603 4645 4688 4731 4774 35 26 9568 9611 9654 9697 9741 9784 33 26 259 330 37 9827 9870 9914 9957 43 32 27 5332 5375 5418 5461 5504 5547 32 28 9.90087 9130 9173 9216 9259 9303 31 28 5590 5633 5675 5718 5761 5504 5547 32 29 0346 0389 0432 0476 0519 0562 30 29 0346 0389 0432 0476 0519 0562 30 30 9.90605 0648 0692 0735 0778 0821 29 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 31 0864 0988 0951 0994 1037 1081 28 1081 0994 0										4044	4087	4130	4173	4216	4259	37
25		8789	8832	8876	8919	8962	9005	36								
26	1	9049	9092	9135	9178	9222	9200	37		4900	4603	4045	4088	4731	4774	35
28 9,90087 0130 0173 0216 0259 0303 31 28 259 0346 0389 0432 0476 0519 0562 30 29 0346 0389 0432 0476 0519 0562 30 29 0366 0648 0692 0735 0778 0821 29 0310 0864 0908 0951 0994 1037 1081 28 31		0568	9331	0654	0607	07/1	078/	33	1 -1	5075	4000 5118	5161	5203	4909 52/6	5280	33
28 9.900087 0130 0173 0216 0259 0303 31 28 0346 0389 0432 0476 0519 0562 30 0360 0389 0432 0476 0519 0562 30 0364 0389 0432 0476 0519 0562 30 0364 0389 0432 0476 0519 0562 30 0364 0389 0432 0476 0519 0562 30 0364 0486 0498 0519 0441 0418 04185 0418 04185 0418 04185 0418 04185 0418 04185 0418 04		9827	9870	9014	9097	9/41	43	32	1 1							
29 0.3460389 0.432 0.476 0.519 0.562 30 30 9.90605 0.648 0.692 0.778 0.821 30 0.864 0.908 0.951 0.994 1.037 1.081 2.88 31 0.864 0.908 0.951 0.994 1.037 1.081 2.88 31 1.124 1.167 1.210 1.253 1.297 1.340 27 33 1.383 1.426 1.469 1.573 1.556 1.599 2.6 33 0.848 0.6662 0.		9.900087	ó13o	0173	0216	0259	0303	31		5590	5633	5675	5718	5761	5804	31
31										5847	5890	5933	5976	6019	6062	3o
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33									1 1	6362	6405	6448	6491	6533	602/	25
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35										7134	7177	7220	7262	7305	7348	25
36										7391	7434	7477	7520	7563	7605	24
38		2160	2204	2247	2290	2333	2376	23	36	7648	7691	7734	7777	7820	7863	23
39																
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43		3714	3758	3801	3844	3887	3030	17		0101	0234	9277	9320	0362	0405	17
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47 5008 5052 5095 5138 5181 5224 12 47 0476 0519 0562 0604 0647 0690 12 12 48 5267 5310 5353 5397 5440 5483 11 48 0733 0776 0819 0861 0904 0947 11 0990 1033 1075 1118 1161 1204 10 10 10 10 10 10 10		4491	4534	4577	4620	4663	4707	14								
48		4750	4793	4836	4879	4922	4965	13	1 1							
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54 6819 6862 6905 6948 6991 7034 5 54 2274 2316 2359 2402 2445 2488 5 7077 7120 7163 7207 7250 7293 4 55 2530 2573 2616 2659 2702 2744 4 4 5 56 7336 7379 7422 7465 7508 7513 3 56 2787 2830 2873 2915 2958 3001 3 7594 7637 7680 7723 7766 7809 2 57 3044 3087 3129 3172 3215 3258 2 3258 32		6302	6345	6388	643 ı	6474	6517	7		1760	1803	1846	1889	1931	1974	7
55										2017	2060	2103	2145	2188	2231	
56		0819	7120	0905	0948	0991	7054	0 1								
57 7594 7637 7680 7723 7766 7809 2 57 3644 3687 3129 3172 3215 3258 2 258 7853 7896 7939 7982 8025 8668 1 58 3300 3343 3386 3429 3471 3514 1 1 1 1 1 1 1 1 1		7336	7370	7422	7465	7508	7551	3								
58								1 1								
59 8111 8154 8197 8240 8283 8326 0 59 3557 3600 3642 3685 3728 3771 0 60" 50" 40" 30" 20" 10"	58	7853	7896	7939	7982	8025	8068	I	58	3300	3343	3386	3429	3471	3514	
Co-tangent of 51 Degrees.	59	8111	8154	8197	8240	8283	8326	0	59	3557		3642	3685	3728	3771	0
P. Part 1" 2" 3" 4" 5" 6" 7" 8" 9" P. Part 1" 2" 3" 4" 5" 6" 7" 8" 9"								ij								.si
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(4 9 13 17 22 26 30 35 39 1 3 17 21 26 30 34 39	P.	Part		-	- ,		_	- 1	P			_				
		{ 4	9 1	3 17	72 5	26 30	35	39		\ 4	9 1	3 17	21 5	26 30	34	39

Sine of 40 Degrees.	7					- G	AKI	1 11	191 1	CBIN	E 5.					
0 9.88867 Sog3 S118 S143 S168 S193 S91 1	ij	Si	ine of	40 I	Degre	es.			j.		Sine of	41]	Degre	es.		
1 8218 8243 8268 829 8416 846 840 457 2 733 7256 733 7355 735 735 735 735 735 735 735 73	Z	0"	10"	20"	30"	40"	50"		Z					I		
2 8368 8393 8419 844 8469 8494 57 2 7733 7258 7852 7360 7303 7354 57 38 519 854 8458 65 854 850 864 85	0								0	9.8169	3 6967	6991	7016	7040	7064	59
S	1								11	70	88 7112	7137	7161	7185	7209	58
4 8666 8664 8716 8746 8796 8794 55 4 7524 7548 7592 7596 7662 7644 55 5818 844 8866 8869 8994 9019 9044 9069 9044 9369 9044 9369 9044 9369 9044 9369 9044 9369 9044 9369 9044 9369 9044 9369 9044 9369 9344 9369 9344 9369 9344 9369 9419 9444 9469 9464 9468 9444 9469 9464 9468 9464 9464 9464 9464 9464 9469 9464 9469										723	7258	7282	7306	7330	7354	57
S819 8844 886 894 910 9044 906 9094 531 6 88 9094 901 9044 906 904 905 904 905 904 905 904 905 904 905 905 905 905 905 905 905 905 905 905										73	79 7403	7427	7431	7475	7499	56
6	1 5									75	8 7540	7572	7390	7020	7044	55
T			800/	0010	0044	0060	000/	53		78	3 7837	7862	7886	7703	7709	53
8	1	0110	0144	9169	9194	0210	0244	52	11	70	8 7082	8006	8030	8055	8070	52
9 9419 9444 9469 9494 9519 9544 95 8 9 943 918 943 919 944 113 88518 856 8584 869 8633 8657 48 8618 975 874 918 917 917 917 918 918 918 918 918 918 918 918 918 918	8									810	3 8127	8151	8175	8100	8223	51
1	9	9419	9444	9469	9494	9519	9544	50	9	824	7 8272	8296	8320	8344	8368	50
12	10	9.809569	9594	9619	9643	9668	9693	49	10	9.81836	2 8416	8440	8464	8488	8512	40
13 0.810017 0.042 0.067 0.092 0.117 0.142 46 13 0.167 0.191 0.167 0.167 0.191 0.167 0.		9718	9743	9768	9793	9818	9843	48	11	853	6 8560	8584	8609	8633	8657	48
14 o167 0191 o216 o24 lo266 o291 45 16 o460 o340 o340 o340 o450 o460 o460 o360 o460 o564 o580 o450 o564 o580 o450 o460	1	9868	9893	9918	9943	9967	9992	47	11 _	868	8705	8729	8753	8777	8801	47
15			1	1 1	٠.			1	11 .	889	5 8849	8873	8897	8921	8945	46
16									11 -	890	9 0993	9017	9041	9065	9089	45
17									II -	911	39137	9101	9193	9209	9233	44
18									!!	0/10	1 0/25	0440	0/23	0/07	0527	40
19	1 5								11 2	05/	5 0560	0503	0617	06/1	0665	11
20	1								19	968	99713	9737	9761	9785	9800	40
22	1 -	9 811061	1086	1110	1135	1160	1185	39	20	9.81983	2 9856	J9880	9904	9928	9952	39
22		1210	1234	1259	1284	1309	1334	38	21	997	$6 \dots$	24	48	72	96	38
24	22	1358	1383	1408	1433	1457	1482	37		9.82012	00143	0167	0191	0215	0239	37
25									ا ما	026	3 0287	0311	o335	0359	0382	36
26	1 4	1655	1680	1705	1730	1754	1779	35	1 21	040	6 0430	0454	0478	0502	0526	35
27	1								1 -1							
288	(1932	1977	2001	2020	2001	2076	33	í I							
230		2100	2123	2130	0300	2199	0350	32								
36 q.812544 2569 2594 2618 2643 2668 29 30 q.821265 1288 1312 1336 1360 1384 29 2869 2717 2742 2766 2791 2815 28 31 1407 1431 1455 1479 1502 1526 28 32 2888 3012 2037 3066 3086 3111 26 33 1693 1716 1740 1744 1746 1745 1740 1744 1746 1745 1740 1744 1748 1811 26 33 1333 3307 3381 3307 3381 3466 24 35 1977 2001 2025 2049 2072 2096 24 2337 3578 3602 3627 3661 3676 3700 22 37 2262 2286 2309 2333 2357 2381 2323 238 3725 3749 3774 3799 3823 3848 21 38 2404 2428 2452 2475 2499 2523 21 2144 2488 2452 2475 2499 2523 21 2414 2415 2414									1 1							
31									30	0.82126	5 1288	1312	1336	1360	1384	20
32										140	7 1431	1455	1479	1502	1526	28
33	32								32	155	0 1574	1598	1621	1645	1669	27
35	33	2988	3012	3037	3062	3086	3111	26	33	169	3 1716	1740	1764	1788	1811	26
36		3135	3160	3185	3209	3234	3258	25		183	5 1859	1883	1906	1930	1954	25
37	1 1															
38 3725 3749 3774 3799 3823 3848 21 38									1. 1							
39																
40 9.814019 4044 4068 4093 4117 4142 19 40 9.822688 2712 2736 2759 2783 2807 19 4166 4191 4215 4240 4264 4289 18 41 2830 2854 2878 2901 2925 2948 18 42 2972 2996 3019 3043 3067 3090 17 43 4460 4484 4509 4533 4558 4582 16 43 314 3137 3161 3185 3208 3332 16 44 4607 4631 4656 4680 4704 4729 15 44 3255 3279 3303 3326 3350 3373 15 455 4753 4778 4802 4827 4851 4876 14 45 3397 3421 3444 3468 3491 3515 14 45 4753 4778 4802 4827 4851 4876 14 45 3397 3421 3444 3468 3491 3515 14 475 5046 5071 5095 5120 5144 5168 12 47 3680 3704 3727 3751 3774 3798 12 48 5133 5217 5242 5266 5200 5315 11 48 3821 3845 3868 3892 3915 3399 11 5339 5364 5388 5412 5437 5461 10 49 3963 3986 4010 4033 4057 4080 10 50 9.815485 5510 5534 5558 5583 5607 9 50 9.824104 4127 4151 4174 4198 4221 9 50 9.815485 5510 5534 5558 5585 5895 778 5802 5826 5851 5875 5899 7 52 4386 4409 4433 4456 4480 4503 7538 5024 5948 5972 5996 6021 6045 6 53 4552 4550 4574 4557 4621 4644 6 6069 6094 6118 6142 6167 6191 5 54 4668 4691 4715 4738 4761 4785 5 6215 6240 6264 6288 6312 6337 4 55 4808 4832 4855 4879 4902 4926 4 5607 6531 6555 6579 6604 6628 2 57 5090 5113 5136 5160 5183 5207 2 5996 6021 6045 6 6 6361 6385 6409 6434 6458 6482 3 56 4949 4972 4996 5019 5043 5066 3 579 6507 6531 6555 6579 6604 6628 2 57 5090 5113 5136 5160 5183 5207 2 5996 6021 6045 6 53 4949 4972 4996 5019 5043 5066 3 579 6097 6091 6092 6044 6128 6079 6094									1 _ 1							
41																
42		4166	4101	4215	4240	4264	4280	18								
43	1 : 1	4313	4338	4362	4387	4411	4436	17	1 : 1							
44										311	4 3137	3161	3185	3208	3232	16
45	1	4607	4631	4656	468o	4704	4729	15	44	325	5 3279	33o3	3326	335o	3373	15
47		4753	4778	4802	4827	4851	4876	14								
48	1 : 1	4900	4924	4949	4973	4998	5022	13		353	9 3562	3586	3609	3633	3656	13
49										368	0 3704	3727	3751	3774	3798	12
50 0.815485 5510 5534 5558 5583 5607 9 509.824104 4127 4151 4174 4198 4221 9 51 5632 5656 5680 5705 5729 5753 8 51 4245 4268 4292 4315 4339 4362 8 52 5778 5802 5826 5851 5875 5899 7 52 4386 4409 4433 4456 4480 4503 7 52 4564 5948 5972 5996 6021 6045 6 53 4527 4550 4574 4597 4621 4644 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		5193	5361	5300	5/	5/2-	5/6-	II		362 362	3 3086	6070	1032	3915	1939	II
51 5632 5656 5680 5705 5729 5753 8 51 4245 4268 4292 4315 4339 4362 8 52 5778 5802 5826 5851 5859 5859 7 52 4386 4409 4433 4456 4480 4503 7 53 5924 5948 5972 596 6021 6045 6 6 53 4527 4550 4574 44597 4621 4644 6 54 6069 6094 6118 6142 6167 6191 5 54 4668 4691 4715 478 4761 4785 5 55 6215 6240 6288 6312 6337 4 55 4888 4832 4852 4879 4902 4926 4 56 6361 6385 6409 6434 6458 6482 3 56 4949 4972 4992 5019 5043 5666 3 5090 5113 5136 5160	49	0 875/85	55.0	552%	5550	5583	5607			0.80410	1/1100	4010	4033 /15/	4007	1201	
52 5778 5802 5826 5851 5875 5899 7 52 4386 4409 4433 4456 4486 4503 7 532 4504 5972 5996 6021 6045 6 53 4527 4550 4574 4597 4621 4644 6 6669 6094 6118 6142 6167 6191 5 54 4668 4691 4715 4738 4761 4785 5 56 6215 6240 6264 6288 6312 6337 4 55 4808 4832 4855 4879 4902 4926 5019 5043 5066 3 56 609 6631 6555 6579 6604 6628 2 57 5090 5113 5136 5160 5183 5207 2 5090 5113 5136 5160 5183										y.02410	5 4268	4202	43 T 5	4330	4362	8
53								- 1		438	6 4400	4433	4456	4480	4503	
54 6069 6094 6118 6142 6167 6191 5 54 4668 4691 4715 4738 4761 4785 5 6215 6240 6264 6288 6312 6337 4 55 4808 4832 4855 4879 4902 4926 4 5 5 6507 6531 6555 6579 6604 6628 2 57 5000 5113 5136 5160 5183 5207 2 5 6652 6676 6701 6725 6749 6773 1 58 6798 6822 6846 6870 6894 6919 0 59 5371 5394 5417 5441 5464 5488 0 6000 5000 5000 5000 5000 5000 5000										452	7 4550	4574	4597	4621	4644	6
55		60 6 0	6094	6118	6142	6167	6191			466	8 4691	4715	4738	4761	4785	5
56 6361 6385 6409 6434 6458 6482 3 56 4949 4972 4996 5019 5043 5066 3 57 6507 6531 6555 6579 6604 6628 2 57 5090 5113 5136 5160 5183 5207 2 58 6652 6676 6701 6725 6749 6773 1 58 5230 5254 5277 5300 5324 5347 1 5404 5464 5488 0 60" 50" 40" 30" 20" 10" 2 60" 50" 40" 30" 20" 10" 2 2		6215	6240	6264	6288	6312	6337			480	8 4832	4855	4879	4902	4926	4
58 6652 6676 6701 6725 6749 6773 1 58 5230 5254 5277 5300 5324 5347 1 546 5488 0 6798 6822 6846 6870 6894 6919 0 59 5371 5394 5417 5441 5464 5488 0 60" 50" 40" 30" 20" 10" 10" 10 10 10 10 10		6361	6385	6409	6434	6458	6482	3		494	9 4972	4996	5019	5043	5066	3
59 6798 6822 6846 6870 6894 6919 0 59 5371 5394 5417 5441 5464 5488 0 60" 50" 40" 30" 20" 10" 50" 40" 30" 20" 10" Co-sine of 49 Degrees.								1		509	0 2113	5136	5160	5183	5207	
60" 50" 40" 30" 20" 10" Co-sine of 49 Degrees. E Co-sine of 48 Degrees.								- 1		523	0 5254	5277	2300	5324	5.49	
Co-sine of 49 Degrees.	29					····		0	39							-
of the of the Begrees.							10"	ġ			سنبا	ليسيبا			10"	i i
P. Part \ \ \begin{pmatrix} 1'' & 2'' & 3'' & 4'' & 5'' & 6'' & 7'' & 8'' & 9'' \ 2 & 5 & 7 & 10 & 12 & 15 & 17 & 20 & 22 \end{pmatrix} \] P. Part \ \ \begin{pmatrix} 1'' & 2'' & 3'' & 4'' & 5'' & 6'' & 7'' & 8'' & 9'' \ 2 & 5 & 7 & 10 & 12 & 14 & 17 & 19 & 21 \end{pmatrix}																
(2 5 7 10 12 15 17 20 22 2 5 7 10 12 14 17 19 21	P.	$Part \left\{ \begin{array}{ll} 1'' & 5 \\ 2 & \end{array} \right.$		_		•	-		Р.							
	L	(2	J 7	10	12 1	ə 17	20 5	22			ə 7	10	12 1	4 1/	19	21

Min.	Tan	gent	of 40	Deg	rees.			Min.	Tar	gent		Deg	rees.		
	0"	10"	20"	30"	40"	50"			0"	10"	20"	30"	40"	50"	
0	9.923814							0	9.939163	9206	9248	9291	9333	9376	5
I				4198				I	9418	9461	9503	9546	9588	9531	58
2	4327	4369	4412	4455	4498	4540	57	2	9673	9716	9758	9801	9843	9886	5
3	4583	4626	4669	4711	4754	4797	56	3	9928	9971	13	56	98	.141	5
4	4840	4882	4925	4968	2011	5053	55		9.940183						
5				5224				5		0481					
6				5481				6		0736					
7	5009	5002	2094	5737	2780	5822	52	7		0991					
8				5993				8		1246					
9				6250				9		1501					
- 1	9.926378			6762					9.941713	2011					
11	6800	6033	6076	7019	000J	0040	40	11		2266					
3	71/7	7180	7970	7275	7001	7104	46	13		2521					
14	7/03	7//6	7/88	7531	757/	7616	45	14		2776					1 :
5	7400	7702	7400	7787	7830	7870	4.6	15		3030					
6	7015	7058	8001	8043	8086	8120	43	16		3285					
7				8299				17		3540					
8				8555				18		3795					
19				8812				19		4050					
	9.928940								9.944262						
21	0106	0238	9281	9324	366	0400	38	21		4559					
22	9452	9494	9537	9580	9622	9665	37	22		4814					
23	9708	0750	9793	9836	9878	0021	36	23		5069					
24	9964	6	49	92	. 134	.177	35	24	5281	5323	5366	5408	545 I	5493	3
25	9.930220							25	5535	5578	5620	5663	5705	5748	3
26				0603				26		5832					
27				0859				27	6045	6087	6130	6172	6214	6257	3
8				1115				28		6342					
29				1371				29		6596					
30	9.931499	1542	1584	1627	1669	1712	20		9.946808						
31	1755	1797	1840	1883	1925	1968	28	31		7105					
32				2138				32		7360					
33	2266	2309	2351	2394	2437	2479	26	33		7614					
34	2522	2565	2607	265o	2692	2735	25	34	7827	7869	7911	7954	7096	8039	2
35¦	2778	2820	2863	2906	2948	2991	24	35		8123					
36	3033	3076	3119	3161	3204	3246	23	36	8335	8378	8420	8463	8505	8548	2
37	3289	3332	3374	3417	3459	3502	22	37	8590	8632	8675	8717	8760	8802	2
38	3545	3587	363o	3672	3715	3758	21	38		8887					
39	3800	3843	3885	3928	3971	4013	20	39		9141					
	9.934056	4098	4141	4184	4226	4269	19	40	9.949353	9396	9438	9480	9 5 23	9565	I
41	4311	4354	4397	4439	4482	4524	18	41	9608	9650	9692	9735	9777	9819	I
42	4567	4610	4652	4695	4737	4780	17	42	9862	9904	9947	9989	31	74	1
43	4822	4865	4908	4950	4993	5035	16		9.950116						
44				5206				44		0413					
45	2333	5570	3419	5461	2204	2546	14	45		0667					
46	5589	JUJ2 500-	5074	5717	2729	3802 6-F	13	46		0921					
47	5044	5007	3930	5972	6015	62-0	12	47		1176					
48	0100	63.0	644-	6227	65-5	6560	II	48		1430					
49	9.936611	6652	6606	6483	6-0-	6803	10	49		1684					
51	6866	6000	605	6994	0.036	0023	9		9.951896	1938	1901	2023	2000	2100	
52	7101	716/	7906	7249	7030	7079	8	51	2130	2193	0/9	2277	2520	2502	
53	7377	7/10	7/160	7504	7291	7580	7	5 ₂ 5 ₃		2447 2701					
54	7632	7674	7717	7759	7800	7845	5	54		2955					
55	7887	7030	7070	8015	805	8100	4	55	376-	3209	3050	3040	3336	3380	
56	81/10	8185	8225	8270	8310	8355	3	56		3463					
57	8308	8/1/0	8/83	8525	8568	8610	2	57	36-5	3718	3560	3800	38/5	388-	
58	8653	8605	8738	8780	8803	8865	1	58		3972					
50	8008	8050	8003	9035	0078	0121	0	59		4226					
_	60"	50"	40"				-	139					· · · · · · · · · · · · · · · · · · ·		-
					20"	10"	Min.		60"	50"	40"	30"	20"	10"	١
D.	Co-ta	ngen 2" 3'			egrees		9"		(1//	ingen 2" 3			$\frac{\text{egree}}{6''}$		9
г.	Part $\begin{cases} 1 \\ 4 \end{cases}$	9 13		21 9			38	P.	Part \ \ \ \ \ \ 4	8 1	_		25 30	-	3

4	Si	ne of	42 I					Γ. Ι	Si		43]	Degre	es.		
Min	0"	10"	20"	30"	40"	50"		Min	0"	. 10"	20"	30"	40"	50"	
0	9.825511							0	9.833783	3806	3828	3851	3874	3896	59
1	5651	5875	5698 5838	5721 5861	5885	5008	58	I	3919	3941	3964	3986	4009	4032 4167	58
3			5978					3	4180	4212	1231	1257	1280	4302	56
4			6118					4	4325	4347	4370	4392	4415	4437	55
5			6258					5	4 460	4482	4505	4527	4550	4572	54
6			6398					6	4595	4617	4640	4662	4685	4707	53
7 8			6538 6677					8	473o 4865	4732	4770	4797	4020	4842	51
9			6817					9						5112	
	9.826910								9.835134						
11			7096					11						5381	
12			7235					12						5515 5 650	
13 14			7374 7514					13						5784	
15			7653					15	5807	5820	5851	5874	5896	5918	44
16	774 5	7768	7792	7815	7838	7861	43	16						6653	
17	7884	7907	7931	7954	7977	8000	42	17						6187	
18			8069					18						6321 6455	
19	9.828301		8208					19	9.836477						
21	8439	8462	8485	8509	8532	8555	38	21						6722	
22	8578	8601	8624	8647	8670	8693	37	22	6745	6767	6789	6812	6834	6856	37
23			8762					23						6990	
24 25			8901					24						7123	
25 26			9039 9177					25 26	7270	7301	7324	73/6	7368	7257 7390	33
27	9269	9292	9315	9338	9361	9384	32	27	7412	7435	7457	7479	7501	7524	32
28	9407	9430	9453	9470	9499	9522	31	28	7546	7568	7590	7612	7635	7657	31
29	9545	9568	9591	9614	9637	9660	30	29	7679	7701	7723	7746	7768	7790	30
30	9.829683							31	9.837812	7054	7007	8012	803/	7923 8056	28
32	0050	0082	9867	28	51	74	27	32	8078	8100	8123	8145	8167	8189	27
	9.830097	0120	0142	0165	0188	0211	26	33						8322	
34	0234	0257	0280	0303	0326	0349	25	34	8344	8366	8388	8410	8433	8455	25
35			0417					35	8477	8499	8521	8543	8565	8587	24
36			0555					36 37						8720 8853	
38	0784	0807	0829	0852	0875	0803	21	38						8985	
39			0967					39	9007	0020	0051	9073	9095	9118	20
1 .	9.831058								9.839140	9162	9184	9206	9228	9250	19
41			1241					41						9382 9514	
42			1378					42						9646	
44			1651					44						9778	
45	1742	1765	1788	1811	1833	1856	14	45	9800	9822	9844	9866	9888	9910	14
46			1924					46	9932	9954	9976	9998	20	42	13
47	2015	2038	2197	2084	2100	2129	12		9.840064					0306	
48	2132	2311	2334	2356	2370	2402	10	48 49						0437	
50	9.832425	2447	2470	2493	2515	2538	9	50	9.840459	0481	0503	0525	0547	0569	9
51	2561	2584	2606	2629	2652	2674	8	51						0700	1
52	2697	2720	2742	2765	2788	2810	7	52						0832	
53	2833	2000	2878 3014	303	3060	3089		53 54	0034	1007	1020	1051	1079	0963	
55	3105	3128	3150	3173	3106	3218		55						1226	4
56	3241	3263	3286	3300	3331	3354	3	56	1247	1269	1291	1313	1335	1357	3
57	3377	3399	3422	3444	3467	3490	2	57	1378	1400	1422	1444	1466	1488	2
58	3512	43535	3557	3580	3603	3025	I	58						1619	
59	60"	5070	3693	3710	20"	10"	-	59	60"	50"	40"	30"	20"	10"	
			of 47		<u> </u>	10.	Min	-			of 46			1 20	Min.
-	1.11	2" 3			6" 7"	8"	9"	-	(1//	2" 3			6" 7'	′ 8″	9"
P.	Part \ 2	5 7	-		14 16	•	21	P.	Part 2		7 9		13 16		20
								Ш	`						

g	Tan	gent	of 42	2 Deg	rees.			Min.		Tar	igent	of 43	3 Deg	rees.		
Mh	0"	10"	20"	'	40"	50"				0"	10"	20"	30"	40"	50"	
0	9.954437	448o	4522	4564	4607	4649	59	0	9.	969656	9698	9740	9783	9825	9867	59
1	4691	4734	4776	4819	4861	4903	58	1		9909	9951	9994	36	78	.120	58
2				5073					9.	970162						
3	5/5/	5/42	5539	5327 5581	5603	5665	55	3 4							0627 0880	
5				5835				5		0009	0064	1007	10/90	TOOL	1133	54
6	5061	600/	60/6	6088	6131	6173	53	6		1175	1218	1260	1302	13/1/	1386	53
7	6215	6258	6300	6342	6385	6427	52	7		1420	1471	1513	1555	1507	1640	52
8				6596				8							1893	
9	6723	6766	6808	685o	6893	6935	50	9							2146	
ió	9.956977	7020	7062	7104	7146	7189	49		9.	972í88	2230	2273	2315	2357	2399	49
11	7231	7273	7316	7358	7400	7443	48	11							2652	
12	7485	7527	7570	7612	7654	7697	47	12							2905	
13				7866				13							3159	
14	7993	8035	8077	8120	8162	8204	45	14		3201	3243	3285	3327	3370	3412	45
15				8373				15							3665	
16				8627 8881				16							3918	
17				9135				17 18							4171	
- 1	9000	0304	0346	9389	0/31	0/73	41	1 1							4677	
20	9.959516	0558	0600	06/12	0685	0727	30	19	٥.	974720	1762	4804	4846	4888	4030	30
21	0760	0812	0854	9896	0038	0081	38	21	9.						5183	
	9.960023	0065	0108	0150	0102	0234	37	22		5226	5268	5310	5352	5394	5437	37
23	0277	0319	0361	0404	0446	0488	36	23		5479	5521	5563	5605	5647	5690	36
24				0657				24		5732	5774	5816	5858	5901	5943	35
25				0911				25							6196	
26				1165				26							6449	
27				1418				27							6702	
28				1672				28							6955	
29	1799	1841	1883	1926	1968	2010	30	29							7208	
31	9.962052								9.	977250	7292	7534	7377	7419	7401	29
32	2560	2540	2391	2433 2686	2475	2517	20	31 32		7303	7343	7307	7030	7072	7714	20
33				2940				33		8000	8051	8003	8135	8178	8220	26
34				3194				34		8262	8304	8346	8388	8/31	8473	25
35	3320	3363	3405	3447	3480	3532	24	35							8726	
36	3574	3616	3650	3701	3743	3785	23	36							8979	
37	3828	3870	3912	3954	3997	4039	22	37		9021	9063	9105	9147	9190	9232	22
38				4208				38		9274	9316	9358	9400	9442	9485	21
39				4461				39		9527	9569	9611	9653	9695	9738	20
	9.964588							40	9.	979780	9822	9864	9906	9948	9990	19
41				4968						980033						
42				5222				42							0496	
43				5475				43		0538	0381	0023	0005	0707	0749	16
44 45				5729 5982				44		0791	10034	10070	0918	10900	1002	13
46				6236				45							1508	
47				6489				47		1550	1502	1634	1677	1710	1761	12
48	6616	6658	6700	6742	6785	6827	ΙΙ	48		1803	1845	1887	1020	1072	2014	II
49	6869	6911	6954	6996	7038	7080	10	49	1	2056	2008	2140	2182	2224	2267	10
50	9.967123	7165	7207	7249	7291	7334	9			982309	2351	2393	2435	2477	2519	9
51	7376	7418	7460	7503	7545	7587	8	51		2562	2604	2646	2688	2730	2772	8
52	7629	7672	7714	7756	7798	7840	7	52	1	2814	2857	2899	2941	2983	3025	7
53	7883	7925	7967	8000	8052	8094	6	53		3067	3100	3152	3194	3236	3278	6
54	8136	8178	8220	8263	8305	18347	5	54		3320	3362	3404	3447	3489	3531	5
55				8516				55		3573	3615	3657	3099	3742	3784	4
56	8043	0000	0727	8769	0012	0004	3	56							4037	
57 58	8896	0938	0980	9023	9005	9107	2	57 58							4289	
-	9149	9192	9234	9276	9518	9300	I			4552	460-	14410	4438	4500	4542	I
59				9529		-	-	59	-						4795	0
	60"	50"	40"	30"	20"	10"	Min		-	60"	50"	40"	30"	20"	10"	Min.
	<u> </u>			17 D								t of				1
	n (1"	2" 3	" 4"	5"	6" 7"	′ 8″	9''	11		. (1"	2" 3	3" 4"	5"	6" 7	" 8"	9"

	Si	ine of	44	Degre			T	١.	- -	S	ine of	145	Dogra	,		1
Min	0"	10"	20"	30"	40"	50"	1	Mia.	-	-0" N	10"	20"	30"		50"	
0	9.841771	1793	1815	1837	1858	1880	59	0	9.	849485	9506	9527	9548	9569	9590	59
I				1967				I		9611	9632	9653	9674	9695	2716	58
3				2098				3		9730 086/	0885	9700	9801	9822 9948	9843	57
4	2294	2316	2337	2359	2381	2403	55	4		9990		32	153	74	95	55
5	2424	2446	2468	2490	2511	2533	54	5	9.	850116	0137	0158	0179	0200	0221	54
6				2620 2750				6	1	0242	0263	0284	0305	0326 0451	0347	53
7 8	2815	2837	2850	2880	2002	2024	51	8		0403	0514	0535	0556	0577	0508	5 t
9	2946	2967	2989	3011	3032	3054	50	9		0619	0640	0661	0682	0703	0724	50
	9.843076	3097	3119	3141	3162	3184	49	13	9.	850745						
11	3336	3357	3370	3271 3401	3422	3444	40	11		0070	1017	1038	1058	0954 1079	1100	48
13	3466	3487	3509	353o	3552	3574	46	13		1121	1142	1163	1184	1205	1226	46
14	3595	3617	3639	3660	3682	3703	45	14		1246	1267	1288	1309	1330	1351	45
15 16	3725	3747	3808	3 7 90 3919	30/1	3063	44	15 16		1372	1393	1413	1434	1455 1580	1476	44
17				4049				17	1	1622	1643	1664	1685	1.705	1726	43
18	4114	4135	4157	4178	4200	4222	41	18		1747	1768	1789	1810	183o	1851	41
19				4308				19						1955		
21	9.844372			4437				21	9.	851997				2080		
22				4696				22		2247	2267	2288	2309	2330	2350	37
23				4825				23	•	2371	2392	2413	2434	2454	2475	36
24 25				4954				24 25						2579		
26				5083 5211				26						2703 2828		
27	5276	5297	5319	5340	5362	5383	32	27		2869	2890	2911	2931	2952	2973	32
28	5405	5426	5447	5469	5490	5512	31	28						3676		
29 30	9.845662	5683	5705	5598	5019	5760	30	29 30	0.	3118 853242	3263	3283	3304	3201	3221	30
31	5790	5812	5833	5855	5876	5897	28	31	9.	3366	3387	3408	3428	3449	3470	28
32	5919	5940	5962	5983	6004	6026	27	32		3490	3511	3532	3552	3573	3594	27
33				6111				33		3614	3635	3655	3676	3697	3717	26
34 35	6304	6325	6346	6240 6368	638a	6410	24	35		3862	3883	3003	3024	3821 3944	3065	2/1
36	6432							36		3986	4006	4027	4047	4068	4089	23
37				6624				37						4192		
38 39				6752 6880				38 39						4315 4439		
40	9.846944	6965	6986	7008	7029	7050	19		9.	85448o						
41	7071	7093	7114	7135	7157	7178	18	41	•					4686		
42				7263				42						4809		
43 44	7454	7476	7407	7391 7518	7530	7561	15	43						4932 5055		
45	7582	7603	7624	7645	7667	7688	14	45		5096	5117	5137	5158	5178	5199	14
46	7709							46		5219	5240	5260	5281	5301	5322	13
47 48	7836 7964							47 48		5/65	5485	5506	5526	5424 5547	5567	12
49	8091	8112	8133	8154	8176	8197	10	49		5588	5608	5629	5649	5670	56go	10
50	9.848218	8239	8260	8282	8303	8324	9	50	9.8	355711	5731	5751	5772	5792	5813	9
51 52	8345 8472						8	51 52		5656	5056	5007	5895	5915	5935	8
53	85gg						7	53		6078	6000	6110	6140	6038 6160	6180	7
54	8726	8747	8768	8789	8810	883ı	5	54		6201	6221	6242	6262	6282	63o3	5
55	8852						4	55						6405		4
56 57	8979 9106	9000	9021	9042	9003	9085	3	56 57		6568	6588	6600	6620	6527 6649	6670	3
58	9232	9253	9274	9295	9316	9338	I	58						6771		I
59	9359	9380	9401	9422	9443	9464	0	59		6812	6832	6853	6873	6893	6914	0
-	60"	50"	40"	30"	20"	10"	Min.			60"	50"	40"	30"	20"	10"	Min.
				Degre		1	. 11				sine c					
P. I	Part / - "	3" 4 6	4'' 9		7" 3 15)" 19	Р.	Par	$t \begin{cases} 1'' \\ 2 \end{cases}$	2" 3" 4 6	′ 4″ 8	-	2 7"		9" 19
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1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 6 11 7 18 19 20 1 1 1 2 2 2 2 3	5090 5343 5596 6101 6354 6607 7112 9.987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	5132 5385 5638 5891 6143 6396 6649 6902 7154 7407 76913 8166 8418 8671 8924 9177 9429	5174 5427 5680 5933 6185 6438 6691 7197 7449 7702 7955 8208 8460 8713 8966	5216 5469 5722 5975 6228 6480 6733 6986 7239 7491 7744 7997 8250 8503 8755	5259 5511 5764 6017 6270 6523 6775 7028 7281 7534 7786 8039 8292	5301 5553 5806 6059 6312 6565 6817 7070 7323 7576 7829 8081	58 57 56 55 54 53 52 51 50 49	3 4 5 6 7 8	0505 0758 1011 1263 1516 1769 2021	0547 0800 1053 1305 1558 1811 2063 2316	0590 0842 1095 1348 1600 1853 2106 2358	0632 0884 1137 1390 1642 1895 2148	0674 0926 1179 1432 1684 1937 2190 2442	0716 0969 1221 1474 1727 1979 2232 2485	57 56 55 54 53 52 51 50
3 4 5 6 7 8 9 10 11 12 11 3 11 4 11 5 11 6 11 7 11 8 11 9 12 2 2 2 3	5596 5848 6101 6354 6607 6860 7112 9.987365 7618 78711 8123 8376 8629 8882 9134 9387 9440 9.989893	5638 5891 6143 6396 6649 6902 7154 7407 7660 7913 8166 8418 8671 8924 9177 9429	5680 5933 6185 6438 6691 6944 7197 7449 7702 7955 8208 8460 8713 8966	5722 5975 6228 6480 6733 6986 7239 7491 7744 7997 8250 8503 8755	5764 6017 6270 6523 6775 7028 7281 7534 7786 8039 8292	5806 6059 6312 6565 6817 7070 7323 7576 7829 8081	56 55 54 53 52 51 50 49	3 4 5 6 7 8	0758 1011 1263 1516 1769 2021	0800 1053 1305 1558 1811 2063 2316	0842 1095 1348 1600 1853 2106 2358	0884 1137 1390 1642 1895 2148	0926 1179 1432 1684 1937 2190 2442	0969 1221 1474 1727 1979 2232 2485	56 55 54 53 52 51 50
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5 6 7 8 9 10 11 11 12 13 11 14 15 16 11 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	6101 6354 6607 6860 7112 9.987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	6143 6396 6649 6902 7154 7407 7660 8166 8418 8671 8924 9177 9429	6185 6438 6691 6944 7197 7449 7702 7955 8208 8460 8713 8966	6228 6480 6733 6986 7239 7491 7744 7997 8250 8503 8755	6270 6523 6775 7028 7281 7534 7786 8039 8292	6312 6565 6817 7070 7323 7576 7829 8081	54 53 52 51 50 49	5 6 7 8	1263 1516 1769 2021 2274	1305 1558 1811 2063 2316	1348 1600 1853 2106 2358	1390 1642 1895 2148 2400	1432 1684 1937 2190 2442	1474 1727 1979 2232 2485	54 52 51 50
6 7 8 9 10 11 11 12 13 11 14 15 16 11 17 18 19 22 19 22 19 22 23 23 24 24 25 26 26 27 27 27 27 27 27 27 27 27 27 27 27 27	6354 6607 6860 7112 9.987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	6396 6649 6902 7154 7407 7660 7913 8166 8418 8924 9177 9429	6438 6691 6944 7197 7449 7702 7955 8208 8460 8713 8966	6480 6733 6986 7239 7491 7744 7997 8250 8503 8755	6523 6775 7028 7281 7534 7786 8039 8292	6565 6817 7070 7323 7576 7829 8081	53 52 51 50 49	6 7 8	1516 1769 2021 2274	1558 1811 2063 2316	1600 1853 2106 2358	1642 1895 2148 2400	1684 1937 2190 2442	1727 1979 2232 2485	53 52 51 50
7 8 9 110 111 112 113 114 115 116 117 118 119 119 122 122 122 123	6607 6860 7112 9.987365 7618 8123 8376 8629 8882 9134 9387 9640	6649 6902 7154 7407 7660 7913 8166 8418 8671 8924 9177 9429	6691 6944 7197 7449 7702 7955 8208 8460 8713 8966	6733 6986 7239 7491 7744 7997 8250 8503 8755	6775 7028 7281 7534 7786 8039 8292	6817 7070 7323 7576 7829 8081	52 51 50 49	7 8 9	1769 2021 2274	1811 2063 2316	1853 2106 2358	1895 2148 2400	1937 2190 2442	1979 2232 2485	52 51 50
8 9 110 111 112 113 114 115 116 117 118 119 122 122 122 123	6860 7112 9.987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	6902 7154 7407 7660 7913 8166 8418 8671 8924 9177 9429	6944 7197 7449 7702 7955 8208 8460 8713 8966	6986 7239 7491 7744 7997 8250 8503 8755	7028 7281 7534 7786 8039 8292	7070 7323 7576 7829 8081	51 50 49	8	2021 2274	2063 2316	2106 2358	2148 2400	2190 2442	2232 2485	51 50
9 110 111 112 113 114 115 116 117 118 119 120 121 122 122 123	7112 9.987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	7154 7407 7660 7913 8166 8418 8671 8924 9177 9429	7197 7449 7702 7955 8208 8460 8713 8966	7239 7491 7744 7997 8250 8503 8755	7281 7534 7786 8039 8292	7323 7576 7829 8081	50 49	9	2274	2316	2358	2400	2442	2485	50
10 11 11 12 13 14 15 16 11 17 11 18 19 20 21	9 987365 7618 7871 8123 8376 8629 8882 9134 9387 9640	7407 7660 7913 8166 8418 8671 8924 9177 9429	7449 7702 7955 8208 8460 8713 8966	7491 7744 7997 8250 8503 8755	7534 7786 8039 8292	7576 7829 8081	49	10							
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13 14 15 16 17 18 19 20 21 22 23	7871 8123 8376 8629 8882 9134 9387 9640	7913 8166 8418 8671 8924 9177 9429	7955 8208 8460 8713 8966	7997 8250 8503 8755	8039 8292	8081		11	2779	2821	2864	2906	2948	2990	48
14 15 16 17 18 19 20 21	8123 8376 8629 8882 9134 9387 9640 9.989893	8166 8418 8671 8924 9177 9429	8208 8460 8713 8966	8250 8503 8755	8292		47	12	3032	3074	3116	3158	3200	3243	47
15 16 17 18 19 20 21 22 23	8629 8882 9134 9387 9640 9.989893	8671 8924 9177 9429	8713 8966	8755	8545		46	13	3285	3327	336g	3411	3453	3495	46
16 17 18 19 20 21 22 23	8882 9134 9387 9640 9.989893	8924 9177 9429	8966	8755		8587	45	14				3664			
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18 19 20 21 22 23	9387 9640 9.989893	9429		9008	9050	9092	43	16				4169			
19 20 21 22 23	9640 9 . 989893	9429						17				4422			
20 21 22 23	9.989893	0680	9471	9913	0808	9999	41	18				4674 4927			
21 22 23	9.990145	0035	9/24	3/00	, 6T	9000	30	20	10.005053						
22	, ,,	0187	9711 0230	0272	031/	0356	38	21				5432			
- 1					0567			22				5685			
2/1					0819			23				5938			
					1072			24				6190			
25					1325			25				6443			
26					1577			26				6696			
27					1830			27				6949			
28					2083			28	7075	7117	7159	7201	7243	7285	31
29					2336			29	7328	7370	7412	7454	7490	7538	30
31	9.992420				2841			31	10.007580	7022	7004	7959	8001	8044	29
32					3094			32				8212			
33	3178	3220	3262	3304	3346	3388	26	33				8465			
34	3431	3473	3515	3557	3599	3641	25	34				8717			
35					3852			35				8970			
36					4104			36	9097	9139	9181	9223	ç265	9307	23
37	4189	4231	4273	4315	4357	4399	22	37	9349	9391	9433	9476	9518	9560	22
38					4610			38	9602	9644	9686	9728	9770	9813	21
39					4862			39				9981			
	9.994947								10.010107						
41	5/50	5/0/	5536	55-8	5368 5620	5663	18	41				0487			
43					5873			42				0739 0992			
44					6126			44				1245			
45					6378			45				1497			
46	6463	6505	6547	6580	6631	6673	13	46				1750			
47					6884			47				2003			
48					7136			48	2129	2171	2214	2256	2298	2340	11
49	7221	7263	7305	7347	7380	7431	10	49	2382	2424	2466	2509	2551	2593	10
50	9.99 7 473 7726	7515	7558	7600	7642	7684	9	50	10.012635	2677	2719	2761	2803	2846	9
51	7726	7768	7810	7852	7894	7937	8	51				3014			
52	7979	8021	8063	8105	8147	8189	7	52				3267			
53 54	823I	8506	8560	86.	8400	86-5	6	53	3393	3600	3477	3520	3002	395-	6 5
55					8652 8905			54 55				3772			
56	8080	0031	0021	0003	9158	0247	3	56	3099	1104	1936	4025 4278	4320	4360	3
57	09/19	028/	0326	0368	9410	0/53	2	57	4132	1/1/194	4/80	4531	1573	4615	2
58	0405	9537	0570	0621	9663	9705	I	58				4784			
59					9916			59				5036			
	60"	50"	40"	30"	20"	10"	-		60"	50"	40"	30"	20"	10"	1
	Co-ta	'		-	-		Min.		Co-ta	<u>'</u>					Min.
			" 4"		6" 7"		9"		(1// 0				7"		9"
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		no of	46.7	 Domin		A K 1 .	T	Π.			C 47	D			ī -
Min.	0,	ine of	20'	30"	40"	50"		Min	0"	ine of	20"	Degre 30"	es.	50"	
0	9.856934	6954	6975	6995	7015			0	9.864127	4147	4167	4186	4206	4226	59
I	7056	7076	7097	7117	7137	7158	58	1	4245	4265	4284	4304	4324	4343	58
3		7198						3	4363	4383	4402	4422	4441	4461 4579	57
4		7442						4	4598	4618	4637	4657	4676	4696	55
5	7543	7563	7584	7604	7624	7645	54	5	4716	4735	4755	4774	4794	4813	54
6		7685						6	4833	4853	4872	4892	4911	4931	53
7 8	7780	7807 7928	7827 7048	7047	7867	7888	52 51	8	4950 5068	4970	4990	5706	5029	5048 5165	52
9		8049						9	5185	5204	5224	5244	5263	5283	50
10	9.858151	81718	3191	8211	8231	8252	49	10	9.865302	5322	5341	5361	538o	5400	49
11		8292						11						5517	
13	8393 8514	8413 8 8534 8	3433	8575	8474	8494	47	12						5634	
14	8635	8655	3675	8606	8716	8736	45	13						5751 5867	
15		8776						15	5887	5906	5926	5945	5965	5984	44
16	8877	8897	3917	8937	8958	8978	43	16	6004	6023	6042	6062	6081	6101	43
17	8998	9018	9038	9058	9078	9098	42	17						6217	
18	0230	9139 9259	2270	0300	0320	03/0	41	18	6353	6373	6302	6412	6/31	6334 6450	41
20	9.859360	9380	3400	9420	9440	9460	39		9.866470	6480	6500	6528	6547	6567	39
21	9480	9501	9521	9541	9561	9581	38	21	6586	66o6	6625	6644	6664	6683	38
22	9601	9621	9641	9661	9681	9701	37	22						6800	
23 24	08/2	9741 9 9862 9	2882	9701	9002	9022	35	23 24	6035	605/	607/	6003	7013	6916 7032	35
25		9982						25						7148	
26	9.860082	0102	0122	0142	0162	0182	33	26	7167	7187	7206	7225	7245	7264	33
27		0222						27	7283	7303	7322	7341	7361	7380	32
28		0342					- 1	28	7399	7419	7438	7427	7470	7496 7612	31
29 30	9.860562							29 30	9.867631	7650	7660	7689	7708	7727	20
31	/	0702						31	7747	7766	7785	78o4	7824	7843	28
32		0822						32	7862	7882	790I	7920	7939	7959	27
33 34		1061						33 34						8074 8190	
35		1181						35	8200	8228	8247	8267	8286	8305	24
36		1300						36						8420	
37		1420						37						8536	
38		1539 1						38 39						8651 8766	
39 40	9.86:758	1658 1							9.868785						
41	1877	1897	1916	1936	1956	1976	18	41						8996	
42	// .1	2016					- 1	42						9111	
43		2135 2						43	9130	9149	9168	0303	9207	9226 9341	15
44		2372 2						44	9243 9360	9204	0308	9417	0436	9455	14
46	2471	2491 2	2511	2531	2551	2570	13	46	9474	9494	9513	9532	9551	9570	13
47	12590	26102	263o	2650	2669	2689	12	47	9589	9608	9627	9646	9665	9685	12
48	2709	2729 2	2748	2768	2788	2808	II	48	9704	9723	9742	9701	9780	9799	II
49 50	9.862946	2847 2 2066 2	2085	3005	2900 3025	30/15	9	49 50	9.869933	9052	9930	30.72	9094	9914	9
51	3064	3084 3	3104	3124	3143	3163	8	51	9.870047	0066	0085	0104	0123	0142	8
52	3183	3203 3	3222	3242	3262	3281	7	52	0161	0180	0199	0218	0238	0257	7
53	3301	3321 3	3341	3360	3380	3400	6	53 54		0295					-
54 55	3538	3439 3 3557 3	3577	3507	3616	3636		55		0409 0523					
56	3656	3675	3695	3715	3734	3754	3	56	0618	0637	0656	0675	0694	0713	3
57	3774	3793	3813	3833	3852	3872	2	57	0732	0751	0770	0789	0808	0827	2
58		3911					I	58	0846	0865	0884	0903	0922	0941	0
59	60"	4029 Z	4049	30"		10"	0	59	60"	0979 507	40"			1054	
		sine o				10"	Min.			sine				10	Min.
	(1//)	2" 3"	4"		7"	8"	9"			2" 3'			5" 7"	8'1	9"
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انے	Tans	zent «	of 46	Degr	rees.			i	Tan	gent	of 47	Deg	rees.		Γ
Min	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	1
0	10.015163	5205	5247	5289	5331	5373	59	0	10.030344	o386	0429	0471	0513	o555	5
1	5416	5458	5500	5542	5584	5626	58	I	0597	0640	0682	0724	0766	0808	5
2						5879		2		0893					
3	5921	5963	6006	6048	6090	6132	56	3		1146					
4						6385		4		1400					
5						6638		5		1653					
6						6891		6	1864	1906	1948	1991	2033	2075	5
7	6933	6975	7017	7059	7101	7143	52	7		2160					
8	7186	7228	7270	7312	7354	7396	51	8	2371	2413	2455	2497	2540	2582	5
9						7649		9		2666					
0	10.017691								10.032877						
1	7944	7986	8028	8071	8113	8155	48	11		3173					
2						8408		12	3384	3426	3409	3511	3553	3595	14
3						8661		13		3680					
4						8914		14		3933					
5	8930	8998	9040	9082	9124	9166	44	15		4187					
6	9209	9231	9293	9333	9377	9419	43	16		4440					
7						9672		17		4694					
8	9714	9757	9799	9041	9003	9925	41	18		4947					
9	9907	10	52	03/	.130	.178	20	19	10.035412	5201					
						0684				5708					
2						0937		21		5961					
3						1190		22 23		6215					
4						1443		24		6468					
5		1			~ ~ .	1696	1	25		6722					
6						1949		26		6975					
7						2202		27		7229					
8						2455		28	7//0	7483	7525	7567	7600	7652	13
9	2/07	2530	2581	2623	2666	2708	30	29		7736					
	10.022750								10.037948						
1						3214		31		8243					
2						3467		32		8497					
3						3720		33		8751					
4						3973		34		9004					
5						4226		35	0216	9258	0300	0343	0385	0/27	2
6						4479		36	9470	9512	9554	0506	0630	0681	2
7						4732		37		9766					
8						4985		38		19					
9						5238			10.040231						
ó	10.025280	5323	5365	5407	5440	540 i	ΙQ		10.040484						
1	5534	5576	5618	566o	5702	5745	18	41		0781					
2						5998		42		1034					
3						6251		43	1246	1288	13 30	1373	1415	1457	ı
4						6504		44	1500	1542	1584	1627	1669	1711	1
5						6757		45	1753	1796	1833	1880	1923	1965	1
6						7010		46		2050					
7	7052	7095	7137	7179	7221	7263	12	47		2303					
8	7305	7348	7390	7432	7474	7516	II		2515	2557	2600	2642	2684	2727	I
9	7559	7601	7643	7685	7727	7770	10	49	2769	2811	2854	2896	2938	2980	1
	10.027812	7854	7896	7938	7981	8023	9		10.043023						
1	8065	8107	8149	8192	8234	8276		51	3277	3319	3361	3404	3446	3488	
2	8318						7	52		3573					
3	8571						6	53	3785	3827	3869	3912	3954	3996	
4	8825	0007	9909	8951	8993	9036	5	54		4081					
5	9078	9120	9162	9204	9247	9289	4	55		4335					
5	9331	9373	9416	9458	9200	9542	3	56	4546	4589	4031	4073	4716	4758	
7	9584	9027	9009	9711	9753	9795	2	57	4800	4843	4885	4927	4970	5012	
8	9838	9000	9922	9904	6	49	1	58	5054	5097	2139	181C	5224	5266	
9	10.030091						0	59		5351					L
1	60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	
-	Co-tar	gent	of 43	3 Deg	grees.		Z		Co-tar	ngent	of 45	2 De_{l}	grees.		1
	D. (1" 2	<i>''</i> 3''	4''		7"	8" 5	9"					. '			1

Γ.		no of	18 1	Jagra						Sine	of /	19 I	James			
Min	0"	10"	20"	Degre	40"	507		Min	0"	10		20"	30"	40'	50"	
0	9.871073	1092	IIII	1130	1149	1168	59	0	9.8777	30 779	8 7	816	7835	7853	7871	59
1	1187	1206	1225	1244	1263	1282	58	I	78	90 799	8 7	926	7945	7963	7981	58
3	1301	1320	1339	1358	1377 1490	1500	56	3						8072 8182		
4	1528	1547	1566	1585	1604	1622	55	4						8292		
5					1717			5	83	28 832	16 8	365	8383	8401	8419	54
6					1830			6						8511		
8					1944 2057			8						8620 8729		
9	, , <u>, , , , , , , , , , , , , , , , , </u>		i - '	_	2170	1 1	I I	9						8838		
	9.872208							10	9.8788	75 889	38	911	8929	8948	8966	49
iı			1 -		2396		1	11						9057		
13					2509 2622			13	90	93 911	1 9	129 238	9148	9166 9275	9184	47
14					2735			14	03	1 032	20 0	347	9257	9384	9293	45
15					2847			15	94:	20 943	38 9	456	9474	9492	9511	44
16					2960			16	95:	29 954	79	565	9583	9601	9619	43
17					3073			17						9710		
18					3185 3298			18						9819 9927		
	9.873335	3354	3373	3391	3410	3429	39		9.8799							
21	3448	3466	3485	35o4	3522	354i	38	21	9.8800	72 000	0 0	108	0126	0144	0162	38
22					3635			22						0253		
23 24					3747 3859			23 24						0361 0469		
25					3971			25						0577		
26	4009	4027	4046	4065	4083	4102	33	26	06	:3 o63	3 I O	649	0667	0686	0704	33
27	4121	4139	4158	4177	4195	4214	32	27						0794		
28					4307 4419			28 29						0902 1010		
29 30	9.874456								9.8810							
31	4568	4586	4605	4624	4642	4661	28	31	11:	53 117	71 1	189	1207	1225	1243	28
32					4754			32						1333		
33					4866			33						1441 1548		
34					4977 5088			35						1656		
36					5200			36	160	2 171	OI	728	1746	1763	1781	23
37					5311			37						1871		
38					5422			38 39						1978 2086		
39	9.875571	5580	5608	5626	5534 5645	5663	10	40	9.8821							
41					5756			41	22	29 224	6 2	264	2282	2300	2318	18
42					5867			42						2407		
43					5978 6088			43 44						2514 2621		
44					6199			45						2728		
46	6236	6255	6273	6291	6310	6328	13	46	27	54 278	2 2	799	2817	2835	2853	13
47	6347	6365	6384	6402	6421	6439	12	47	28	71 288	8 2	906	2924	2942	2960	12
48	6457	6586	6605	6603	6531 6642	6660	II	48	29°	77 299 34 314	2 3	120	3137	3049 3155	3173	10
49 50	9.876678	6607	6715	6734	6752	6770	9	50	0.8831	320	0 3	226	3244	3262	3280	Q
51	6789	6807	6826	6844	6862	6881	8	51	320	7 331	:5 3	333	3351	3368	3386	8
52	6899	8196	6936	6954	6973	6991	7	52	34	o4 34:	22 3	439	3457	3475	3493	7
53	7010	7028	7046	7065	7083	7101	6 5	53						3581 3688		5
54 55	7120 7230	72/8	7267	7285	7193 7303	7322	4	55	37:	23 374	í1 3	759	3776	3794	3812	4
56	7340	7358	7377	7395	7413	7432	3	56	38:	29 384	17 3	865	3883	3900	3918	3
57	7450	7468	7487	7505	7523	7542	2	57	39	36 39	3	971	3989	4006	4024	2
58	7560	7578	7597	7615	7633	7652	1	58						4113 4219		0
59	7070 60″	7088	7707	7725	7743	7702	0	59	60"	50		40"	30"	20"	10"	
				Degi		10	Min.	,		o-sin				-		Min.
P	(1//	2" 3"	4"	5" (3" 7"		9"	P	Part $\begin{cases} 1' \\ \end{cases}$		3"	4"	-	6" 7"	-	9"
1.	Part 2	4 6	7	9 1	11 13	15	17		1411) 2	4	5	7	9 1	11 13	14	16

Min.	Tang	gent	of 48	Deg	rees.			Min.	Ta	ngent	of 49	Deg	rees.		
Z	0"	10"	20"	30"	40"	50"		M	0"	10%	20"	30"	40"	50"	
0	10.045563							0							
I						6028		I		92 1135					
2						6282		2		47 1390					
3						6537		3	10	02 1645 58 1900	1000	1730	1773	1013	55
5	6833	6875	6018	6060	7000	6791 7045	54	5	21	13 2155	2108	22/1	2283	2326	5/
6						7299		6		68 2411					
7						7553		7		23 2666					
8	7505	7638	7680	7723	7765	7807	51	8		79 2921					
9	7850	7892	7934	7977	8010	8062	50	9	31	34 3177	3219	3262	3304	3347	50
10	10.048104	8146	8189	8231	8273	8316	49	10	10.0633	39 3432	3475	3517	356o	3602	49
11						8570		11		45 3687					
12						8824		12	39	00 3943	3985	4028	4070	4113	47
13	8867	8909	8951	8994	9036	9079	46	13		56 4198					
14	9121	9163	9206	9248	9290	9333	45	14		1 4454					
15						9587		15	40	67 4709 22 4965	4702	4794	4037	4079	44
16	- 9029	9072	9714	9737	9799	9841	43	16		78 5220					
17	9004 10.050138					96		17	54	33 5476	5518	5567	5603	5646	42
19						0604		18	56	39 5731	577/	5816	5850	5002	40
	10.050647								10.0659						
21						1113		21		00 6242					
22						1368		22		55 6498					
23	1410	1452	1495	1537	158o	1622	36	23	67	1 6754	6796	6839	6881	6924	36
241	1665	1707	1749	1792	1834	1877	35	24		37 7009					
25						2131		25		22 7265					
26						2386		26		78 7521					
37						2640		27	77	34 7776	7819	7862	7904	7947	32
8						2895		28		0 8032					
30		2979	3022	3370	3361	3149	30	29	10.0685	45 8288					
31						3658		31		57 8800					
32						3913		32		3 9055					
351						4168		33		69 9311					
34	4210	4252	4205	4337	438o	4422	25	34	95	25 9567	9610	9652	9695	9738	25
55	4465	4507	4549	4592	4634	4677	24	35	97	80 9823	9866	9908	9951	9994	24
36						4931		36	10.0700						
37						5186		37		92 0335					
38						5441		38		48 0591					
39						5696		39		04 0847					
	10.055738								10.0710						
41						6205		41		16 1359					
42 43						6460 6715		42		73 1615 29 1871					
44						6970		44		85 2128					
45						7224		45		41 2384					
46	7267	7300	7352	7304	7437	7479	13	46		97 2640					
47						7734		47	28	53 2896	2939	2981	3024	3067	12
48						7989				10 3152					
49	8032	8074	8117	8159	8202	8244	10	49		66 3409					
	10.058287	8329	8372	8414	8456	8499	9		10.0736	22 3665	3708	3750	3793	3836	
51	8541	8584	8626	8669	8711	8754		51	38	78 3921	3964	4007	4049	4092	8
52					8966		7	52		35 4178					7
53 54					9221		6	53		g: 14434					6
54 55	9300	0604	9391	9434	9476	9519	5 4	54		48 4590 04 4947					5 4
56	0817	0850	0000	9009	9732	9774	3	56	49 51	60 5203	5246	5280	533+	5374	
57	10.060072	011/	015	0100	9907	028/	2	57	5/	17 5460	5500	55/5	5588	563	2
58	0327	0360	0/12	0454	0407	0539		58		73 5716					
59	0582	0624	0667	0700	0752	0704		159		30 5973					
-	60"	50"	40"		20"	10"		-9	60"	50"	40"		207	10"	-
	Ce-ta		-		'		Min.			tangen					Min.
	(1// 6	2" 3"			" 7"		9"		r (1"	2" 3'			7/1		9"
Ρ.	Part / "	2" 3" 8 13	_	21 2			38	F.	Fart \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	9 • 13			i 30	-	38
						`	1								

	•					106	ARI	1 .1	177 1	COINE	4 5.					
-		l Si	ne of	50 1	legre	AG			1	Si	ne of	51 I	Degre	OS.		
- 1	T.						FOU		Min	0"						
	_	- J		20'	30"	40"	50"				10"	20"	30"	40"	50"	
-	0								0	9.890503	0520	0537	0554	0571	0588	59
1	Ţ			4395					I	0605	0622	0639	0656	0673	0690	58
-	2			4501					2	2707	0724	0741	0758	0775	0792	57
,	3			4607					3	0809	0826	0843	0860	0877	0894	56
1	4	4677	4695	4713	4730	4748	4766	55	4	0911	0928	0945	0962	0979	0996	55
-	5			4818					5						1098	
	6			4924					6	1115	1132	1149	11166	1183	1200	53
-	7			5030					7	1217	1234	1251	1268	1285	1302	52
1	8	5100	5118	5135	5153	5170	5188	5 r	8	1319	1336	1353	1370	1387	1404	51
- 1	9			5241					9	1421	1438	1455	1472	1489	1506	50
	10	9.885311							10	9.891523						
1	11	5416	5434	5451	5469	5486	5504	48	11						1709	
- 1	12	5522	5539	5557	5574	5592	5609	47	12	1726	1743	1760	1777	1794	1810	47
-	13			5662					13	1827	1844	1861	1878	1895	1912	46
	14	5732	5749	5767	5784	5802	5819	45	14	1929	1946	1963	1980	1996	2013	45
J	15			5872					15	2030	2047	2064	2081	2098	2115	44
1	16	5942	5960	5977	5995	6012	6030	43	16	2132	2149	2165	2182	2199	2216	43
-	17	6047	6065	6082	6099	6117	6134	42	17	2233	2250	2267	2284	2300	2317	42
-	18	6152	6169	6187	6204	6222	6239	41	18	2334	2351	2368	2385	2402	2419	41
1	19	6257	6274	6292	6309	6327	6344	40	19						2520	
	20	9.886362							20	9.892536	2553	2570	2587	2604	2621	39
	2 I	6466	6484	6501	6519	6536	6554	38	21						2722	
30	22			6606					22	2739	2755	2772	2789	2806	2823	37
1	23	6676	6693	6710	6728	6745	6763	36	23						2924	
-	24	6780	6798	6815	6832	685o	6867	35	24	2940	2957	2974	2991	3008	3024	35
ı	25	6885	6902	6919	6937	6954	6972	34	25	3041	3058	3075	3092	3108	3125	34
1	56	6989	7006	7024	7041	7059	7076	33	26						3226	
- [27			7128					27						3327	
١	28	7198	7215	7232	7250	7267	7285	31	28	3343	3300	3377	3394	3410	3427	31
	29	7302	7319	7337	7334	7371	7389	30	29	3444	3401	3477	3494	3311	3528	30
-		9.887406	7423	7441	7430	7470	7493	29		9.893544						
-	3 r			7545					31						3728	
-7	32			7649					32	3745	2960	3779	3793	2012	3829	27
1	33	7718	7730	7753	7770	7707	7000	20	33	3040	3063	3079	3090	3912	3929	20
	34	7022	7039	7857	7074	7091	8010	0/	34	4046	4063	4000	4006	4013	4029 4130	0/
	35			7961 8064					36	4746	4163	4180	4106	4113	4230	03
	36			8168					37	4140	4263	4280	4206	/313	433o	20
1	37 38			8272					38						4430	
- 1	3o			8375					39						453o	
-		9.888444								9.894546	4563	4580	4506	4613	4620	10
1	41			8582					41						4729	
-	42			8686					42						4829	
	43			8789					43						4929	
	44	8858							44	4045	4962	4970	4995	5012	5028	15
1	45	8961	8978	8006	9013	9030	9047	14	45	5645	5062	5078	5005	5111	5128	14
	46	9064	9082	9000	9116	9133	9150	13	46	5145	5161	5178	5194	5211	5227	13
1	47	9168	9185	9202	9210	9236	9253	12	47	5244	5261	5277	5294	5310	5327	12
1	48	9271	9288	9305	9322	9339	g356	II	48	5343	536o	5377	5393	5410	5426	II
1	49	9374	9391	9408	9425	9442	9459	10	49	5443	5459	5476	5493	5509	5526	10
	50	9.889477	9494	9511	9528	9545	9562	9	50	9.895542	5559	5575	5592	5608	5625	9
-	51	9579	9597	9614	963 I	9648	9665	8	51	5641	5658	5675	5691	5708	5724	8
-	52	9682	9699	9716	9734	9751	9768	7	52	5741	5757	5774	5790	5807	5823	7
Ì	53	9785	9802	9819	9836	9853	9871	6	53				5889			6
1	54	9888	9905	9922	9939	9956	9973	5	54				5988			5
1	55	9990	• • • 7	25	42	59	76	4	55				6087			4
	56	9 890093	0110	0127	0144	0161	0178	3	56				6186			3
	57	0195	0212	0230	0247	0264	0281	2	57	6236	0252	0209	6285	0302	6/-	2
	58	0298						I	58				6384			I
1	59	0400						0	59				6483			0
1		60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
i				of 39		ces.							Deg			
Ī	р	Part / -	2" 3"			7"		9"	р	Part 7	2" 3			6" 7"		9"
l	1.	1 art { 2	3 5	7	9 1	0 12	14	16	١.	1 at { 2	3 5	7	8	10 12	13	15

-	Tan	gent.	of 50	Degr	rees.			ď	Tans	rent	of 51	Deg	rees.		
Min.	0"	10″	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	
								1	10.091631						
1 2				6571 7828				1 2					2061 2320		
3	6956	6999	7042	7085	7127	7170	56	3	2406	2449	2492	2535	2578	2621	56
4	7213	7256	7298	7341	7384	7427	55	4					2837		
5 6	7470	7512	7333	7598 7855	7807	7084	53	5					3095 3354		
7	7983	8026	8069	8111	8154	8197	52	7					3612		
8	8240	8283	8325	8368	8411	8454	51	8	3698	3741	3784	3828	3871	3914	5 1
9	8497 10.078753			8625				9	3957 10.094215				4129		
11				9139				11					4647		
12	9267	9310	9353	9396	9438	9481	47	12	4733	4776	4819	4862	4905	4948	47
13				9652				13					5164		
14	9781			9909				15					5423 5682		
16	0295	0338	0381	0423	0466	0500	43	16					5940		
17	0552	0595	o638	0680	0723	0766	42	17	6027	6070	6113	6156	6199	6242	42
18				0937				18					6458		
20	1000 10.081323			1195				19	10.096803				6717		
21	1580	1623	1666	1709	1752	1704	38	21	7062	7106	7140	7102	7235	7278	38
22	1837	1880	1923	1966	2009	2052	37	22	7321	7365	7408	7451	7494	7537	37
23				2223				23	7580	7624	7667	7710	7753	7796	36
24 25				2480 2738				24 25					8012 8271		
26				2995				26					8531		
27	3123	3166	3209	3252	3295	3338	32	27	8617	866o	8703	8747	8790	8833	32
28	3381	3424	3467	3509	3552	3595	31	28	8876	8919	8963	9006	9049	9092	31
29	3638 10. 0 83896			3767				29	9136	9179	9222	9205	9308	9352	30
31				4282				31					9827		
32	4410	4453	4496	4539	4582	4625	27	32	9913	9957		43	86	. 130	27
33	4668	4711	4754	4797	4839	4882	26		10.100173						
34 35	4925 5183	5226	5260	5054 5312	5355	5307	25	34					o6o5 o865		
36				5569				36					1124		
37				5827				37					1384		
38				6084				38					1643		
39 //0	10.086471			6600				39	1730				1903		
41				6857				41	2249	2293	2336	2379	2422	2466	18
42	6986	7029	7072	7115	7158	7201	17	42	2509	2552	2596	2639	2682	2725	17
43	7244	7287	7330	7373	7416	7459	16	43	2769	2812	2855	2899	2942	2985	16
44 45	7760	7803	7846	7631 7889	7074	7075	1/1	44					3202 3462		
46	8018	8061	8104	8147	8190	8232	13	46	3548	3592	3635	3678	3722	3765	13
47	8275	8318	8361	8404	8447	8490	12	47	3808	385 r	3895	3938	3981	4025	12
48	8533	883/	88	8662	8705	8748	II	48	4068	4111	4155	4198	4241 4501	4285	II
49 50	10.080040	0002	0135	8920	0221	0264	0	49 50	4528 10.104588	4571 4631	4413	4450	4761	4805	1
51	9307	9350	9393	9436	9479	9522	8	51	4848	4891	4935	4978	5021	5065	8
52	9565	9608	9651	9436 9694 9952	9737	9780	7	52	5108	5152	5195	5238	5282	5325	7
53	9823 10.090082	9866	9909	9952	9995	39	6 5	53 54	5368	56-6	5455	5498	5542	5585	6
55	o3/in	0383	0426	0469	0512	0297	4	55					5802 6062		
56	°0598	0641	0684	0727	0770	0813		56	6149	6192	6236	6279	6322	6366	3
57	o856	0899	0942	0985	1028	1071	2	57	6409	6453	6496	6539	6583	6626	2
58 50				1243			I	58					6843		
59	60"	50"	40"	30"	20"	10"		59	60"	50"	7017	7000	7103	7147	
	Co-tai			-			Min.		Co-tai			1			Min.
. p	Part \$ 1" 5	2" 3"	4"	5" 6	" 7"		9"	D	(1// 0				7"		9"
	1 art { 4	9 13	17	21 2	6 30	34	39	r.		9 13	17	22 2	6 30	35	39

ď	Si	ine of	52	Degre	es.		Π	d		s	ine o	f 53	Degr	ees		
Min	0"	10"	20"	30"	40"	50"		Min		0"	10"	20"	30"	40"	50"	
- 1	9.896532							0	9.9	02349	2364	2380	2396	2412	2428	59
2				6680 6779				I		2444	2460	2475	2491	2507 2602	2523	58
3				6877				3		263/	2650	2666	2681	2697	2018	56
4	6926	6943	6959	6976	6992	7009	55	4		2729	2745	2761	2776	2792	2808	55
5	7025	7041	7058	7074	7090	7107	54	5		2824	2840	2856	2871	2887	2003	54
6	7123	7140	7156	7172	7189	7205	53	6		2919	2935	2950	2966	2982	2998	53
7 8	7222	7236	7234	7271 7369	7207	7303	5 r	8		3014	3029	3045	3001	3077 3171	3093	52
9	7418	7434	7451	7467	7483	7500	50	9		3203	3210	3235	3250	3266	3282	50
	9.897516	7533	7549	7565	7582	7598	49	10	9.9	03298	3313	3329	3345	336 I	3377	49
11	7614	7631	7647	7663	768o	7696	48	11		3392	3408	3424	3440	3455	3471	48
12	7712	7729	7745	7761	7778	7794	47	12		3487	3503	3518	3534	3550	3566	47
13	7008	702/	7043	7859 7957	7070	7000	40 45	13		3676	3601	3013	3029	3644 3739	3000	46
15	8006	8022	8030	8055	8071	8088	44	15						3833		
16	8104	8120	8136	8153	8169	8185	43	16						3927		
17				8250				17						4021		
18				8348				18						4116		
20	9.898494			8446 8543				19	0.00	4147 04241				4210		
21				8641				21	9.9					4398		
22	8689	8706	8722	8738	8754	8770	37	22						4492		
23	8787	8803	8819	8835	8852	8868	36	23						4586		
24 25	8884	8900	8916	8933	8949	8965	35	24		4617	4632	4648	4664	4679	4695	35
26				9030 9127				25 26						4773 4867		
27	9176	0102	0208	9224	0240	0256	32	27						4960		
28	9273	9289	9305	9321	9337	9354	31	28		4992	5007	5023	5638	5054	5070	31
29	9370	9386	9402	9418	9434	9450	3o	29		5085	5101	5116	5132	5148	5163	3о
	9.899467	9483	9499	9515	9531	9547	29		9.99	5179						
31	9564	9280	9396	9612 9709	9028	9044	28	31 32						5334		
33	9757	9077	0780	9806	0822	0838	26	33		5/150	5474	5400	5506	5428 5521	5537	26
34				9902				34		5552	5568	5583	5599	5614	563o	25
35	9951	9967	9983	9999	15	31	24	35		5645	5661	5676	5692	5708	5723	24
	9.900047							36		5739	5754	5770	5785	5801	5816	23
37 38				0192				37 38		5005	5047	5056	5078	5894 5987	5909	22
39				0385				39						6080		
	9.900433	0449	o465	0481	0497	0513	19		9.90	6111						
41				0578				41	• •					6265		
42				0674				42						6358		
43				0770 0866				43 44		6/80	6/07	6513	6508	645 i 6544	6550	15
45				0962				45		6575	6500	6605	6621	6636	6652	14
46				1058				46		6667	6683	6698	6713	6729	6744	13
47				1154				47						6821		
48				1250				48						6914		
49 50	9.901394			1346			9	49 50	0.00	0945	7050	7068	7083	7006	7022	
51				1537			8	51	4.4					7191		9
52	1585	1601	1617	1633	1649	1665	7	52		7222	7237	7252	7268	7283	7298	7
53	1681	1697	1713	1729	1745	1760	6	53		7314	7329	7344	7360	7375	7391	6
54 55				1824			5 4	54 55		7406	7421	7437	7452	7467	7483	5 4
56	1072	1000	1904	1920 2015	2031	20/17	3	56						7559 7651		3
57	2063	2070	2005	2110	2126	2142	2	57						7743		2
58	2158	2174	2190	2206	2222	2238	I	58		7774	7789	7805	7820	7835	785 I	I
59	2253	2269	2285	2301	2317	2333	0	59		7866	788 I	7896	7912	7927	7942	0
	GO" Co-s	50"	40 ² of 27	30" Degr	20" ees.	10"	Min.		(50" Co-	sine	40" of 36	Journ Degr	20" rees.	10"	Min.
	(1//)	2" 3"			7''	8"	9"				2" 3"			3" 7"	8"	9"
PI									Part							

Mir.	Tang	gent	of 52	Degr	rees.			Min.		Tang	gent (Degi	rees.		
	0"	10"	20"	30"	40"	50"			0"		10"	20"	30 '	40"	50"	
	10.107190	7234	7277	7320	7364	7407	59		10.12	2886 2-19	2929	2973	3017	3061	3105	59
1 2				7581 7841				1 2			3192 3455					
3	7972	8015	8058	8102	8145	8180	56	3		3674	3718	3762	3806	385o	3893	56
4	8232	8275	8319	8362	8406	8449	55	4		3937	3981	4025	4069	4113	4157	55
5	8493	8536	8579	8623	8666	8710	54	5	•	4200	4244	4288	4332	4376	4420	54
6	8733	8797	8840	8884 9144	0788	0970	50	6		4403 /1727	4507 4770	4331 4814	4858	4009	4003	52
7 8	9275	9318	9361	9405	9448	9492	51	8		4990	5034	5077	5121	5165	5209	51
9	9535	9579	9622	9666	9709	9753	50	9	:	525 3	5297	5341	5385	5428	5472	5o
IC	10.109796	9840	9883	9926	9970	13	49	1 1	10.12							
12	10.110057			0448				11		5760 6043	5823 6087	6131	6175	6210	6262	40
13				0709				13			6350					
14	0839	o833	0926	0970	1013	1057	45	14			6614					
15				1231				15			6877					
16				1492 1753				16		7097 2 360	7141 7404	7100	7229	7273	7580	43
18				2014				18		7624	7668	7712	7756	7800	7844	41
19	2145	2188	2232	2275	2319	2362	40	19		7888.	7932	7976	8020	8063	8107	40
	10.112406	2449	2493	2536	2580	2623	39	1 1	10.12	8151	8195	8239	854-	8327	8625	39
21				2798 3059				21		8670	8459 8723	8767	8811	8855	8800	37
23				3320				23		8943	8987	9031	9075	9119	9163	36
24	3451	3494	3538	3581	3625	3669	35	24		9207	9251	9295	9339	9383	9427	35
25				3843				25	•	9471	9515	9559	9603	9647	9691	34
26 27				4104 4366				26 27	,	9733	9779 ••43	9023	9007	9911	9955	32
28	4496							28	10.13	9999 0263	0307	0351	0395	0439	0483	31
29				4889				29		0527	0571	0615	0659	0703	0747	3ა
	10.115020	5063	5107	5150	5194	5238	29		10.13	0791	0835	0879	0923	0967	1011	29
32	55/3	5586	5630	5412 5674	5430	5499	28	31 32			1099 1364					
33	5804	5848	5892	5935	5979	6023	26	33			1628					
34	6066	6110	6153	6197	6241	6284	25	34		1848	1892	1936	1981	2025	2069	25
35				6450				35			2157					
36 37	685 ₂	6805	6030	6721 6982	7026	7070	23	36			2421 2686					
38	7113	7157	7201	7244	7288	7332	21	38		2906	2950	2994	3039	3083	3127	21
39	7375	7419	7463	7506	7550	7594	20	39		3171	3215	3259	3303	3347	3391	20
	10.117637	7681	7725	7768	7812	7856	19		10.13							
41				8030 8292						3065	374 4 4009	3709 4053	4007	1077	1186	17
43				8555						4230	4274	4318	4362	4406	4451	16
44				8817				44			4539					
45 46	8948	8992	9035	9079	9123	9166	14	45			4804 5069					
47	9210	0516	9297 0560	9341 9603	0647	9429 9601	12	46		5200	5334	5378	5422	5466	5510	12
48	9735	9778	9822	9866	9999	9953	II	48		5555	5599	5643	5687	5731	5775	11
49	9997	41	84	.128	.172	.216	10	49		5820	5864	5908	5952	5996	6041	10
50 51	10.120259	0565	0347	0391 0653	0434	0478	9		10.13	635 ₀	6394	6/38	6/83	6502	6577	8
52	0784	0828	0872	0033	0050	1003		52			6659					
53	1047	1001	1134	1178	1222	1266	6	53		6881	6925	6969	7013	7057	7102	6
54	1309	1353	1397	1441	1484	1528	5	54		7146	7190	7234	7279	7323	7367] [
55 5 6				1703				55 56		7411	7455	7500	7844	7288	7032	3
57				2229				57		7942	7986	8031	8075	8110	8163	2
58	2360	2404	2448	2491	2535	2579	1	58		8208	8252	8296	8341	8385	8429	I
59				2754			0	59		8473	8518	8562	8606	865o	8695	
	60"	50"	40"	30"	20"	10"	Min.		60		50"	40"	30'	20"	10"	Min.
!	Co-ta	ngen 2'' 3'		5" 6			9"				ngent		5″ €	_		9"
P	Part $\begin{cases} 1^{n} \\ 4 \end{cases}$	2" 3" 9 13	-		6 31		9" 39	P.	. Part }	-	9 13	-	5" 6	•	_	9" 4 0
	` .							<u> </u>								

-								171 1	T	SINI						1
Min.	Si 0'			Degre		E011		Min.		Si 0"		55]				
-	9.907958	10"	20"	30"	8010	803/	50	-		913365	3370	330.4	3/00	3 402	3 / 2 0	_
1				8095				I		3453	3468	3482	3409	3512	3527	39 58
2				8187				2	1	3541	3556	3571	3585	3600	3615	57
3				8279				3		363o	3644	3659	3674	3688	3703	50
4 5	8324	8340	8355	8370	8385	8401	55	4		3718	3733	3747	3762	3777	3791	55
6				8462 8553				5 6		3806	3000	3836	3850	3865 3953	3880	54
7				8644				7	1	3082	3007	1012	1026	4041	1056	50
8				8736				8		4070	4085	4100	4114	4129	4144	51
9	8781	8797	8812	8827	8842	8857	50	9		4158	4173	4188	4202	4217	4232	5c
	9.908873									914246	4261	4276	4290	4305	4320	49
II	8964	8979	8994	9009	9025	9040	48	II						4393		
12	9000	9070	9000	9191 9192	9110	9131	47 46	13	,					4481 4568		
14	9237	0252	9267	9283	9207	0313	45	14	1					4656		
15	9328	9343	9358	9374	9389	9404	44	15		4685	4700	4714	4729	4744	4758	44
16	9419	9434	9449	9464	9480	9495	43	16		4773	4787	4802	4817	4831	4846	43
17	9510	9525	9540	9555	9570	9586	42	17	ı					4919		
18	9001	9010	9051	9646	9001	9070	41	18	1					5006		
19	9.909782	0707	0812	9737	08/13	0858	30	19	0.	915123	5137	5152	5166	5094 5181	5106	30
21	9873	9888	9903	9918	9933	9948	38	21	3.	5210	5225	5239	5254	5268	5283	38
22	9963	9978	9994	9	24	39	37	22		5297	5312	5326	5341	5356	5370	37
	9.910054							23						5443		
24				0190				24	1					553o		
26				0280 0370				25 26						5617 5704		
27				0461				27						5791		
28				0551				28						5878		
29				0641				29		5907	5921	5936	5950	5965	5979	3о
	9.910686								9.	915994						
31	0776	0791	0806	0821	0836	0851	28	31		6081						
32 33	o866			1001				32		6167 6254						
34				1001				34		6341						
35				1181				35		6427	6442	6456	6470	6485	6499	24
36				1271				36		6514	6528	6543	6557	6571	6586	23
37				1360				37		6600	6615	6629	6643	6658	6672	22
38				1450 1540				38 39		6687 6773	6787	6800	6816	6830	68/5	21
	9.911584								٥.	916859						
41				1719				41	7.	6946						
42	1763	1778	1793	1808	1823	1838	17	42		7032	7046	7060	7075	7089	7104	17
43	1853	1868	1883	1897	1912	1927	16	43		7118	7132	7147	7161	7175	7190	16
44	1942	1957	1972	1987	2002	2017	15	44		7204	7210	7233	7247	7201	7270	15
45 46	2031 2121	2136	2150	2165	2180	2105	13	45 46		7290 7376	7300	7405	7410	7433	7448	13
47	2210							47		7462	7476	7491	7505	7519	7534	12
48	2299	2314	2329	2344	2358	2373	11	48		7548	7562	7576	7591	7605	7619	11
49	2388	2403	2418	2433	2448	2462	10	49		7634	7648	7662	7677	7691	7705	10
	9.912477						9		9.	917719	7734	7748	7762	7777	7791	8
51 52	2566 2655						8 7	51 52		7805 7891	7005	7010	703/	70/18	7077	7
53	2744						6	53		7976	7991	8005	8010	8033	8048	6
54	2833	2848	2862	2877	2892	2907	5	54		8062	8076	8090	8105	8119	8133	5
55	2922	2936	2951	2966	2981	2995	4	55		8147						4
56	3010						3	56		8233						3
57 58	3099						2	57 58		8318 8404						2
59	3187 3276						0	59		8489	85a3	8517	8532	8546	8560	0
-4	60"	50"	40"	30"	20"	10"	_			60"	50"	40"	30"		10"	
1	Co-s			Degr			Min		_			of 34				Min
p i	Port (1' 5	2 ' 3"			" 7"	8"	9"	P	D-	61// 6	2" 3'			" 7"	_	9"
1.1	art } 2	3 5	6	8 9	11		14	Р.	ıal	rt { 1	3 4	6	7	9 10	12	13

e l	Tang	gent	of 54	Degr	rees.			Min.			gent					
E .	0"	10"	20"	30"	40"	50"				0''	10"	20"	30"	40"	50"	L
- 1	10.138739	8783	8828	8872	8916	8960	59	1	10.	154773	4 : .		120	120		1
1	9000	9049	9093	9138 9403	9102	9220	57	1 2						5221 5490		
3	0536	0580	0625	9669	0713	0758	56	3						5759		
4	9802	9846	9891	9935	9979	24	55	4						6029		
5 1	10.140068							5		6118	6163	6208	6253	6298	6343	5
6	0334	0378	0423	0467	0511	o556	53	6						6567		
7	0600	0644	0689	0733	0777	0822	52	7						6836		
8				0999				8						7106 7375		
9	1132							9	10.	157465	7510	7555	7600	7645	7680	1
I .				1797				11						7914		
2				2064				12						8184		
3	///		1	2330	, ,			13						8453		
4				2596				14						8723		
5				2863				15						8993		
6				3129 3396				16						9263 9532		
7 8				3662				18		0622	0667	0712	0757	9802	0847	4
9	3796	3840	3885	3929	3974	4018	40	19		9892	9937	9982	27	72	.117	4
	10.144062	4107	4151	4196	4240	4285	39	20	ıo.	160162	0207	0252	0297	0342	0387	3
I				4463				21		0432	0477	0522	0567	0612	0657	3
2				4729				22		0703	0748	0793	0838	0883	0928	3
3				4996 5263				23 24						1153 1423		
5				5530				25						1693		
6	5664	5708	5753	5797	5842	5886	33	26		1784	1829	1874	1919	1964	2009	3
7				6064				27		2054	2099	2144	2189	2234	2279	3
8				6331				28						2505	l .	
9				6598				29	_					2775		
0 1	622	9777	0821	7133	6910	5955	29	30	10.	162866				3317		
2	7267	7311	7356	7400	7///	7/222	27	32						3588		
3	7534	7578	7623	7668	7712	7757	26	33						3858		
4	7801	7846	7890	7935	7980	8024	25	34						4129		
5				8203				35		4220	4265	4310	4355	4400	4445	2
6				8470				36						4671		
7	8004	8048	8693	8738	8782	8827	22	37						4942		
8	0071	0184	0901	9005 9273	9030	9090	21	38 39						5213 5485		
	10.149407								10.	165575						
I	9675	9719	9764	9809	9853	9898	18	4 r						6027		
2	_ 9 943	9987	32	76	.121	.166	17	42						6299		
	10.150210							43						6570		
5				0612 0880				44						6842 7113		
6			1	1149				45 46		720/	72/10	7023	73/10	7385	7/30	1
7				1417				47						7657		
8	1551	1595	1640	1685	1730	1774	11	48		7747	7792	7838	7883	7928	7974	I
9	1819	1864	1908	1953	1998	2043	10	49		8019	8064	8109	8155	8200	8245	I
	10.152087	2132	2177	2221	2266	2311	9		10.	168291	8336	8381	8427	8472	8517	r
I 2				2490 2758			1	51		8563	8608	8653	8699	8744	8789	
3				3027				52 53		0000	0000	0107	09/1	9016	9333	
4	3161	3206	3250	3295	3340	3385	5	54		0370	0/12/1	0460	0515	9560	0605	
5				3564			4	55		9651	9696	9742	9787	9832	9878	
6	3698	3743	3788	3832	3877	3922	3	56		9923	9968	4	59	9832	150	
7	3967	4012	4056	4101	4146	4191	2		10.	170195	0241	0286	0331	0377	0422	1
8				4370			I	58		0468	0513	0558	0604	0649	0695	
9				4639	1		-	59						0922		1
-	60"	50"	40"	30"	20"	10"	Min.			60"	50"	40"	30"	20"	10"	
	Co-tai									Co-tai				0		1_
p	Part	2" 3' 9 13	-		" 7" 7 31		9" 4 0	P.	Par	+ / - "	2" 3" 9 14			7" 7"		8" 36

Γ.	9:	ino of	56.1	Dogra		ARI			~		577	Dogw	•		_
Mgi Mgi	- 0'	10"	20"	Degre	40"	50"		Min	0"	ne of	20"	30"	40"	50"	1
0	3.918574							0	9.923591	36o5	3619	3632	3646	366o	59
1	8659	8674	8688	8702	8716	8730	58	1	3673	3687	3701	3714	3728	3742	58
3	8830	8844	8858	8872	8886	8815 8900	56	3	383 ₇	3851	3865	3878	3802	3824 3906	156
4						8985		4	3010	3033	3046	3060	3074	3987	55
5						9070		5	4001	4015	4028	4042	4055	4069	54
6	9085	9099	9113	9127	9141	9155	53	6	4083	4096	4110	4124	4137	4151	53
8	9169	9184	9198	9212	9220	9240	52	7 8	4164	4178	4192	4205	4219	4232 4314	52
9	0330	0353	0367	0381	0305	9325 9410	50	9	4328	4200 4341	4273 4355	4267 4368	4382	4314	50
10	9.919424	9438	9452	9466	9480	9494	49		9.924409						
11	9508	9522	9537	9551	9565	9579	48	II	4491	4504	4518	453 ı	4545	4559	48
12	9593	9607	9621	9635	9649	9663	47	12	4572	4586	4599	4613	4626	4640	47
13	9077	9092	9700	9720	9734	9748 9832	40	13 14						4721 4803	
15						9917		15						4884	
16	9931	9945	9959	9973	9987	I	43	16	4897	4911	4924	4938	4952	4965	43
	9.920015	0029	0043	0057	0071	0085	42	17	4979	4992	5006	5019	5033	5046	42
18						0170		18	5060	5073	5087	5100	5114	5127	41
19	9.920268					0254		19	9.925222	5235	52/0	5262	5276	5208 5280	30
21						0422		21						5370	
22	o436	0450	0464	0478	0492	0506	37	22						5451	
23						0590		23						5532	
24						0674		24						5613	
26						0758 0842		25 26						5693 5774	
27						0925		27						5855	
28	0939	0953	0967	0981	0995	1009	31	28	5868	5882	5895	5908	5922	5935	31
29						1093		29	5949	5962	5976	5989	6002	6016	30
30	9.921107					1170		30	9.926029					6177	
32						1343		32						6257	
33	1357	1371	1385	1399	1413	1427	26	33	6270	6284	6297	63 1 1	6324	6337	26
34						1510		34	6351	6364	6377	6391	6404	6418	25
35	1524	1538	1552	1566	1580	1593	24	35						6498 6578	
36						1677 1760		36 37						6658	
38						1843		38	6671	6685	6698	6711	6725	6738	21
39	1857	1871	1885	1899	1912	1926	20	39	6751	6765	6778	6791	68o5	6818	20
	9.921940								9.926831	6845	6858	6871	6885	6898	19
41						2092		41						6978 7058	
42						2175 2258		42						7138	
44	2272	2286	2300	2313	2327	2341	15	44						7217	
45						2424		45	7231	7244	7257	7270	7284	7297	14
46						2507		46	7310	7324	7337	7350	7363	7377	13
47						2589 2672		47 48	7390	7483	7410	7500	7523	7456 7536	II
49	2686	2700	2713	2727	2741	2755	10	49	7549	7562	7576	7589	7602	7615	
50	9.922768	2782	2796	2810	2823	2837	9	50	9.927629	7642	7655	7668	7681	7695	9
51	2851	2865	2878	2892	2906	2920	8	51	7708	7721	7734	7748	7761	7774	
52	2933	2947	30/3	2975 3057	3077	3002	7	52 53		7801 7880					7
54	3010	3112	3126	3139	3153	3167	5	54		7959					5
55	3181	3194	3208	3222	3235	3249	4	55	8025	8038	8052	8065	8078	8091	4
56	3263	3277	3290	3304	3318	3331	3	56	8104	8118	8131	8144	8157	8170	3
57	3345	3359	3372	3386	3400	3414	2	57	8183	8197	8210	8300	8236	8329	2
58				3468 355o			1 0	58 59	8263 83/2	8355	8368	8381	830/	8407	0
- 59	60"	50"	40"	30"	20"	10"		29	60"	50"	40"	30"	20"	10"	-
				Degi			Min.	-		sine o					Min.
-	(1")	2" 3"			" 7"	8"	9"	_	(1/)	2" 3"			7"		9"
P.	Part { 1	3 4	6		3 10		13	Ρ.	Part { 1	3 4	5	7	3 9		12
							;								

3	Tang	gent o	of 56	Degr	rees.			д	1	Tan	gent	of 57	Deg	rees.		
K	0"	10"	20"	30"	40"	50"		Min		0"	10"	20''	30"	40"	50"	
0	10.171013	1058	1103	1149	1194	1240	59	0	10.	187483						
I		133 i						I		7759	7805	7851	7898	7944	7990	58
2		1603						2		8036	8082	8128	8174	8220	8267	57
3		1876						3			8359					
5		2149						4			8636					
6		2421						5 6		0000	8913	0939	9000	9001	9097	53
- 1		2694 2967						1		0/20	9190 9467	0513	0550	0605	0651	50
7	3105	3240	3286	333 T	3377	3/22	51	8		0608	9744	0700	0836	0882	9031	51
9		3513						9			21					
10	10.173741	3786	3832	3877	3023	3068	40		ıo.	190252						
11	4014	4o6o	4105	4151	4196	4242	48	11		0529	0576	0622	o668	0714	0760	48
12	4287	4333	4378	4424	4469	4515	47	12			o853					
13	4561							13			1130					
14	4834	4880	4925	4971	5016	5062	45	14			1408					
15	5107							15			1686					
16		5427						16			1963					
17	5655							17			2241					
	5928 6202							18			2519 2797					
20	10.176476							20	10.	193029	3075	3121	3168	321/	3260	30
21	6749							21		3307	3353	3300	3446	3402	3538	38
22	7023	7060	7115	7160	7206	7252	37	22		3585	3631	3678	3724	3770	3817	37
23	7297							23			3909					
24	7571	7617	7663	7708	7754	7800	35	24			4188					
25	7846	7891	7937	7983	8028	8074	34	25			4466					
26	8120	8165	8211	8257	83o3	8348	33	26			4745					
27	8394	8440	8485	8531	8577	8623	32	27			5023					
28	8668	8714	8760	8805	8851	8897	31	28			5302					
29	8943	8988	9034	9080	9120	9171	30	29	• •	5034	5580	5027	5073	5720	5700	30
31	10.179217							31	10.	195813	6138	3900	6037	3999	6304	29
32	9492 9766	9337	0858	9029	9075	9720	20	32			6417					
	10.180041	0087	0132	0178	022/	0270	26	33			6696					
34	0316							34			6975					
35	0590							35		7208	7254	7301	7347	7304	7440	24
36	0865							36		7487	7533	, 7580	7626	7673	7719	23
37		1186						37		7766	7813	7859	7906	7952	7999	22
38	1415	1461	1507	1553	1598	1644	21	38		8045	8092	8138	8185	8232	8278	21
39	1690	1736	1782	1828	1874	1919	20	39			8371					
	10.181965								10.	198604	8651	8697	8744	8791	8837	19
41	2241	2286	2332	2378	2424	2470	18			8884	8930	8977	9024	9070	9117	18
42	2516	2502	2008	2653	2099	2745	17	42		9164	9210	9257	9303	9350	9397	17
43	2791							43		9443	9490	9337	9383	9030	9070	10
45		3112 3388						44	10	9723 200003	9770					
46	3618	3664	3700	3755	3801	38/17	73	45	10.		0330					
47	3893	3030	3085	4031	4077	4123	12	47			0610					
48	4169	4215	4261	4307	4353	4300	II	48			0890					
49	4445	4491	4537	4583	4629	4674	10				1170					
50	10.184720	4766	4812	4858	4004	4950	0		10.	201404	1450	1497	1544	1591	1637	9
51	4996	5042	5088	5134	5180	5226	8	51		1684	1731	1777	1824	1871	1918	8
52	5272	5318	5364	5410	5456	5502	7	52		1964	2011	2058	2105	2151	2198	1 7
53		5594					6	53		2245	2292	2338	2385	2432	2479	6
54	5824	5871	5917	5963	6009	6055	5	54		2526	2572	2619	2666	2713	2759	5
55		6147					4	55		2806	2853	2900	2947	2993	3040	4
56 57	0377	6423	0409	67.5	6001	6007	3	56		3087	3134	3181	3227	3274	3321	3
58	6653	6076	0743	0791	0537	0084	2	57		3308	3415	3401	3208	3000	3002	2
59	6930	7252						58 59		3049	3696 3977	4002	4070	411-	1761	1
-4	60"	50"	40"	·	20"	10"	0	29		60"	50"	40"	30"	20"		
1							Min.		,						10"	Min.
	Co-tai				C.			_		Co-tai				_		
	Part { 1" 5	2" 3"	4"	5" 6	" 7"	8" :	9"		Par	. (1" 2	." 3 "	4"	5" 6	" 7"	8"	9"

1 2 3 4	9.928420	10"	20"												1
1 2 3 4	9.928420			30"	40"	50"		Min	0"	10"	20"	30″	40"	50"	
2 3 4		8434	8447	8460	8473	8486	59	0	9.933066	3078	3091	3104	3116	3129	59
3 4	8499	8513	8520	8539	8552	8565	58	I	3141	3154	3107	3179	3192	3205	58
4	8578	8591	8605	8618	8631	8644	57	2	3217	3230	3243	3255	3268	3280	57
						8723 8801		3 4	3360	33o6 3381	3304	3/07	3/14	3330	56
5						8880		5	3//5	3457	3/70	3/80	3/05	3508	5.6
6						8959		6	3520	3533	35/15	3558	3571	3583	53
7						9037		7	3506	3608	3621	3633	36/6	3650	52
8	0050	9063	9077	9090	0103	0116	51	8		3684					
9	9050 91 2 9	9142	9155	9168	9181	9194	5o	9	3747	3759	3772	3784	3797	3810	50
10	9.929207	9220	9233	9247	9260	9273	49	Ιó	9.933822	3835	3847	386o	3872	3885	49
11	9286	9299	9312	9325	9338	9351	48	11	3898	3910	3923	3935	3948	3960	48
12	9364	9377	9390	9403	9416	9429	47	12		3985					
13	9442	9455	9468	9482	9495	9508	46	13	4048	4061	4073	4086	4098	4111	46
14	9521	9534	9547	9560	9573	9586	45	14	4123	4136	4148	4161	4174	4186	45
15	9599	9612	9625	9638	9651	9664	44	15		4211					
16	9677	9690	9703	9716	9729	9742	43	16		4286					
17	9755							17		4361					
18	9833	9846	9839	9872	9885	9898	41	18		4436					
19	9911	9924	9937	9930	9903	9970	30	19	4499	4511	4524	4530	4549	4501	40
								21	9.934574	4661	4599	4611	4624	4030	39
2 I	9.930067							22		4661 4736					
23	0223							23		4811					
24	0300							24	4873						
25	0378							25		4960					
26	0456							26		5035					
27	o533							27		5109					
28	0611							28		5184					
29	0688							29		5258					
	9.930766							30	9.935320	5333	5345	5358	5370	5382	29
31	0843							31	5395	5407	5420	5432	5444	5457	28
32	0921							32		5482					
33	0998							33	5543	5556	5568	5581	5593	56o5	26
34						1139		34		563o					
35	1152							35	5692	5704	5717	5729	5741	5754	24
36						1294		36	5700	5778	2791	5803	500	5828	23
37	1306							37 38		5852					
38	1383 1460							39	5988	5926	6013	6005	5903	6050	21
39	9.931537								9.936062						
41	1614							41	6136						
42	1691							42	6210						
43						1832		43	6284						
44	1845							44	6357	6370	6382	6394	6406	6419	15
45						1985		45	643i	6443	6456	6468	648o	6492	14
46						2062		46	6505	6517	6529	6542	6554	6566	13
47	2075							47	6578						
48	2151	2164	2177	2189	2202	2215	11	48	6652	6664	6676	6689	6701	6713	II
49	2228	2240	2253	2266	2279	2291	- (1	49	6725						
	9.932304						9		9.936799	1180	0823	0836	0848	6000	8
51	2380	2393	2400	2419	2431	2444	8	51	6872 6046	6050	6055	6000	600/	0933	
52	2457	2409	2402	2495	2508	2520	7	52 53	6946						6
53	2533						5	54	7019	7031	7043	7000	7000	7000	5
55	2609 2685	2602	2033	2047	2000	2073	4	55	7092 7165	7104	7117	7129	721/	7226	
56	2762	2090	2711	2800	2810	2805	3	56	7238	7251	7263	7275	7287	7200	4
57	2838						2	57	7312						2
58	2914						1	58	7385	7307	7400	7421	7433	7446	I
59	2990						0	59	7458	7470	7482	7404	7506	7518	0
4	60"	50"	40"	30"	20"	10"		- 9	60"	50"	40"	30"	20"	10"	
1				Degr		10	Min.			sine c					Min.
							!							8"	9"
_	Port / "	3 4			7" 7 " 3 9		9" 12	P.	Part / "	$2'' \ 3'' \ 2 \ 4$	4" 5	5" 6		_	g" 11

ď	Tan	gent	of 58	Degr	ees.			,ri	Tan:	gent	of 59	Deg	rees.		Γ
Mnd.	0''	10"	20"	30"	40"	50"		Min.	0"	10"	20"	30"	40"	50"	
0	10.204211	4258	4304	4351	4398	4445	59	О	10.221226						
1				4633				I					1703		
2				4914				2					1990		
3				5195				3					2276		1
5	5336	5383	5430	5477	5924	5050	5.4	5	2372	2419	2467	2010	2563	2010	5
6				5758 6040				6	2036	2700	30/0	3088	2849 3136	2097	5
- 1	6181	6027	627/	6321	6368	6/15	52	7					3423		
7 8	6/62	6500	6556	6603	6650	6607	5 r	8					3710		
9	6744	6701	6838	6885	6.932	6979	50	9	3805	3853	3001	3040	3997	4044	5
ó	10.207026	7073	7120	7167	7214	7261	49	10	10.224092	4140	4188	4236	4284	4332	4
1	7308	7355	7402	7449	7496	7543	48	11	4379	4427	4475	4523	4571	4619	4
2	7590	7637	7684	7731	7778	7825	47	12	4667	4714	4762	4810	4858	4906	4
3	7872	7919	7966	8013	8060	8107	46	13	4954	5002	5050	5098	5145	5193	4
41				8295				14	5241	5289	5337	5385	5433	5481	4
5				8578				15					5720		
6				886o				16					6008 6296		
7 8	9001	0331	0378	9143 9425	0/40	0510	42	17 18					6583		
9	0566	061/	0661	9708	0755	0802	41	19					6871		
	10.209849	0806	0043	0001	38	85	30		10.226967						
	10.210132							21					7447		
2				0556				22					7736		
3	• 0698	0745	0792	0839	0886	0934	36	23	7832	788o	, 7928	7976	8024	8072	3
4	0981	1028	1075	1122	1170	1217	35	24	8120	8168	8216	8264	8312	836o	3
5	1264	1311	1358	1405	1453	1500	34	25					8601		
3				1689				26					8889		
7	1830	1878	1925	1972	2019	2066	32	27	8985	9033	9081	9130	9178	9226	3
8	2114	2161	2208	2255	2303	2350	31	28					9466		
9				2539				29	9563	9611	9659	9707	9755	9803	3
	10.212681							30	10.229852	9900	9940	9990	44	- 92	2
1				3106 3390					10.230140				0622		
3				3674				32 33					0911		
4				3958				34					1201		
5				4242				35					1490		
6	4384	4431	4478	4526	4573	4620	23	36	1586	1635	1683	1731	1779	1828	2
7				4810				37	1876	1924	1973	2021	2069	2117	2
8	4952	4999	5047	5094	5141	5189	21	38	2166	2214	2262	2310	2359	2407	2
9	5236	5284	5331	5378	5426	5473	20	39	2455	2504	2552	2600	2648	2697	2
	10.215521	5568	5615	5663	5710	5758	19	40	10.232745	2793	2842	2890	2938	2987	1
I	5805	5852	5900	5947	5995	6042	18	41	3035	3083	3132	3180	3228	3277	1
2				6232				42	3325	3373	3422	3470	3518	3567	I
3				6517				43	3015	3003	3712	3700	3808	3857	I
5				6801 7086				44					4099 4389		
6	7220	7276	732/	7371	7/10	7/66	13	46					4679		
7	7514	756r	7600	7656	770/	7751	12	47	1776	1825	4873	4021	4970	5018	1
ś	7799	7846	7804	7941	7980	8036	11	48	5067	5115	5164	5212	5260	5300	ľ
9	8084	8131	8170	8226	8274	8322	10	49	5357	5406	5454	5503	5551	5600	ī
o	10.218369	8417	8464	8512	8559	8607	9	5o	10.235648	5696	5745	5793	5842	5890	1
1	8654	8702	8750	8797	8845	8802		51	5030	5087	6036	6084	6133	6181	1
2	8940	8987	9035	9083	9130	9178	7 6	52	6230	6278	6327	6375	6424	6472	
3	9225	9273	9321	9368	9416	9463	6	53	6521	6569	6618	6666	6715	6763	
4	9511	9339	9006	9654	9701	9749	5	54	6812	6860	6909	0957	7006	7055	
5	9797	9044	9892	9939	9987	35		55	7103	7152	7200	7249	7297	7346	1
9	10.220082	0130	0178	0220	0273	0521	3	56	7394	7443	7492	7340	7589	7637	1
7 8				0511				57	7086	7734	7783	7032	7880	7929	1
9	0034	0088	10749	0797 1083	1137	1170	0	58					8172 8463		
7	60"	50"	40"	30"	20"	10"	-	59		50"			_		1
							Min.		Go to		40"	30"	20"	10"	- 1
	Co-tar								Co-tai						L
	Part $\left\{ \begin{array}{ll} 1'' & 5 \\ 5 & \end{array} \right\}$	2" 3"	4''	5" 6	" 7"	8"	9"		Part $\begin{cases} 1'' & 2 \\ 5 & 1 \end{cases}$	2" 3"	4''	5" 6	" 7"	8"	9'

	Si	ine of	f 60 1	Degre				M I	· ~		61 7	Dom)OG]-
Min.	0"	10"	20"		40"	50"		Min	0"	ine of	20"	30"	40"	50"	{
0								0	9.944819						
1 2						7664 7737		1 2	1889	1901	1913	1924	1936	1948	58
3	7749	7761	7773	7786	7798	7810	56	3	2029	2041	2052	2064	2076	2087	56
4	7822	7834	7846	7858	7870	7883	55	4	2099	2111	2122	2134	2146	2157	55
5 6	7893 7067	7907	7919	7931 8004	8016	7955 8028	53	5 6	2109	2180 2250	2192	2204	2215	2227	53
7	8040	8052	8064	8076	8088	8100	52	7	2308	2320	2331	2343	2355	2366	52
8						8173 8245		8		2390	1 1	1 1 -	1 1	1 :	1 .
10	9.938258	8270	8282	8204	8306	8318	40	9	9.942517	2459 2520					
11	8330	8342	8354	8366	8378	8390	48	11	2587	2598	2610	2621	2633	2645	48
12	8402 84 0 5	8414	8426	8439	8523	8463 8535	47	13	2656	2668 2737	2679	2691	2702	2714	47
14	8547	8559	8571	8583	8595	8607	45	14		2806					
15	8619	8631	8643	8655	8667	8679	44	15	2864	2876	2887	2899	2910	2922	44
16	8691 8763	8703	8715	8800	8812	8751 8824	43	16		2945 3014					
17 18	8836	8848	8860	8872	8884	8896	41	18		3083					
19	8908	8920	8932	8944	8956	8968	40	19	3141	3153	3164	3176	3187	3199	40
20 21	9.938980 9052	8992	9004	9016	9028	9040	39	20 21	9.943210	3222 3291					
22	9123	9135	9147	9159	9171	9183	37	22		336o					
23	9195	9207	9219	9231	9243	9255	36	23		3429					
24 25	9267	9279 0351	9291	9303	0387	9327 9399	35	24		3498 3566					
26	9410	9422	9434	9446	9458	9470	33	26	3624	3635	3647	3658	3670	3681	33
27	9482	9494	9506	9518	953o	9542	32	27	3693	3704	3715	3727	3738	3750	32
28 29	9554 9625	0637	9578	9590	0673	0685	30	28 29		3773 3841					
30	9.939697	9709	9721	9733	9744	9756	29		9.943899	3910	3921	3933	3944	3956	29
31	9768	9780	9792	9804	9816	9828	28	31		3978					
32 33	9840 9911	9832	9863	9873	9007 0050	9899	$\frac{27}{26}$	32 33		4047 4115					
34	9982							34		4184					
	9.940054							35		4252					
36 37	0125					0184		36 3 ₇		4321 4389					
38	0267	0279	0291	0303	o314	0326	21	38	4446	4457	4468	448o	4491	4503	21
39	0338	0350	0362	0374	0385	0397	20	39	4514	4525	4537	4548 46+6	4559	4571	20
40	9.940409 0480							41	9.944582 4650	4661					
42	0551	o563	0575	o586	0598	0610	17	42	4718	4730	4741	4752	4764	4775	17
43	0622							43		4798					
44 45	0693 0763							44	4022	4865 4933	4045	4956	4099	4911	14
46	o834	0846	o858	0870	0881	0893	13	46	4990	5001	5013	5024	5035	5046	13
47	0905	0917	0928	0940	0952	0964	12	47	5058	5069 5137	5080	5092	5103	5114	12
48 49	0975 1046	1058	1070	1081	1093	1105	10	48	5193	5204	5216	5227	5238	5250	10
50	9.941117	1128	1140	1152	1164	1175	9	50	9.945261	5272	5283	5295	53o6	5317	9
51 52	1187 1258	1199	1211	1222	1304	1246	8	51 52		5340 5407					
53	1328	1340	1351	1363	1375	1387	7 6	53	5464	5475	5486	5497	55og	5520	6
54	1398	1410	1422	1433	1445	1457	5	54	553ı	5542	5554	5565	5576	5587	5 4
55 5 6	1469 1539						4	55 56	5598 5666	5610 56 7 7	5688	5700	5711	5722	3
57	1609	1621	1632	1644	1656	1667	2	57	5733	5744	5756	5767	5778	5789	2
58	1679	1691	1702	1714	1726	1738	I	58	5800	5812	5823	5834	5845	5857	1
59	1749	50"	1773	30"	20"	1808	0	59	5868	5879 50"	5890 40"	30"	20"	10"	
ŀ				$\frac{30^{\circ}}{\text{Degr}}$		10	Min.			sine o				2.5	Min.
	(111 0	2" 3"		5" 6		8" (9"			2" 3"			" 7"	8"	9"
Р.		2 4		6 7			11	ľ.	Part \ 1" !	2 3	5		7 8		10

1	Tang	gent	of 60	Deg	rees.			ri li	Tang	gent	of 61	Deg	rees.		
Min	ייט	10"	20"	30"	40"	50"		Min	0"	10"	20"	30″	40"	50"	
0	10.238561								10.256248						
1 2						9096 9388		1 2					6745 7043		
3						9680		3					7341		
4	9728	9777	9826	9874	9923	9972	55	4	7441	7490	7540	7590	7640	7689	55
5	10.240021							5	7739	7789	7839	7888	7938 8237	7988	54
6	0605	0654	0703	0752	0800	0557 0849	52	7					8535		
8	0898	0947	0995	1944	1093	1142	51	8					8834		
9						1434		9					9133		
10	10.241483	1825	1873	1029	1078	1727 2020	49 48	11	10.259233				9432		
12						2313		12					31		
13	2362	2411	2459	2508	2557	2606	46	13	10.260130	0180	0230	0280	o33o	o38o	46
14	2655	2704	2753	2801	2850	2899 3192	45	14					0629		
15 1 6						3486		15					0929 1229		
17	3535	3584	3632	3681	3730	3779	42	17	1329	1379	1429	1479	1529	1579	42
18						4073		18	1629	1679	1729	1779	1829	1879	41
19	4122					4366		19	1929	1979	2029	2079	2129	2179	40
21						4954		21	2529				2729		
22	5003	5052	5101	5150	5199	5248	37	22	2829	2879	2929	2979	3029	3079	37
23						5542		23					3330		
24 25						5836 6131		24 25					3630 3931		
26						6425		26					4232		
27	6474	6523	6572	6621	6670	6720	32	27	4332	4382	4433	4483	4533	4583	32
28						7014		28	4633 4934	4683	4734	4784	4834	4884	31
30	10.247358	7407	7456	7505	7554	7309 7604	20	29 30	10.265236	5286	5336	5386	5436	5487	20
18	7653	7702	7751	7800	7849	7899	28	31	5537	5587	5637	5688	5738	5788	28
32						8194		32					6039		
33 34						8489 8784		33	6442				6341 6643		
35	8833	8882	893r	8981	9030	9079	24	35					6945		
36	9128	9178	9227	9276	9325	9375	23	36	7045	7096	7146	7196	7247	7297	23
37 38	9424	9473	9522	9572	9621	9670	22	3 ₇ 38					7549		
- 1	10.250015					9966 0261		39					7851 8153		
	10.250311	0360	0409	0459	0508	0557	19		10.268254	8304	8355	8405	8456	8506	19
41						0853		41					8758		
42						1149		42 43	0009	0909	0263	9010	9061 9364	9111	17
44	1495	1544	1594	1643	1692	1742	15	44	. 9465	9515	9566	9616	9667	9717	15
45						2038		45	9767	9818	9868	9919	9970	20	14
46 47						2335 2631			10.270071	0121	0172	0222	0273	0323	13
48						2928			0574	0728	0473	0820	0879	0030	II
49	2977	3027	3076	3126	3175	3225	10	49	0980	1691	1082	1132	1183	1233	10
50	10.253274	3324	3373	3423	3472	3521	9		10.271284						9
51 52	3868	3018	3070	1017	4066	3818 4116		51 52					1790 2094		8
53	4165	4215	4264	4314	4363	4413	7 6	53					2398		7 6
54	4462	4512	4561	4611	4661	4710	5	54	2499	2550	2601	2651	2702	2753	5
55 56	4760	4809	4859	4908 5206	4958	5008	4	55					3006		4 3
57	5355	5404	5454	5504	5553	5603	3	56 57					3310 3615		2
58	5652	5702	5752	5801	5851	5901	I	58					3919		ī
59	5950	6000	6049	6099	6149	6198	0	59	4021	4072	4122	4173	4224	4275	0
	60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
-	Co-ta						1 1		Co-tar						
P	Part/ "	2″ 3′ 10 15	_	5" 6 25 2	" 7" 9 34		9" 44	P.	Part /	$^{\prime\prime}_{0} \ _{15}^{\prime\prime}$		5" 6 25 3	" 7" 0 35	8" 9 40 4	
L.	, ,		~ ~ 0	~ ~ ~		00			, , ,	• 1.7	~0		, ,,,	7U *	

Min.				Degre				Min.		ne of					
_	0"	10"	20"	30"	400	50"		l	0"	10"	20"	30″	40′′	5(11	_
0	9.945935							0		9892	9902	9913	9924	9935	15
1	6002	6013	6024	6036	6047	6058	58	I	9945	9956	9967	9977	9988	9999	15
2	6069	6o8o	6092	6103	6114	6125	57	2	9.950010	0020	0031	0042	0052	0063	5
3						6192		3	0074	0084	0095	0106	0117	0127	15
4	6203	6214	6226	6237	6248	6259	55	4		0149					
5						6326		5		0213					
6						6393		6		0277					
- 1						646o		7		o34i					
78						6526		8		0405					
- 1						6593		9		0469					
9	9.946604							10	9.950522	0533	05//	0554	0565	0576	1
11						6726		11	0586	0597	0605	0618	0600	0630	1
12	- 1 - 1				l - * -			12							
13						6793				0661					
1	60	6000	60-20	6-01	65	6860	40	13	0714	0724	0733	0740	0730	0707	15
14						6926		14		0788					
15						6993		15		0852					
16						7059		16		0915					
17						7125		17	0968	0979	0990	1000	1011	1021	4
18						7192		18		1043					
19						7258		19	1096	1106	1117	1127	1138	1148	1
20	9.947269	7280	7291	7302	7313	7324	39	20	9.951159						
21						7390		21	1222	1233	1244	1254	1265	1275	3
22						7456		22	1286	1296	1307	1317	1328	1339	13
23						7522		23		1360					
24	7533	7545	7556	7567	7578	7589	35	24		1423					
25						7655		25		1486					
26	7665	7676	7687	7608	7700	7720	33	26		1549					
i	7000	70,0	7007	7090	7709	7786	30	27		1613					
27								28		1676					
28	7797	7000	7019	7030	7041	7852	31	li i							
29	7003	7074	7000	7090	7907	7918	30	29		1739					
	9.947929	7940	7921	7902	7973	7984	29		9.951791						
31						8049		31		1865					
32						8115		32	, , ,	1928					4
33						8181		33		1990					
34	8192	8203	8213	8224	8235	8246	25	34		2053					
35	8257	8268	8279	8290	8301	8312	24	35		2116					
36	8323	8334	8344	8355	8366	8377	23	36	2168	2179	2189	2200	2210	222 I	2
37	8388	8399	8410	8421	8432	8443	22	37		2241					
38	8454	8464	8475	8486	8497	8508	21	38	2294	2304	2314	2325	2335	2346	2
39						8573		39	2356	2367	2377	2387	2398	2408	2
40	9.948584								9.952419						
41	8650	866o	8671	8682	8603	8704	18 l	41		2492					
42						8769		42		2554					
43						8834		43	2606	2617	2627	2637	2648	2658	1
44						8899		44	2660	2679	2680	2700	2710	2720	,
45						8964		45		2741					
								46		2803					
46						9029		. '		2866					
47						9094		47							
48						9159		48		2928	0	0	10	10.0-	1 _
49						9224		49	2900	2990	2000	2011	30021	3031	1
	9.949235	9246	9256	9267	9278	9289	9		9.953642	3032	3002	3073	3003	3093	1
51	9300	9310	9321	9332	9343	9354	8	51		3114					
52	9364	9375	9386	9397	9408	9418	7	52		3176					
53	9429	9440	9451	9462	9472	9483	6	53		3238					
54	9494	9505	9515	9526	9537	9548	5	54	3290	3300	3310	3321	3331	3341	
55	9558	9560	9580	9591	9602	9612	4	55	3352	3362	3372	3382	3393	3403	
56	9558 9623	9634	9645	9655	9666	9677	3	56	3413	3424	3434	3444	3455	3465	1
57	9688	9608	9700	9720	9731	9741	2	57	3475	3485	3496	3506	3516	3527	
58	9752	0763	9774	0784	9705	9806	1	58	3537	3547	3557	3568	3578	3588	
59				9849			0	59	3500	3609	3610	3629	3640	365o	1
7	60"	50"	40"	30"	20"	10"		-	60"	50"	40"		20"	10"	`-
1		sine o		_		10	Min.			sine					
	L _O -	SITIA (M 2/	Degr	rees.		انخا	1	Un-	sine (11 20	Ther.	LCCS.		1

.1	Tang	ent	of 62	Degr	rees.			ė		Tan	gent	of 63	Deg	rees.		1
Mir	077	10"	207	30"	40"	50"		Min	0		10"	20"	30"	40"	50"	1
0	10.274326					4580	50	0	10.20	2834	2886	2038				5
- 1						4885		ı	,,,,,,		3199					
I	4035	4001	5035	5088	5 7 3 0	5190	5.7	2			3511					
3	50.40	5001	53/0	5303	5444	5495	56	3		3550	3824	38#6	3028	3080	4030	5
. [5546	550	564-	5608	5-44	5800	55	и.		6086	4137	4.80	10/1	4903	4345	5
4								4								
5						6105		5		4397	4449	4002	4004	4000	4030	15
6						6411		6			4763					
78						6717		7			5076					
8						7022		8			5389					
9	7073	7124	7175	7226	7277	7328	50	9			5703					
0	10.277379	7430	7481	7532	7583	7634	49	10	10.29							
[I]	7685	7736	7787	7838	7889	7940	48	11			633o					
2	7991	8043	8094	8145	8196	8247	47	12		6591	6644	6696	6748	6801	6853	14
3	8298	8349	8400	8451	8502	8553	46	13		6905	6958	7010	7062	7115	7167	14
4	8604	8655	8706	8757	8809	886o	45	14			7272					
5						9166		15			7586					
6	0217	0268	0320	637I	0422	9473	43	16		7848	7900	7953	8005	8058	8110	14
7	0524	0575	0626	6678	0720	9780	42	17			8215					
8	0831	0882	0033	0084	36	87	41	18			853o					
	10.280138	0180	02/10	0202	03/13	030/	10	19			8845					
	10.280445								10.29							
11						1009		21	10.29	0/00	0/75	0500	0580	0630	0685	٦
- 1								1		9422	9475	08/0	0805	9032	9000	3
2						1316		22	* 0 30		9790					
:3	1307	1419	1470	1321	1372	1624	30		10.30							
4	1073	1720	1777	1829	1880	1931	33	24			0421					
5						2239		25			0736					
6						2547		26			1052					
7						2855		27			1368					
28						3164		28		1631	1684	1737	1789	1842	1895	3
19	3215	3266	3318	3369	3421	3472	30	29		1947	2000	2053	2106	2158	2211	3
30	10.283523	3575	3626	3678	3729	3780	29	30	10.30	2264	2316	2369	2422	2475	2527	2
31	3832	3883	3935	3986	4038	4089	28	31		2580	2633	2686	2738	2791	2844	. 2
32						4398		32		2897	2950	3002	3055	3168	3161	2
33						4707		33		3213	3266	3310	3372	3425	3478	2
34						5016		34		353o	3583	3636	3680	3742	3704	2
35						5325		35		3847	3900	3053	4006	4050	4112	2
36						5634		36			4217					
37	5686	5737	5080	58/0	5802	5943	20	37		1/80	4535	4588	4640	4603	4746	
8	5005	60/6	6008	6.50	6201	6253	0.1	38			4852					
								II -								
39						6562		39	70 30		5170					
	10.286614								10.30	5-5-	5407	5040	5595	5-6/	3099	
ΙI	0924	0973	7027	7079	7130	7182	10	41		3732	5805	2020	3911	2904	0017	1
2	7234	7285	7337	7389	7440	7492	17	42			6123					
[3]	7544	7595	7647	7099	7751	7802	10	43			6441					
44						8113		44			6760					
15	8164	8216	8268	8319	8371	8423	14	45		7025	7078	7131	7184	7237	7290	1
6						8733		46		7344	7397	7450	7503	7556	76 0 9	1
17	8785	8837	8889	8941	8992	9044	I 2	47		7662	7715	7768	7822	7875	7928	3
18	9096	9148	9199	9251	9303	9355	11	48		7981	8034	8087	8141	8194	8247	1
19	9407	9458	9510	9562	9614	9666	10	49		8300	8353	8406	8460	8513	8566	j
0	10.289718	9769	0821	6873	9925	9977	9	50	10.30	8619	8672	8726	8779	8832	8885	,
51	10.290029	0081	ó132	ó184	0236	0288	8	51			8992					
52	0340	0302	0444	0496	0547	0500		52		9258	9311	0364	9418	9471	9524	
3	0651	0703	0755	0807	0850	10011	7	53		0577	9631	6684	0737	0700	08//	
54	0963	1015	1066	1118	1170	1220	5	54		0807	9950	1	5,57	1110	164	1
55				1430			4	55	10.31	7277	3300	032/	0377	0//30	0/8/	
56							3	56	10.01							
						1846	1 :			0957	0590	0044	0097	0730	0004	
57						2158	2	57		0007	0910	0904	1017	1070	1124	:
8						2470	I	58			1231					
9				<u> </u>		2782	0	59			1551				1765	1
	60".	50"	40"	30"	20"	10"	ä		60		50"	40"	30"	20"	10"	T
ı	Co-tai	igent	of 2	7 De	grees		Min.		(Co-ta	ngent	of 2	6 De	grees		1
		0			J		1	11			0					1

-	S	ine of	f 64	Degre	es.		:		Г	S	ine of	f 65	Degre	900		
Min.	0"	10"	20"	30"	40"	50"	!	Min	-	0"	10"	20"	30"	40"	50"	
0	9.953660							0	9.	957276	7286	7295	7305	7315	7325	50
1				3753				1	ľ	7335	7344	7354	7364	7374	7384	58
2				3814				2		7393	7403	7413	7423	7433	7442	57
3 4				3876				3		7452	7462	7472	7482	7491	7501	56
5				3937 3998				5		7511	7521	7580	7540	7550 7609	7500	5.6
6				4060				6		7628	7638	76/8	7658	7667	7677	53
7	4090	4101	4111	4121	4131	4141	52	7		7687	7697	7707	7716	7726	7736	52
8	4152	4162	4172	4182	4192	4203	51	8		7746	7755	7765	7775	7785	7794	51
9				4243				9		7 804	7814	7824	7833	7843	7853	50
	9.954274								9.	957863	7872	7882	7892	7902	7911	49
II				4366				II		7921	7931	7940	7950	7960	7970	48
13				4427 4488				13		7979	7909	7999	8065	8018 8077	8028	47
14				4549				14						8135		
15				4610				15						8193		
16	4640	465o	4661	4671	4681	4691	43	16						8251		
17	4701	4711	4721	4732	4742	4752	42	17		8271	8280	8290	8300	8309	8319	42
18	4762	4772	4782	4792	4802	4813	41	18		8329	8339	8348	8358	8368	8377	41
19	4823	4833	4843	4853	4863	4873	40	19						8426		
	9.954883	4894	4904	4914	4924	4934	39		9.	958445						
21				49 7 4 5035				21		8561	85	859	8500	8542	86001	38
23				5096				22 23						8657		
24	5126	5136	5146	5156	5166	5176	35	24		8677	8686	8606	8706	8715	8725	35
25	5186	5106	5207	5217	5227	5237	34	25		8734	8744	8754	8763	8773	8783	34
26	5247	5257	5267	5277	5287	5297	33	26						8831		
27	5307	5317	5327	5337	5348	5358	32	27		885o	886o	8869	8879	8888	8898	32
28				5398				28		8908	8917	8927	8937	8946	8956	31
29				5458				29						9004		
	9.955488								9.	959023	9033	9042	9052	9061	9071	29
31 32	5600	5670	5600	5579 5639	5566 5666	5650	28	31		9080	9090	9100	9109	9119	9128	28
33	5660	5670	5680	5699	5700	5770	26	32 33		9138 9195	0205	9137	9107	9170	9100	27
34	5720	5730	5740	5759	576a	5770	25	34		0253	0262	0272	0282	9291	0301	25
35	5780	5799	5800	5819	5820	5830	24	35						9348		
36	5849	5859	5869	5879	5889	5899	23	36						9406		
37	5909	5919	5929	5939	5949	5959	22	37		9425	9434	9444	9453	9463	9473	22
38				5999				38		9482	9492	9501	9511	9520	9530	2 I
39				6059				39		9539	9549	9558	9568	9577	9587	20
	9.956089	6-59	6-69	6178	6-00	6138	19		9.	959596	9606	9615	9625	9634	9644	19
41				6238				41		9654	9003	9073	9002	9092	9701	10
43				6298				43		9711	0777	0787	9709	9806	0815	16
44				6357				44						9863		
45				6417				45		9882	9891	9900	9910	9919	9929	14
46	6447	6457	6466	6476	6486	6496	13	46		9938	9948	9957	9967	9976	9986	13
47				6536				47		9995	5	14	24	33	43	12
48				6595					9.	960052	0061	oc 71	0080	0090	0099	11
49				6655			- 1	49		0109						
51	9.956684						8	51	9.	960165						8
52				6773 6833			7	52		0222				0260		7
53				6892			6	53		0335						6
54				6951			5	54		0392						5
55				7010			4	55		0448	o458	0467	0477	o486	0495	4
56	7040	7050	7059	7069	7079	7089	3	56		0505	0514	0524	o533	0542	0552	3
57	7099	7109	7118	7128	7138	7148	2	57		0561						2
58				7187			I	58		0618						1
59		·	-	7246			0	59		0674						0
-	60"	50"	40"	30"	20"	10"	Min.			60"	50"	40"	30"	20"	10"	Min.
				Degr								of 24				
P. 1	Port J - "	2" 3" 2 3	4" 4	5" 6			9" 9	Р.	Pa	rt \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	$\frac{2''}{2} \frac{3''}{3}$	4 4		3" 7 " 6 7	8" 8	9"
		~ 3	- 1	5 6			0			(1	~ 3		<u> </u>	6 7		9

-	Tane	gent o	of 64	Degr	rees.			ď	Tr	ngent	of 65	Deg	rees.		
Min.	0"	10"	20"	30"	40"	50"	-	Min	0"	10"	20"	30"	40′′	50"	
	10.311818								10.3313						
I						2406 2727		2	10	57 1712 37 2042	2007	2153	2208	2263	57
3						3048		3		18 2373					
4	3102	3155	3209	3263	3316	3370	55	4	26.	18 2703	2758	2813	2868	2924	55
5						3691		5	29	79 3034	3089	3144	3199	3254	54
6						4013		6		9 3364 40 3695					
7	4388 4388	4120	4405	4540	4603	4334 4656	5 ₁	8		1 4026					
9						4978		9		4358					
Ιó	10.315032	5086	5139	5193	5247	5300	49		10.3346						
ΙΙ	5354	5408	5461	5515	5569	5623	48	ΙΙ		55 5021					
12 13						5945 6268		12 13	56 ₅	97 5352 29 5684	57/10	5705	5850	5006	47
14						6590		14		6016					
15	6644	6698	6752	6806	686o	6913	44	15		3 6349					
16	6967	7021	7075	7129	7183	7236	43	16		5 6681					
17	7290	7344	7398	7452	7500	7560	42	17		8 7013					
18	7013	7007	8045	8000	7029 8153	7883 8206	41	18		91 7346 24 7679					
20	10.318260	8314	8368	8422	8476	853o	39		10.3379	7 8012	8068	8123	8179	8234	39
21						8854		21	820	0 8345	8401	8456	8512	8568	38
22						9178		22		3 8679					
23						9502		23 24		9012 90 9346					
24 25						9826 .151		25		4 9680					
	10.320205							26	99	8 14	70	.125	.181	.237	33
27						0800		27	10.34020	2 0348	0404	0460	0515	0571	32
28						1125		28	06:	0682	0738	0794	0850	0905	31
29 30						1450		29	10.34120	6 1350					
31						2100		31	_ :	1687	1 .				1 5 1
32	2154	2209	2263	2317	2371	2426	27	32	19	6 2022	2078	2133	2189	2245	27
3 3	2480	2534	2588	2643	2697	2751	26	33		2357					
34 35						3077 3403		34 35		36 2692 72 3028					
36						3729		36		8 3364					
37						4055		37	36	14 3700	3756	3812	3868	3924	22
38	4110	4164	4219	4273	4327	4382	21	38	39	30 4o36	4092	4148	4204	4260	21
39						4708		39		6 4372					
41	10.324763					5362		40	10.3446	39 5045					
42						5689		42		26 5382					
43						6016		43		53 5719					
44						6343		44		00 6056					
45						6671		45		37 6393 74 6731					
46 47						6999 7326		46		74 0731					
48	7381	7436	7490	7545	7600	7654	11			7406					
49	7709	7764	7818	7873	7928	7982	10	49	76	38 7744	7800	7857	7913	7969	10
	10.328037	8092	8147	8201	8256	8311			10.3480	26 8082	8139	8195	8551	8676	8
51 52	8604	8749	8803	8858	8013	8639 8068	1 1	51 52	8=	54 8421 53 8759	8815	8870	8028	8085	7
53		9077						53	90	41 9098	9154	9211	9267	9324	6
54	9351	9406	9461	9516	9571	9625		54	93	30 9437	9493	9550	9606	9663	5
55	9680	9735	9790	9845	9900	9955		55	97	19 9776	9832	9889	9945	2	4
56									10.3500						
57 58		0394					2 I	57 58		98 0454 37 0794					
59	1	1053					0	59		77 1134					
广	60"	50"	40"	30"	20"	10"		ŕ	60"	50"	40"	30"	20"	10"	
	Co-ta	0	of 2	5 De	grees		Min.		Co-	angen	t of 2	4 De	grees		Min.
p		2" 3"	_		" 7"		9"	р	Part \ 1"	2" 3"	_	-	7"		9"
	'art { 5	11 16	22	27 3	3 38	43	49	1.	1 art { 6	11 17	22	28 3	3 39	45	59

					U G A		111		-		2 0 111 2				
Min.				Degre		For		Min.				Degre		,	
-	0"	10"	20"	30"	40"	50"	50		0"	10"	20"	30"	40"		-
0	9.96073 <i>0</i>	0706	0805	0814	0824	0833	58	I	9.964026 4080	4033	4044	4106	4115	4071	58
2	0843	0852	0861	0871	0880	0889	57	2						4178	
3	0899	0908	0917	0927	0936	0945	56	3	4187	4196	4205	4214	4222	4231	56
4				0983				4	4240	4249	4258	4267	4276	4285	55
5				1039				5						4338 4392	
7				1151				7						4445	
8				1207				8	4454	4463	4471	448o	4489	4498	51
9	1235	1244	1253	1263	1272	1281	50	9	4507	4516	4525	4534	4542	4551	50
1	9.961290	1300	1309	1318	1328	1337	49		9.964560	4569	4578	4587	4596	4604	49
11				1374 1430				11	4666	4675	4684	4603	4049	4658 4711	40
13		1 1 -	1 : 4	1485		1	1	13						4764	
14	1513	1523	1532	1541	155o	1560	45	14	4773	4781	4790	4799	4808	4817	45
15				1597				15						4870	
16				1652 1708				16	4879	4887	4896	4905	4914	4923 4975	43
17				1763				17	4084	4003	5002	5011	5020	5028	42 /T
19				1819				19						5081	
20	9.961846	1856	1865	1874	1883	1892	39		9.965090	5099	5107	5116	5125	5134	39
21	1902	1911	1920	1929	1939	1948	38	21						5187	
22				1985 2040				22						5239 5292	
24	2012	2021	2086	2095	2104	2113	35	24	53oı	5300	5318	5327	5336	5344	35
25	2123	2132	2141	2150	2159	2169	34	25	5353	5362	5371	5379	5388	5397	34
26				2205				26	5406	5414	5423	5432	5441	5449	33
27	2233	2242	2251	2260	2269	2279	32	27						5502	
28				2315 2370				28 29	5563	5572	5580	5580	5508	5554 5607	30
29 3c	9.962398								9.965615						
31	2453	2462	2471	2480	2489	2498	28	31	5668	5676	5685	5694	5702	5711	28
32	2508	2517	2526	2535	2544	2553	27	32						5763	
33	2562	2572	2581	2590	2599	2008	25	33	5772	5933	5840	5798	5850	5816 5868	20
34				2645 2699				34	5876	5885	580/	5002	5011	5920	24
36				2754				36	5929	5937	5946	5955	5963	5972	23
37	2781	2790	2799	2809	2818	2827	22	37	5981	5989	5998	6007	6015	6024	22
38	2836			2863				38						6076	
39	2890	2899	2909	2918	2927	2930	20	39	9.966136					6128	
41	962945			3027				41						6232	
42				3081				42	6240	6249	6257	6266	6275	6283	17
43	3108	3117	3126	3135	3144	3153	16	43	6292	6301	6309	6318	6326	6335	16
44	3163	3172	3181	3190	3199	3208	15	44						6387	
45				3244 3298				45 46	6//-	6/156	6/6/	6/173	6/82	6438 6490	13
47	1			3352				47	6499	6507	6516	6525	6533	6542	12
48	3379	3388	3398	3407	3416	3425	LI	48	6550	6559	6567	6576	6585	6593	II
49	3434	3443	3452	3461	3470	3479	10	49	6602	6610	6619	6628	6636	6645	
50	9.963488	3497	3506	3515	3524	3533	8	50 51	9.966653	6002	65070	673	6530	6748	8
51	3506	3605	36±4	3569 3623	3632	3641		52						6799	
53	3650	3659	3668	3677	3686	3695	6	53	6808	6816	6825	6833	6842	6850	6
54	3704	3713	3722	3730	3739	3748	5	54	6859	6867	6876	6884	6893	6902	5
55	3757	3766	3775	3784	3793	3802	4	55	6910	6919	6927	6936	6944	6953	4 3
56	3811	3820	3829	3838 3892	3007	3010	3	56 57	7013	7021	7036	7038	7045	7004	
58				3946				58	7064	7072	7081	7080	7098	7106	I
59	3972	3981	3990	3999	4008	4017	0	59						7157	
1	60"	50"	40"	30"	20"	10"	-	٢	60"	50"		30"	20"	10"	.ji
				Deg	rees.		Min.		Co			Deg			Min.
P	Part J =	2" 3			3" 7"		9"	P.	Part \ 1"	2" 3			6" 7'	-	9"
1	1 411	2 3	3 4	5	5 6	7	8	L.	1	2 3	3 3	4	5 6	7	8

		-		1⊿ O G		In	11		I ANGE.	1 1 5.					9
Min.				Degr	rees.			Min.		gent			rees.		
-	0//	10"	20"	30"	40"	50"	_		0"	10"	20'	30"	40′	50"	
0	10.351417							1	10.372148	2207 2558					
1 2						2040 2381		1 2	2851	2910	2068	3027	3085	3144	57
3						2721		3	3203	3261	3320	3379	3437	3496	56
4	2778	2835	2892	2949	3005	3062	55	4		3613					
5						3403		5		3965					
6						3744		6	4259	4318	4377	4435	4494	4553	53
8	3801	3858	3915	3972	4029	4086	52	7	4012	4670	4729	4788	4847	4900	52
	4143 4484					4427		8	531g	5023 5376	5/35	5/0/	5553	5612	50
10	10 354826							10	10.375670	5720	5788	5847	5006	5065	40
11	5168	5225	5282	5339	5396	5453	48	11	6024	6083	6142	6200	6259	6318	48
12	5510	5567	5624	5681	5738	5795	47	12	6377	6436	6495	6554	6613	6672	47
13	5852	5909	5966	6023	6080	6137	46	13	6731	6790	6849	6908	6967	7026	46
14						6480		14		7144					
15 16	6537 6880							15	7439	7498 7853	7007	7010	8030	8080	44
17	6880 7223							17	81/8	8207	8266	8325	838/	8/1/1	12
18	7566	7623	7680	7737	7795	7852	41	18	8503	8562	8621	8680	8739	8799	41
19	7909	7966	8024	8081	8138	8195	40	19	8858	8917	8976	9035	9094	9154	40
20	10.358253	8310	8367	8425	8482	8539	39	20	10.379213	9272	9331	9390	9450	9509	39
21	8596							21	9568	9627	9687	9746	9805	9864	38
22	8940	8998	9055	9112	9170	9227	37	22	9924	9983	42	.102	.101	.220	37
23 24	9284 9629	9342 9686	9399	0801	0858	9371	35	24	10.380280	0695					
25						.260		25		1051					
	10.360318	0375	0433	0490	0548	0605	33	26		1407					
27	o663	0720	0778	o835	0893	0950	32	27		1764					
28						1295		28	2061	2121	2180	2240	2299	2359	3 r
29						1641	l i	29	2418	2478	2538	2597	2657	2716	30
31	10.361698							30	10.382776	3193	3050	2934	3370	3674	29
32						2332 2678		32	3/01	3550	3610	3670	3720	3780	20
33						3024		33		3908					
34						3370		34	4207	4266	4326	4386	4445	4505	25
35	3428	3486	3543	3601	3659	3717	24	35	4565	4625	4684	4744	4804	4864	24
36						4063		36		4983					
37 38						4410		37		5342					
39						4757 5104		38 39	6000	5701 6060	6120	6180	6240	6200	21
	10.365162								10.38635						
41	5510	5568	5626	5684	5741	5799	18	41	6710	6779	6839	6899	6959	7019	18
42	5857	5915	5973	6031	6089	6147	17	42		7139					
43	6205	6263	6321	6379	6437	6495	16	43	7439	7499	7559	7619	7679	7739	16
44						6843		44		7859					
45 46	0901	0900	7018	7070	7134	7192 7540	14	45 46	8500	8219 8580	8640	8700	8560	8800	14
47						7889				8941					
48	7947	8005	8064	8122	8180	8238	II	48	9241	9302	9362	9422	9482	9542	II
49	8296	8354	8413	8471	8529	8587	10	49	9603	9663	9723	9783	9844	9904	10
50	10.368645	8704	8762	8820	8878	8937	9	50	10.389964	24	85	1.145	.205	.265	9
51	8995	9053	9111	9170	9228	9286	8		10.390326	0386	0446	0507	0567	0627	8
52 53	9344	9403	9461	9319	9578	9636	7	5 ₂		0748					
54	10.370044	9703	0161	0210	0278	0336		54		1472					
55	0304	0453	0511	0560	0628	0686		55	1775	1835	1805	1056	2016	2077	4
56	0745	0803	0862	0920	0978	1037	3	56	2137	2198	2258	2319	2379	2440	3
57						1388		57	2500	2561	2621	2682	2742	2803	2
58				1621			′ I	58	2863	2924	2985	3045	3106	3166	I
59						2090	0	59		3287					
	60" C- 400	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	1	10"	Min.
	Co-tai								Co-ta						
P	Part / -	2" 3"	-		7"		9"	P.	Part J ~	2" 3"	-	-	7"		97
L_	6	12 17	23	29 3	5 40	46	52		6	12 18	3 24	30 3	36 42	48	54

									_						40	
Min.	Si	ine of	68]	Degre	es.			Min.		S	ine of	69]	Degre	ees.		
2	0"	10"	20"	30"	40"	50"	1	N		0"	10"	20"	30"	40"	50"	
0	9.967166	7174	7183	7191	7200	7208	59	0	9	970152	0160	0168	0176	0184	0102	50
1				7242				1		0200	0208	0216	0224	0233	0241	58
2	7268	7276	7285	7293	7302	7310	57	2		0249	0257	0265	0273	0281	0280	57
3	7319	7327	7336	7344	7 353	7361	56	3		0297	0305	0313	0321	0329	0337	56
4				7395				4		o345	o353	0361	0370	0378	0386	55
5	7421	7429	7437	7446	7454	7463	54	5		0394	0402	0410	0418	0426	0434	54
6	7471	7480	7488	7497	7505	7514	53	6		0442	0450	0458	0466	0474	0482	53
7	7522	7531	7539	7547	7556	7564	52	7						0522		
8				7598				8						0570		
9				7649				9		0586	0594	0603	0611	0619	0627	50
10	9.967674							10	9	. 970635	0643	0651	0659	0667	0675	49
11	7725	7733	7742	7750	7758	7767	48	11	1	o683	0691	0699	0707	0715	0723	48
12	7775	7784	7792	7801	7809	7817	47	12	1	0731	0739	0747	0755	0763	0771	47
13	7826	7834	7843	7851	7859	7868	46	13		0779	0787	0795	0803	0811	0819	46
14	7876	7885	7893	7901	7910	7918	45	14						0858		
15	7927	7935	7943	7952	7960	7969	44	15		0874	0882	0890	0898	0906	0914	44
16				8002				16	1	0922	0930	0938	0946	0954	0962	43
17				8053				17	1	0970	0978	0986	0994	1002	1010	42
18				8103				18		1018	1026	1034	1042	1050	1058	41
19				8153				19						1097		
20	9.968178	8187	8195	8203	8212	8220	39	20	9	.971113						
21	8228	8237	8245	8253	8262	8270	38	21	1	1161	1169	1177	1185	1193	1200	38
22	8278	8287	8295	8303	8312	8320	37	22						1240		
23				8354				23						1288		
24				8404				24						1335		
25	8429	8437	8445	8454	8462	8470	34	25						1383		
26	8479	8487	8495	85o3	8512	8520	33	26						1430		
27				8553				27	1	1446	1454	1462	1469	1477	1485	32
28				8603				28						1525		
29				8653				29						1572		
30	9.968678			l. ′ - I					9.	.971588						
31				8752				31						1666		
32				8802				32						1713		
33				8852				33						1761		
34	8877	8885	8893	8901	8910	8918	25	34						1808		
35	8926							35						1855		
36				9000				36						1902		
37	9025	9033	9042	9050	9058	9066	22	37						1949		
38	9075	9083	9091	9099	9108	9116	21	38						1995		
39	9124	9132	9141	9149	9157	9165	20	39						2042		
	9.969173	9182	9190	9198	9206	9215	19		9.	.972058						
41	9223	9231	9239	9247	9256	9264	18	41						2136		
42	9272							42						2183		
43	9321							43						2229		
44	9370	9379	9387	9395	9403	9411	15	44						2276		
45	9420	9428	9436	9444	9452	9461	14	45						2322		
46	9469	9477	9485	9493	9201	9210	13	46						2369		
47	9518	9526	9234	9542	9550	9229	12	47						2416		
48	9567	9575	9583	9591	9599	9608	11	48		2431	2439	2447	2454	2462	2470	11
49	9616	9624	9632	9640	9648	9657	10	49		2478	2485	2493	2501	2508	2516	
	9.969665	9673	9681	9689	9697	9705	9		9.	972524	2532	2539	2547	2555	2563	9 8
51	9714	9722	9730	9738	9746	9754	8	51						2601		
52	9762	9771	9779	9787	9795	9803	7	52		2617	2024	2032	2040	2648	2000	7 6
53	9811	9819	9828	9836	9844'	9852	6	53						2694		
54	9860	9868	9876	9884	9893	9901	5	54		2709	2717	2725	2732	2740	2748	5
55	9909	9917	9925	9933	9941	9949	4	55		2755	2703	2771	2778	2786	2794	4
56	9957 9.970006	9966	9974	9982	9990	9998	3	56		2802	2809	2817	2825	2832	2040	3
57	9.970006	0014	0022	0030	0038	0047	2	57						2878		2
58	0055	0063	0071	0079	0087	0095	I	58						2924		I
59	0103						0	59	_					2970		0
	60"	50"	40"	30"	20"	10"	g l			60"	50"	40"	30″	20"	10"	Min.
	Co-s	sine c	f 21	Degr	ees.	7	Min.			Co-	sine (of 20	Degr	rees.		
73	Paut § 1" 5	2" 3"	4''	5" 6	" 7"	8"	9"	P	D	§ 1"	2" 3"	4"	5" (5" 7 "	8"	9"
Ρ	$\operatorname{Part} \left\{ \begin{array}{l} 1'' \\ 1 \end{array} \right\}$	2 2	3		5 6		7	r.	ra	$\operatorname{irt} \left\{ \begin{array}{c} 1'' \\ 1 \end{array} \right]$	2 2	3	4	5 6	6	7

d	Tangent of 68	Degrees.	l.i	Tangent of 69 Degrees.
Min	0" 10" 20"	30" 40" 50"	Min	0" 10" 20" 30" 40" 50"
0			. 11	10.415823 5886 5948 6011 6074 6137 59
1 2		4136 4197 4258 58 4500 4561 4622 5 ₅		
3		4865 4926 4986 56		المنام المنامة المناسبة
4	5047 5108 5169	5229 5290 5351 55	5 4	7335 7398 7461 7524 7587 7650 55
5		5594 5655 5716 54		1
6		5959 6020 6081 53 6325 6385 6446 52	- 11	0. 10505105 01066-10-510-0015-
8		6690 6751 6812 51		8851 8914 8978 9041 9104 9168 51
9		7056 7117 7178 50		9231 9294 9358 9421 9484 9547 50
11	10.397239 7300 7361	7422 7483 7544 40 7788 7849 7910 48		10.419611 9674 9738 9801 9864 9928 49 9991 54 .118 .181 .245 .308 48
12		8154 8215 8276 4	7 12	10.420371 0435 0498 0562 0625 0689 47
13	8337 8399 8460	8521 8582 8643 46	3 13	0752 0816 0879 0943 1006 1070 46
14		8888 8949 9010 45		
15 16	9071 9132 9194	9255 9316 9377 42 9622 9683 9744 43	1 15	
17		9989 51 . 112 42		
	10.400173 0235 0296	0357 0419 0480 41	1 18	2659 2723 2787 2850 2914 2978 41
19		0725 0787 0848 40		
20	10.400909 0971 1032	1462 1523 1585 38		10.423424 3488 3551 3615 3679 3743 39 3807 3870 3934 3998 4062 4126 38
22		1830 1892 1953 3		
23		2199 2261 2322 36		4573 4637 4701 4764 4828 4892 36
24		2568 2630 2691 35		l réclire de colero les olege los
25 26	3122 3184 3246	2938 2999 3061 32 3307 3369 3430 33	1 25 3 26	
27	3492 3554 3615	3677 3739 3800 32	2 27	
28	3862 3924 3985	4047 4109 4170 31	1 28	
29		4417 4479 4541 30		
31	4073 5035 5007	5158 5220 5282 28		7648 7712 7776 7840 7905 7969 28
32		5529 5591 5653 27		
33		5901 5962 6024 26		8419 8483 8548 8612 8676 8741 26
34 35	6458 6500 6580	6272 6334 6396 25 6644 6706 6768 24	$\frac{5}{4} \frac{34}{35}$	1 0 2 2 2 3 1 1 2 3 4 4 4 4 4 4 4 4 4
36	6820 6801 6053	7015 7077 7139 23	3 36	
37	7201 7263 7326	7388 7450 7512 22	2 37	9965 29 94 . 158 . 223 . 287 22
38	7574 7636 7698	7760 7822 7884 21	38	10.430352 0416 0481 0545 0610 0674 21
39	7946 8008 8070	8132 8195 8257 20 8505 8567 8630 10		0739 0803 0868 0933 0997 1062 20 10.431127 1191 1256 1320 1385 1450 19
41	8692 8754 8816	8878 8940 9003 18	3 41	
42	9065 9127 9189	9252 9314 9376 1	7 42	1902 1967 2032 2097 2161 2226 17
43		9625 9687 9750 16		
44	10.410186 0248 0310	9999 61 . 123 15	5 44 4 45	
46	0560 0622 0685	0747 0809 0872 1	3 46	3458 3522 3587 3652 3717 3782 13
47	0934 0997 1059	1122 1184 1246 1	2 47	3847 3912 3977 4042 4107 4172 12
48	1309 1371 1434	1496 1559 1621 1	48	
49 50	1684 1746 1809	10 0		
51	2434 2497 2559	2622 2684 2747	5 5 1	5407 5473 5538 5603 5668 5733 8
52	2810 2872 2035	2007 3060 3123	7 52	5798 5863 5929 5994 6059 6124 7
53 54		3373 3436 3499 (5 53	
55			5 54 4 55	
56	4314 4377 4440	4502 4565 4628	3 56	7364 7429 7495 7560 7625 7691 3
' 57	4691 4754 4817	4879 4942 5 005 :	2 57	7756 7822 7887 7952 8018 8083 2
58			58	
59	5445 5508 5571 60° 50° 40°	2011 2011 7011	59	600 500 400 300 900 100
	Co-tangent of 2	F		Co-tangent of 20 Degrees.
-	(111 011 011 111	5" 6" 7" 8" 9"	-11	6 1 1 0 1 0 1 1 1 1 0 1 0 1 0 1 0 1
1		31 3 7 43 49 56		Part 6 13 19 26 32 39 45 51 58
_				

_	G: 470 D		G: 4mg D	
Min.	Sine of 72 Degrees.	Min.	Sine of 73 Degrees.	
	0" 10" 20" 30" 40" 50"		0" 10" 20" 30" 40" 50"	1
	9.978206 8213 8220 8227 8234 8241 59		9.980596 0603 0609 0616 0622 0628 56	
I	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	I		8
3	8329 8336 8343 8350 8357 8363 56	3		
4	8370 8377 8384 8391 8397 8404 55	4		5
5	8411 8418 8425 8431 8438 8445 54	5	0789 0795 0802 0808 0815 0821 5	K
6	8452 8459 8465 8472 8479 8486 53	6		
7	8493 8499 8506 8513 8520 8527 52	7		
8	8533 8540 8547 8554 8561 8567 51	8		
9	8574 8581 8588 8594 8601 8608 50	9		
	9.978615 8622 8628 8635 8642 8649 49	11	0 9.980981 0987 0993 1000 1006 1012 4	
II	8655 8662 8669 8676 8682 8689 48	II		
13	8696 8703 8709 8716 8723 8730 47 8737 8743 8750 8757 8764 8770 46	13		
14	8777 8784 8791 8797 8804 8811 45	14		
15	8817 8824 8831 8838 8844 8851 44	15		
16	8858 8865 8871 8878 8885 8892 43	16		
17	8898 8905 8912 8918 8925 8932 42	17		
18	8939 8945 8952 8959 8965 8972 41	18		
19	8979 8986 8992 8999 9006 9012 40	19		
	9.979019 9026 9033 9039 9046 9053 39	11	9.981361 1367 1373 1380 1386 1392 3	
21	9059[9066]9073[9079]9086[9093]38	21	1 .661	
22	9100 9106 9113 9120 9126 9133 37	22		
24	9140 9146 9153 9160 9166 9173 36 9180 9186 9193 9200 9206 9213 35	24		5
25	9220 9227 9233 9240 9247 9253 34	25		
26	9260 9267 9273 9280 9287 9293 33	26		
27	9300 9306 9313 9320 9326 9333 32	27		
28	9340 9346 9353 9360 9366 9373 31	28		
29	9380 9386 9393 9400 9406 9413 30	29		
30	9.979420 9426 9433 9439 9446 9453 29	30		
31	9459 9466 9473 9479 9486 9492 28	31		
32	9499 9506 9512 9519 9526 9532 27	32		
33	9539 9545 9552 9589 9565 9572 26	33		_
34	9579 9585 9592 9598 9605 9612 25 9618 9625 9631 9638 9645 9651 24	34 35		
35 36	9658 9664 9671 9678 9684 9691 23	36		
37	9697 9704 9711 9717 9724 9730 22	37		
38	9737 9743 9750 9757 9763 9770 21	38		
39	9776 9783 9790 9796 9803 9809 20	39	2072 2078 2084 2091 2097 2103 20	0
40	9.979816 9822 9829 9836 9842 9849 19	40	9.982109 2115 2122 2128 2134 2140 10	
41	9855 9862 9868 9875 9881 9888 18	41		
42	9895 9901 9908 9914 9921 9927 17	42		
43	9934 9940 9947 9954 9960 9967 16	43		5
44	9973 9980 9986 9993 9999 6 15 9.980012 0019 0026 0032 0039 0045 14	44		
45	0052 0058 0065 0071 0078 0084 13	46		
47	0091 0097 0104 0110 0117 0123 12	47	2367 2373 2380 2386 2392 2398 15	2
48	0130 0136 0143 0149 0156 0163 11	48	2404 2410 2416 2422 2429 2435 11	1
49	0169 0176 0182 0189 0195 0202 10	49	2441 2447 2453 2459 2465 2471 10	
50	9.980208 0215 0221 0228 0234 0241 9		9.982477 2484 2490 2496 2502 2508	9.
51	0247 0254 0260 0267 0273 0280 8	51		8
52	0286 0293 0299 0306 0312 0318 7	52		7 6
53	0325 0331 0338 0344 0351 0357 6 0364 0370 0377 0383 0300 0306 5	53		5
54	0364 0370 0377 0383 0390 0396 5 0403 0409 0416 0422 0429 0435 4	54		4
56	0442 0448 0454 0461 0467 0474 3	56		3
57	0480 0487 0493 0500 0506 0513 2	57		2
58	0519 0525 0532 0538 0545 0551 1	58	2769 2775 2781 2787 2793 2799	I
59	0558 0564 0571 0577 0583 0590 0	59		0
1	COU TOU 100 000 000 100	1	2011 2011 2011 2011	i
1	Co-sine of 17 Degrees.		Co-sine of 16 Degrees.	
-	(1/1 0/1 0/1 4/1 5/1 0/1 7/1 0/1 0/1	n	Dani (1" 2" 3" 4" 5" 6" 7" 8' 9"	
P.	Part \ \ \begin{pmatrix} 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 & \\ 1 & 1 & 2 & 3 & 3 & 4 & 5 & 5 & 6 \end{pmatrix}	Ρ.	Part \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
L		-		

	Tane	rant a	of 72	Degr	299			ا نہ ا	Tan	gent	of 7 3	Dec	rees.		Γ
F.	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	1
0	10.488224					8582	50	o	10.514661	4736	4812	4887	4962	5038	5
I						9013		ı		5188					
2						9443		2		5641					
3	9515	9587	9659	9731	9802	9874	56	3		6094					
4	9946	18	90	.162	.234	.306	55	4	6471	6547	6623	6698	6774	6849	5
	10.490378	0449	0521	0593	0665	0737	54	5	6925	7001	7076	7152	7228	7303	5.
6						1169		6	7379	7455	7330	7000	7002	7730	5
3						1602 2035		8	7033	7909 8364	8440	8516	8502	8667	5
8						2468		1 1		8819					
9	10.492540							9	10.519199						
ı	2073	3046	3118	3100	3263	3335	48	II	9655	9731	0807	0883	9959	35	4
2	3407	348o	3552	3624	3697	3769	47		10.520111	0187	0263	ó34o	0416	0492	4
3						4204		13	o568	0644	0720	0797	0873	0949	4
4						4638		14	1025	1101	1178	1254	1330	1407	4
5	4711	4783	4856	4928	5001	5074	44	15		1559					
6						5509		16	1941	2017	2094	2170	2246	2323	4
7						5945		17		2476					
8	6018							18		2934					
9	10.496891	6264	0000	7100	0743	6818	30	19	10.523777	3394	3030	4007	6083	1/160	3
I						6792		21	4237	4313	4300	4467	4564	4620	3
2						8130		22		4774					
3						8568		23		5235					
4						9007		24		5696					
5	9080	9153	9226	9299	9372	9445	34	25	608í	6158	6235	6312	6389	6466	3
6	9519	9592	9665	9738	9811	9885	33	26	6543	6620	6697	6774	6 851	6928	3
7	9958	31	.104	.178	.251	.324	32	27	7005	7082	7160	7237	7314	7391	3
8	10.500397							28	7468	7545	7623	7700	7777	7854	3
9						1204		29		8009					
	10.501278								10.528395						
I 2						2086 2527		31 32		8937					
3						2969		33		9401 9866					
4						3411		11	10.530254						
5						3854		35		0798					
6						4296		36	1186	1264	1342	1419	1497	1575	2
7						4740		37	1653	1731	1808	1886	1964	2042	2
8	4814	4887	4961	5035	5109	5183	21	38		2198					
9	5257	5331	5405	5479	5553	5627	20	39		2665					
	10,505701	5775	5849	5923	5997	65-6	19	13 :	10.533055						
I						6516		41		3602					
3	5390	77.70	0739	7058	0007	6961 7407	16	42 43		4070 4540					
4	7/81	7555	7630	770/	7778	7853	T.5	44		5009					
5						8299		45	5401	5479	5558	5636	5715	5703	,
6	8373	8448	8522	8596	8671	8745	13	46	5872	5950	6028	6107	6185	6264	1
7	8820	8894	8060	0043	0118	0102	12	47	6342	6421					
8	9267	9341	9416	9490	9565	9640	11	48	6814	6892	6971	7050	7128	7207	1
9	9714	9789	9863	9938	13	9640 87	10	49	7285	7364	7443	7522	7600	7679) 1
	10.510162	0237	0311	o386	0461	0535	9	5o	10.537758						
1	0610	0685	0760	0834	0909	0984		51	8230	8309	8388	8467	8546	8624	
2	1059	1134	1208	1283	1358	1433	7	52	8703	8782	8801	8940	9019	9098	
3	1000	1002	1007	1732	1807	1882		53	9177	9256	9333	9414	9493	9372	
4 5						2332		54 55	10.540125	9730	9009	0360	19907	0521	1
6	2857	2032	3007	3082	3157	3232	3	56	0600	0679	0758	0837	0017	0006	
7				3533			2	57	1075	1154	123/	1313	1302	1479	
8	3758	3833	3908	3984	4050	4134		58		1630					
9	4209	4285	436o	4435	4510	4586	0	59	2027	2106	2186	2265	2345	2424	
4	60"	50"	40"	30"	20"	10"	-	-	60"	50"	40"	30"	20"	10"	+-
	Co-tai			7 De	grees		Min.		Co-ta	ngent	ــــــــــــــــــــــــــــــــــــــ			J	1
-)		2" 3"			7"		9"	11	Post \$ 1" \$	0			0-200	8"	$\frac{1}{9}$

_i	Si	ne of	74]	Degre	es.			i	Si	ne of	75]	Degre	es.	,	T
Min	0"	10"	20"	30"	40′	50′		Min	0"	10"	20"	30"	40′′	50"	4
	9.982842							0	9.984944	4949	4955	4961	4966	4972	59
1 2				2896 2932				1 2	4970 5011	5017	4989 5023	4995 5028	503/	5000	55
3	2050	2056	2062	2968	2074	2080	56	3	5045	5051	5056	5062	5068	5073	56
4	2986	2992	2998	3óo4	3010	3616	55	4	5079	5084	5090	5096	5101	5107	55
5	3022	3028	3034	3040	3046	3052	54	5	5113	5118	5124	5129	5135	5141	54
6				3076 3112				6				5163			
7 8				3148				8	5213	5210	5224	519 7 5230	5236	52/1	5 T
9				3184				9				5264			
ΙÓ	9.983202	3208	3214	3220	3226	3232	49	10	ς.985280	5286	5291	5297	53o3	5368	49
II				3256				11				5330			
13	3300	3375	3200	3291 3327	3297	3330	47	13				5364 5397			
14	3345	3351	3357	3363	336a	3375	45	14	5414	5410	5425	5430	5436	5442	45
15	3381	3386	3392	3398	3404	3410	44	15	5447	5453	5458	5464	5469	5475	44
16	3416	3422	3428	3434	3440	3446	43	16	5480	5486	5491	5497	5502	5508	43
17	3452	3458	3464	3469	3475	3481	42	17	5514	5519	5525	5530	5536	5541	42
18				35o5 354o				18	5580	5585	5501	5563 5596	5600	5607	41
20	9.983558							19	9.985613						
21				3611				21	5646	5651	5657	5662	5668	5673	38
22	3629	3635	364 r	3647	3653	3658	37	22	5679	5684	5690	5695	5701	5706	37
23				3682				23	5712	5717	5723	5728	5734	5739	36
24 25				3717 3752				24	5745	5750	5750	5761	5707	5972	35
26				3788				25 26	5811	5816	5822	5794 5827	5832	5838	33
27				3823				27	5843	5840	5854	586o	5865	5871	32
28				3858				28	5876	5882	5887	5893	5898	5903	31
29				3893				29	5909	5914	5920	5925	5931	5936	30
	9.983911								9.985942						
31				3963 3998				31	5974	5980	5985 6018	5991 6023	5990	603/	28
3 ₂				4033				33				6056			
34				4068				34				6088			
35	4085	4091	4097	4103	4108	4114	24	35	6104	6110	6115	6121	6126	6132	24
36	4120	4126	4132	4137	4143	4149	23	36				6153			
37	4155	4101	4100	4172	4178	4184	22	37 38	6109	6007	6010	6186 6218	6003	6000	22
38				4207 4242				39	623/	6230	62/5	6250	6256	6261	20
	9.984259							40	9.986266	6272	6277	6282	6288	6293	19
41	4294	4299	43o5	4311	4317	4322	18	41	6299	6304	6309	6315	6320	6325	18
42				4345				42	6331	6336	6342	6347	6352	6358	17
43				4380				43	6363						
44				4414 4449				44				6411 6443			
46	4466	4472	4477	4483	448a	4405	13	46	6459						
47	4500	45o6	4512	4518	4523	4529	12	47	6491	6497	6502	6507	6513	8129	12
48	4535	454o	4546	4552	4558	4563	11	48	6523	6520	6534	6530	6545	655o	II
49	4569	4575	4580	4586	4592	4598		49	6555	65-2	65-0	6571	6600	65.7	
50 51	9.9846o3 4638	4643	4015	4655	4020	4032	8	51	9.986587 6610	662/	6630	6635	66/0	66/6	8
52	4672	4643	4683	4680	460 <i>l</i>	4700	7	52	6651	6656	6661	6667	6672	6677	
53	4706						6	53	6683	6688	6693	6699	6704	6709	6
54	4740	4746	475 I	4757	4763	4768	5	54	6714	6720	6725	6730	6736	6741	5
55	4774						4	55	6746						3
56 57	4808 4840						3	56 57	6778 6809	6815	6820	0794 6825	6831	6836	2
58	4842 4876						I	58	6841	6846	6852	6857	6862	6867	I
59	4910	4916	4921	4927	4932	4938	0	59	6873	6878	6883	6888	6894	6869	0
	60"	50"	40"	30"	20"	10"			60"	50"	40"	30"	20"	10'	d
	Co-	sine o	f 15	Degr	ees.		Min.		Co-	sine d	of 14	Degr	ees.		A
-		2" 3"			" 7"	8"	9"	r	$\operatorname{Part} \left\{ \begin{array}{l} 1^{\prime\prime} \\ 1 \end{array} \right.$	2'' 3'	4"		7'	8"	9"
	Part 3 1	1 2	2		3 4	5	5	ır.	Part \ 1	1 2	2		3 4	4	5

T i	Tan	gent .	of 74	Deg	rees.			ė		Tan	gent	of 75	Deg	rees.		
Min.	0"	10"	20	30"	40"	50"		Min.		0"	10"	20"	30"	40"	50"	_
0									10.	571948	2032 2537					
1 2						$\frac{3378}{3856}$		2		2959	3044	3128	3212	3297	3381	57
3	3936	4016	4095	4175	4255	4335	56	3		3466	3550	3635	3719	3804	3888	56
5						4813 5292		5			4058 4565					
6						5772		6		4989	5073	5158	5243	5328	5413	53
7 8	5852	5932	6012	6092	6172	6252	52	7		5497	5582	5667	5752	5837	5922	52
	6332 6813	6803	6492	6572	6653	6733 7214	51	8			6601					
10	10.547294	7374	7454	7535	7615	7695	49	10	10.	577026						
11	7775	7856	7936	8016	8097	8177	48	11			7622					
13	8237	8820	8001	8081	0062	8659 9142	47	13			8134					
14	9223	9303	9384	9464	9545	9625	45	14		9073	9158	0243	9329	9414	9500	45
15	9706	9787	9867	9948	28	.109	44	15		9585	9671	9756	9842	9928	13	44
17	10.550190					1078		17	10.	580099 0613	0698					
18						1563		18			1213					
19						2049		19			1728					
20	10.552130 2616				1	2000 3021	•	20	10.	582158 2674	2760					
22	3102	3183	3265	3346	3427	3508	37	22		3190	3276	3362	3449	3535	3621	37
23						3995		23			3793					
24 25	4077 4565					4403		24 25		4223	4311	4016	5002	5080	51 7 5	34
26	5053	5135	5216	5298	5379	5461	33	26		5262	5348	5435	5521	56o8	5694	33
27						5950		27			5868				1	1
28						6440 6930		28 29		6821	6387 6908	6005	7081	7168	7255	30
30	10.557012	7093	7175	7257	7339	7421	29	30	10.	587342	7429	7516	7603	7690	7776	29
31	7503	7584	7666	7748	7830	7912 8404	28	31			7950					
33						8896		32 33			8472 8995					
34	8978	9060	9142	9224	9306	9388	25	34		9431	9518	9605	9693	9780	9867	25
35 36	9471	9553 46	9635	9717	9799	9881 .375	24	35	T.O.	9955 590479	0566					
	10.560457							37	10		1091					
38	0952	1034	1116	1199	1281	1364	21	38		1529	1616	1704	1792	1879	1967	21
39	1446 10.561941					1859		39	TO	2055 592581	2142					
41						2850		41	10.		3196					
42	2933	3016	3099	3181	3264	3347	17	42		3636	3724	3812	3900	3988	4076	17
43						3844 4341		43			4252 4781					
45						4839		45			5310					
46	4922	5005	5o88	5172	5255	5338	13	46	•		5840		1 · ·	1	l - ' .	1 1
47 48						5837 6336		47 48			6370 6901					
49	6420	6503	6586	6669	6753	6836	10	40		7344	7433	7522	7610	7699	7788	10
50	10.566920	7003	7086	7170	7253	7337	9	50	10.	597876	7965	8054	8143	8231	8320	9
51 52	7420	7004 8005	7587	8170	7754 8255	7838 8330		51 52		80/9	8498 9031	0120	0200	0208	0387	8
53	8423	8506	8590	8674	8757	8841	6	53		9476	9565	9654	9743	9832	9921	6
54	8925	9008	9092	9176	9260	9343	5		10.	600010	0100	0189	0278	0367	0456	
55 56	9427	9511	9395	9079	9763 .266	.350	. 1	55 56			0635					
57	10.570434	0518	0602	0686	0770	o854		57			1706					
58	0938	1022	1106	1190	1274	1358	I	58			2243					I
59	60"	1527	40"	30"	1779	1803	0	59		60"	2781	2870	30"	3050	3139	
	Co-tai	1					Min.			Co-ta						Min.
P	Part 5 1" 5	2" 3"	4"	5" 6	" 7"	8"	9"	P	Par	, § 1" S	2" 3"	4"	5" 6	" 7"	8" 5	9"
	· · · · · · · · · · · · · · · · · · ·	l€ 25	33	41 4	9 57	65	74	1	ı aı	. 9	17 26	35	43 5	2 61	69 7	78

Min.		ne of						Min.				Degre	es.		
	0"	10"	20"	30"	40"	50"		_	0"	10"	20"	30"	40"	50"	L
0	9.986904	6909	6915	6920	6925	6930	59	0	9.988724						
1	6936	6941	6946	6951	6957	6962	58	1	8753	8758	8763	8768	8772	8777	5
2	6967	6972	6978	6983	6988	6993	57	2	8782	8787	8792	8797	8802	8806	5
3					7019			3	8811	8816	8821	8826	8831	8835	5
4	7030	7035	7040	7045	7051	7056	55	4	8840	8845	885o	8855	886o	8864	5
5	7061	7066	7072	7077	7082	7087	54	5	886g	8874	8879	8884	8880	8803	5
6					7113			6				8913			
7					7144			7				8942			
8	7155	7160	7165	7170	7176	7181	51	8	8056	806r	8066	8970	8075	8080	5
	7186	7101	7106	7202	7207	7212	50	9	8085	8000	800/	8999	000/	0000	15
9	9.987217	7.91	7190	7233	7238	72/3	40	70	9.989014	0018	0994	0999	0033	9009	1/
	9.907217	7222	7220	7266	7269	7240	49		9.909014	9010	0050	9057	9055	9005	14
ΙΙ								II	9042	9047	9032	9037	9002	9000	14
12					7300			12	9071	9070	9001	9085	9090	9093	14
13					7331			13	9100	9103	9109	9114	9119	9124	14
14	7341	7340	7332	7337	7362	7307	45	14	9128	9133	9138	9143	9148	9152	14
15					7393			15	9157	9162	9167	9171	9176	9181	4
16					7424			16				9200			
17					7454			17	9214	9219	9224	9228	9233	9238	4
18	7465	7470	7475	7480	7485	7490	41	18	9243	9247	9252	9257	9262	9266	4
19	7496	7501	7506	7511	7516	7521	40	19	9271	9276	9281	9285	9290	9295	4
	9.987526	7531	7537	7542	7547	7552	39	20	9.989300	9304	9309	9314	9318	9323	3
21					7577			21	9328	9333	9337	9342	9347	9352	3
22	7588	7503	7508	7603	7608	7613	37	22	6 356	6361	6366	9370	0375	9380	3
23					7639			23				9399			
24					7669			24	0/13	0/17	0/122	9427	0/32	0/36	13
25 25					7700			25	9410	04/6	0/50	9455	0460	0464	13
_	7079	7004	7090	7095	7700	7703	33	26	9441	9440	9450	9433	9400	9404	10
26	7710	7713	7720	7723	7730 7761	7733	25	1	9409	9474	9479	9483	9400	9493	2
27	7740	7745	7730	7730	7701	7700	02	27	9497	9302	9507	9511	9510	9321	1
28					7791			28	9525	9530	9535	9539	9544	9549	10
29					7821			29	9553	9558	9563	9568	9572	9277	اا
	9.987832								9.989582						
31.	7862	7867	7872	7877	7882	7887	28	31	9610	9614	9619	9623	9628	9633	2
32	7892	7897	7902	7907	7912	7917	27	32	9637	9642	9647	9651	9656	9661	2
33	7922	7927	7932	7937	7942	7947	26	33	9665	9670	9675	9679	9684	9689	2
34	7953	7958	7963	7968	7973	7978	25	34	9693	9698	9703	9707	9712	9716	2
35	7083	7988	7993	7998	8003	8008	24	35				9735			
36					8033			36	9749	9753	9758	9763	9767	9772	2
37					8063			37	0777	0781	0786	9790	0705	0800	2
38					8093			38	0804	0800	0814	9818	0823	0827	1/2
39					8123			39	0832	0837	08/1	9846	0850	0855	10
49	9.988133	8138	81/3	81/8	8153	8158	10	100	9.989860	086/	0860	0873	0878	0883	
					8183			41	3.959556	0800	0806	9070	9076	9000	J.
41								11 :	9007	9092	9090	9901	3300	3910	
42					8213			42	9913	19919	9922	9929	9955	19900	
43					8242			43	9942	9947	9952	9956	9901	9903	
44					8272			44		9974	9979	9984	9900	9993	1
45	8282	8287	8292	8297	8302	8307	14	45	9997	2			16	20	?[
46					8332				9.990025	10029	0032	10036	0043	0048	2
47					836ı			47	0052	0057	0061	0066	0070	0075)
48		8376	8381	8386	8391	8396	II	48	0079	0084	800	0093	10098	0102	2
49					8420			49				0120			
50	9.988430	8435	8440	8445	8450	8455	9	∥ 50	9.990134						
51	8460	8465	8470	8475	8480	8484	8	51				0175			
52	8480	8404	8400	8504	8509	8514	7	52				0202			
53	8510	8524	8520	8534	8538	8543	6	53				0220			
54					8568			54				0256			
55					8597			55	0270	027	0270	0283	0288	0202	2
56	860-	86+4	86-	8600	8626	863	3	56	02/0	0301	030	0310	0315	0310	
	0007	0012	0017	065	0020	866-			029	0300	0300	3 0337	03/6	0316	3
57					8656			57							
58					8685			58				0364			
59					8714		0	59				0391			1
	60"	50"	40"	30"	20"	10"	ä	H	60"	50"	40"	30"	20"	10"	
	Co	-sine	of 13	Deg	rees.		Min.		Co	-sine	of 12	Deg	rees.		
	$\operatorname{Part} \left\{ \begin{array}{l} 1^{\prime\prime} \\ 1 \end{array} \right.$					0//	9"		(1//				6" 7'	' 8''	1
	_ (1"	2" 3	" 4"	5"	6" 7"	8"	9''	11 -	Part $\begin{cases} 1'' \\ 0 \end{cases}$	2" 3	" 4"	5"	6" 7 '	, 8	"

_				L 0 G	AKI	TH.	NI 1		1 ANGE	N 1 5.					
Mfn.	Tang	gent	of 7 6	Degr	rees.			Min.	Tan	gent	of 77	Deg	rees.		
Z	0"	10"	20"	30"	40"	50"		M	0"	10"	20"	30"	40"	50"	
10	10.603229	3319	3408	3498	3588	3678	59	0	10.636636	6732	6828	6924	7020	7116	59
i	3767	3857	3947	4037	4127	4217	58	1		7309					
2						4756		2	7790	7886	7983	8079	8175	8272	57
3	4846	4936	5026	5116	5206	5296	56	3	8368	8465	8561	8657	8754	885o	56
4	5386	5477	5567	5657	5747	5837	55	4	8947	9043	9140	9237	9333	9430	55
1 5						6378		- 5	9526	9623	9720	9816	9913	10	54
6						6920		6	10.640107						
1 7	7011	7101	7192	7282	7372	7463	52	7		0784					
8						8006		8		1366					
9	8097							9		1948					
	10 So8640	8731	8822	8913	9003	9094	49	1 1	10.642434	2531	2029	2726	2823	2921	49
II	9185	9270	9307	9427	9348	9039	40	II	3010	3115	3213	3310	3407	3303	48
12	9730							12	3002	3700	3797	3093	3992	4090	47
1 .1	10.610276							13		4285					
14	0822							14		4871 5458					
1						1825		15		6045					
16						2373 2922		16	6535	6633	6731	6820	6025	7006	43
17						3471		17		7222					
19						4021		19		7811					
	10.614112							20	10.648303	8402	8500	8500	8607	8706	30
21	4663							21	88n4	8993	1000	0100	0288	0387	38
22						5674		22	0486	9584	6683	9782	9880	9970	37
23						6226			10.650078						
24	6318							24		0770					
25	6871							25		1364					
26						7887		26	1859	1958	2058	2157	2256	2355	33
27	7980	8072	8164	8257	8349	8442	32	27	4455	2554	2653	2752	2852	2951	32
28	8534	8627	8720	8812	8905	8997	31	28		3150					
29	9090	9183	9275	9368	9461	9554	30	29	3647	3747	3846	3946	4046	4145	30
30	10.619646	9739	9832	9925	17	.110	29		10.654245						
	10.620203							31		4943				1 - 1	
32	0761	0854	0947	1040	1133	1226	27	32		5542					
33						1784		33		6142					
34						2344		34		6742					
35						2904		35		7344					
36						3464		36		7946					
37						4025		37	0440	8549	8049	8730	8830	8931	22
4	4119	4213	4300	4400	5056	4587	21	38	9052	9152	9233	9334	9454	9333	21
39		5338	5/3	5505	5610	5150	20	39	10.660261	9757	9037	9930	-665	.100	20
40 41						6277		41		0968					
42						6841		и:		1574					
43						7407		42 43		2182					
44						7972		44	2680	2790	2802	2003	3005	3106	15
45	8067	8161	8256	8350	8444	8539	14	45		3399					
46	8633	8728	8822	8917	9011	9106	13	46		4009					
47	9201	9295	9390	9484	9570	9674	12	47		4620					
48	9768	9863	9958	53	.147	.242	II	48	5129	5231	5333	5435	5537	5630	II
49	10.630337	0432	0527	0622	0716	0811	10	49	5741	5843	5945	6047	6149	6252	10
50	10.630906	1001	1096	1191	1286	1381	9	50	10.666354						
5r						1952		51		7070					8
52		2142	2237	2332	2428	2523	7	52		7684					
53	2618	2713	2809	2904	2999	3095	6	53	8197	8299	8402	8505	8607	8710	6
54	3190	3285	3381	3476	3572	3667	5	54	8813	8916	9018	9121	9224	9327	5
55						4240		55	9430	9532	9635	9738	9841	9944	4
56						4814			10.670047						
57	4910	550-	56-6	5197	5060	5389	2	57		0769					
58	5465	6756	6050	63/0	6444	5964 6540	I	58		1388					
139	60"	50"	40"	30"	20"	10"	-	59	60"	50"	40"	30"			
		1	<u>'</u>	ــــــــــــــــــــــــــــــــــــــ	1		Min.	1					20"	10"	Min.
-	Co-tai						1	<u> </u>	Co-ta	0					1
P	Part / -	2" 3"			" 7"		9"	P	Part / -	2" 3"	-		7"	_	9"
I	. 1 4 1 9	19 28	3 37	46 5	66 65	74	83	11	10	20 30	40	50 C	70	80	90

104			* # O 1			ARI		1			'mo 1				
Min	0"	10"	20"	Degre	es.	50"		Min.	0"	ne of	20"	Degre	es.	50"	
	9.990404						50	-	9.991947				L		50
I				0445				1	1971	1975	1970	1083	1087	1992	58
2	0458	0462	0467	0471	0476	0480	57	2	1996	2000	2004	2008	2012	2016	57
3	0485	0489	0494	0498	0503	0507	56	3						2040	
4				0525				4	2044	2049	2053	2057	2061	2065	55
5				0552				5						2089	
6				o578 o6o5				6						2113	
8				0631				8						2162	
9	0.15			0658				9						2186	
10	9.990671								9.992190						
II				0711				11						2234	
12	0724	0728	0733	0737	0741	0746	47	12						2259	
13				0763				13						2283	
15				0790 0816				14 15						2307	
16				0842				16						2331 2355	
17				0868				17						2378	
18				0895				18						2402	
19	0908	0912	0916	0921	0925	0929	40	19						2426	
20	9.990934	0938	0942	0947	0951	0955	39	20	9.992430						
21				0973				21						2474	
22				0999				22	2478	2482	2485	2489	2493	2497	37
23				1025				23	2501						
24				1051 1077				24 25						2545 2568	
26				1103				26	2572						
27				1128				27						2615	
28				1154				28	2619						
29				1180				29						2662	
30	9.991193								9.992666	2670	2674	2678	2682	2686	29
31				1231				31	2690	269 3	2697	2701	2705	2709	28
32				1257				32	2713						
33				1282				33	2736						
34				1308 1333				35	2759 2783						
36				1359				36						2825	
37				1384				37	2829						
38				1410				38						2871	
39				1435				39	2875						
40	9.991448								9.992898						
41				1486				41	2921						
42	1498	1505	1507	1511	1515	1019	17	42	2944 2967	2940	2932	2930	2900	2963	17
43				1536 1561				43	2907	200/	2008	4979 3002	3005	3000	15
44 45				1586				45	3013	3017	3021	3024	3028	3032	14
46				1612				46	3036	3040	3043	3047	3o51	3055	13
47	1624	1628	1632	1637	1641	1645	12	47	3050	3062	3066	3070	3074	3078	12
48	1649	1653	1657	1662	1666	1670	11	48	3081	3085	3089	3093	3097	3100	11
49				1687			10	49	3104	3108	3112	3115	3119	3123	
	9.991699	1703	1707	1712	1716	1720	9		9.993127	3.52	3134	3138	3142	3140	8
51	1724	1728	1732	1736	1741	1740	8	51 52	3149 3172						
52				1761 1786			7 6	53	3172						7
54				1811			5	54	3217						5
55				1836			4	55	3240	3243	3247	3251	3255	3258	4
56	1848	1852	1856	1860	1865	1869	3	56	3262	3266	3270	3273	3277	3281	3
57	1873	1877	1881	1885	1889	1893	2	57	3284	3288	3292	3296	3299	3303	2
58	1897	1901	1906	1910	1914	1918	I	58	3307						I
59				1934			0	59	3329						0
1	60"	50"	40"	30"	20"	10"	Min.		60"	50"	40"	30"	20"	10"	Min.
				Degr			ì					Degr			
P.	Part /	2" 3"			3" 7"		9"	P.	Part / "	$2'' 3' \\ 1 1$			3" 7 " 2 3	8"	9" 4
	1 1 0	1 1	. 2	2	3 3	_ 	4		1 411 } 0		~		~ 3		*

	Tan	rent :	of 78	Deg	rees			<u> </u>		Tan	gent	of 79	Dem	rees		Г
Min,	0"	10"	20"	30"	40"	50"		Min		0"	10"	20"	30"	40"	50"	
0	10.672525					3043	59	0	10.7	11348	146o	1573	1685		1910	50
1	3147					3666		1	·					2473		
2	3769	3873	3977	4081	4185	4289	57	2						3150		
3	4393	4497	4601	4705	4809	49:3	56	3						3827		
4						5537		4						4506		
5						6163		5						5185		
6	6804	6008	0470	0000	0000	6789 7417	50	6						5866 6547		
78	7521	7626	7731	7835	7012	8045	5 t	8						7230		
9						8674		9						7913		
10						9303		10		8142	8256	8370	8484	8598	8712	40
11	9408	9513	9618	9723	9829	9934	48	11						9283		
	10 680039	0144	0249	o355	o46o	o565	47	12		9512	9627	9741	9856	9970	85	47
13						1197		13	10.7	20199						
14						1830		14						1346		
15						2464		15						2036		
16						3099		16						2726		
17						3735 4371		17 18						3418 4110		
19						5009		19						4804		
20	5115	5221	5328	5434	5540	5647	30	20						5499		
21	5753	586o	5966	6073	6179	6286	38	21						6195		
22						6926		22						6891		
23	7032	7139	7246	7353	7460	7567	36	23						7589		
24	7673	7780	7887	7994	8101	8208	35	24		7822	7938	8055	8171	8288	8405	35
25	8315	8422	8529	8636	8744	8851	34	25						8988		
26						9494		26						9689		
27	10.690246	9709	9610	0568	06=6	.138	32	27	TO 7	1	. 1	' 1		.391		_
29						1430		29	10.7	30625	1/4/6	T563	1681	1798	1016	30
30						2077		30						2503		
31						2724		31						3210		
32						3373		32		3445	3563	3681	3799	3917	4035	27
33	3481	3590	3698	3806	3914	4023	26	33		4153	4271	4389	4507	4625	4744	26
34						4673		34						5335		
35	4782	4890	4999	5107	5216	5325	24	35						6046		
36 37						5977		36						6757		
38	6730	6848	6057	7066	0321	6630 7284	22	$ ^{37}_{38}$						74 7 0 8184		
39	7303	7503	7612	7721	7830	7939	20	39						8899		
40						8595		40		0137	0257	0376	0406	9615	0734	10
41						9252				9854	9973	93	.213	.332	.452	ı 8
42	9362	9471	958 r	9691	9800	9910	17	42	10.7	4ó571						
	10.700020	0129	0239	0349	0459	0569	16		·					1770		
44						1228		44						2490		
45						1889		45		2731	2851	2971	3092	3212	3332	14
46 47						2550								3935		
47 48	3393	3/3/	35//	3655	3765	3213 3876	12	47		4170	5021	51/0	5263	4659 5384	5505	17
49	3087	4007	4208	4310	7420	4540	10	40						6110		
50	4651	4762	4873	4984	5005	5205	9	50		6352	6473	6505	6716	6837	6950	9
51	5316	5427	5538	5649	5761	5872	8	51		708o	7201	7323	7444	7566	7687	8
52	5983	6004	6205	6316	6428	653o	7	52		7809	7930	8052	8174	8295	8417	7
53	6650	6761	6873	6984	7095	7207	6	53		8539	8661	8782	8904	9026	9148	6
54				7653			5	54		9270	9392	9514	9636	9758	9880	5
55	7987	8099	0211	8322	8434	8546	4	55	10.7	50002	0124	0247	0369	0491	0613	4
56 57	8008	0709	0001	8993	9105	9217	3	56						1225		3
	9329	9441	9000	9665	9777	9009	2	57 58						1961	1 .	2
59				1011			I O	59						2697 3435		0
-7	60"	- 50"	40"	30"	20"	10"	-	39		2943	50"	40"	30"	20"	10"	-
							Min.									Min.
	Co-tai	- 11 - 1								Co-tar						
Ρ,	$.\operatorname{Part}\left\{ \begin{array}{ll} 1^{\prime\prime} & 5 \\ 11 & 5 \end{array} \right.$	2// 3// 20 30	-	5" 6			9" 9 7	Ρ.	Part		3//	-	5" 6"			,/ 16
	(11.3	22 32	43	54 6	5 75	80	91			12 2	o 35	47 5	59 70	52	94 10	JO

Min.				Degre				Min.		ine of	81	Degre	es.		
Σ	0"	10"	20"	30″	40"	50"		Z	0"	10"	20"	30"	40"	50"	1
0	9.993351	3355	3359	3363	3366	3370	59	0	9.994620	4623	4627	463o	4633	4637	15
I	3374	3377	3381	3385	3389	3392	58	1	4640	4643	4647	4650	4653	4657	5
2						3414		2	466o	4663	4667	4670	4673	4676	15
3						3437		3	468o	4683	4686	4600	4603	4606	15
4	3440	3444	3448	345i	3455	3459	55	4	4700	4703	4706	4710	4713	4716	5
5	3/62	3466	3470	3473	3477	3481	54	5	1720	4723	4726	4720	4733	4736	5
6						3503		6	4720	4743	4720	4729	4750	4-56	2
						3525		1 1	4759	4745	4740	4749	4/32	4730	2
7						3547		8	4739	4762	4700	4709	4772	4770	10
						356g		I I	4779	4782	4703	4709	4792	4793	2
9								9	4790	4802	4000	4808	4812	4815	2
	9.993572	3270	3330	3383	3307	3391	49		9.994818						
11						3612		II		4841					
12						3634		12		4861					
13						3656		13	4877	4880	4883	4887	4890	4893	4
14						3678		14	4896	4900	4903	4906	4909	4913	4
15	3681	3685	3689	3692	3696	3699	44	15	49-6	49*9	4922	4926	4929	4932	4
ı 6	3703	3707	3710	3714	3717	3721	43	16	4935	4938	4942	4945	4948	4951	4
17	3725	3728	3732	3735	3739	3743	42	17	4955	4958	4961	4064	4068	4071	14
8	3746	3750	3753	3757	3761	3764	41	18		4977					
19	3768	3771	3775	3770	3782	3786	40	19	4003	4997	5000	5003	5006	5000	1
20	9.993789	3703	3707	3800	3804	3807	30	20	9.995013	5016	5010	5022	5025	5020	3
21	3811	381/	3818	3822	3825	3829	38	21	5032	5035	5038	50/1	5045	5048	3
- 1						3850		I I	5057	5054	5050	5061	5066	5060	2
22 23						3872		22	5001	5054	5007	5001	5.02	5.06	2
								23	5070	5073	5077	2000	5005	3000	3
24						3893		24		5092					
25						3914		25	2103	5112	2112	2118	5121	5124	3,
26						3936		26	5127	5131	5134	5137	5140	5143	3
27	3939	3943	3946	3950	3953	3957	32	27	5146	5150	5153	5156	5159	5162	3
28∣						3978		28	5165	5169	5172	5175	5178	5181	3
29						3999		29	5184	5188	5191	5194	5197	5200	3
30	9.994003	4006	4010	4013	4017	4020	29	30	9.995203						
31	4024	4027	4o31	4034	4038	4041	28	31	5222	5225	5228	5232	5235	5238	2
32	4045	4048	4052	4055	4059	4062	27	32	5241	5244	5247	52 5 0	5253	5257	2
33	4066	4069	4073	4076	4080	4083	26	33	5260	5263	5266	5260	5272	5275	2
34						4104		34	5278	5282	5285	5288	5201	5204	2
35						4125		35		5300					
36	4129							36		5319					
37						4167		37		5338					
88						4188		38		5356					
						4209			5370	5375	53-8	538 r	538/	5385	0
39								39							
. 1	9.994212								9.995390						
I						4250		41		5412					
12	4254	4207	4201	4204	4207	427I	17	42	2427	5430	2433	3430	2439	3442	I
13	4274	4278	4281	4285	4288	4292	10	43		5449					
44	4295	4298	4302	4305	4309	4312	10	44	5464	5467	2470	2473	2476	2479	I
45	4316	4319	4322	4326	4329	4333	14	45	5482	5485	5488	3491	5494	5497	I
46	4336	434o	4343	4346	4350	4353	13	46	5501	5504	5507	5510	5513	5516	I
47	4357	436o	4363	4367	4370	4374	12	47	5519	5522	5525	5528	5531	5534	1:
48	4377	4381	4384	4387	4391	4394	ΙI	48	553_{7}	5540	5543	5546	5549	5552	1
10	4308	4401	4404	4408	4411	4415		49	5555	5558	556ı	5564	5567	5570	I
56	9.994418	4421	4425	4428	4432	4435	9	50	9.995573	5576	5579	5582	5585	5588	
51	4438	4442	4445	4448	4452	4455	8	51	5501	5594	5507	56o1	5604	5607	
52	4459	1462	4465	4460	4472	4476	7	52	5610	5613	5616	5610	5622	5625	
53	4479	1/180	1486	4/80	1/102	1406	6	53		5631					
54	4479	4404	4506	4500	45 T 2	1516	5	54	5646	5649	5050	5655	5658	5661	
55	4499	4503	4500	4509	4513	1536			5040 5667	5665	5650	5655	56-5	56-2	
	4519	4023	4520	4330	4555	4550	4	55	5004	5667	560-	56-	56-0	56.6	1
56	4540	4543	4546	4220	4553	4550	3	56	2081	5684	2007	2090	2093	2090	
57	4560	4563	4566	4570	4573	4576	2	57	5699	5702	2702	2708	2711	2714	
58	458o	4583	4587	4590	4593	4597	1	58	5717	5720	5723	5726	5729	5732	
59	4600	46o3	4607	4610	4613	4617	0	59	5 ₇ 35	5738	5741	5744	5747	5750	
	60"	50′′	40"	30"	20"	10"	-		60"	50′′	40"	30"	20"	10"	
	Co	sine	of 9	Degr	ees.		Min.		Co	-sine	of 8	Degr	ees.		Mil
	4 111 6	2" 3'		0	7'' 7''	8"	9"		4 - 11	2" 3"			" 7"	8"	y
	$\operatorname{Part} \left\{ \begin{array}{l} 1^{n-3} \\ 0 \end{array} \right\}$	ം ദ്	4	a: 6	1''	• • • • • • • • • • • • • • • • • • •	9	D	$\operatorname{Part} \left\{ \begin{array}{l} \mathbf{I}^{n-1} \\ 0 \end{array} \right.$	∵ن ن	4	J 0	• •	0	J

	Tane	gent o	of 80	Dem	rees			١.,	Tano	rent.	of 81	Dec	rees		<u> </u>
Min	64	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50"	j
0								0	10.800287	0424	o56o	0696	0833	0969	59
1	4421	4544	4667	4791	4914	5038	58	Ţ	1106	1242	1379	1516	1652	1789	58
2						5779		2	1926	2002	2199	2336	2473 3295	2010	57
3						6522 7266		3 4					4119		
5	7390	7514	7638	7762	7886	8011	54	5	4394	4532	4669	4807	4944	5082	54
6	8135	8259	8384	8508	8633	8757	53	6	5220	5358	5495	5633	5771	5909	53
7						9505		7	6047	6185	6323	6461	6599	6738	52
8	9629 10.760378	9754	9879	0.53	0878	.253	50	8	7706	7014	7102	7291	7429 8261	7208 8300	50
10	1128	1253	1370	1504	1620	1754	40	10	8538	8677	8816	8054	9093	0232	40
11						2507		11	9371	9510	9649	9788	9928	67	48
12						3260			10.810206						
13	3386	3512	3638	3763	3889	4015	46	13	1		- 1	_	1601		
14						4771 5529		14		1	- 1		2440 3280		
16						6287		16					4122		
-	6414	6540	6667	6794	6920	7047	42	17	4403	4544	4685	4825	4966	5107	42
18	7174	7301	7427	7554	7681	7808	41	18					5811		
20	7935 8608	8825	8050	0070	0443	8570 9334	40	19					6658 7506		
21	0461	0580	0716	0844	0071	99	38	20 21	7780	7031	8073	8214	8356	8408	38
i i	10.770227	0354	0482	0610	0737	0865	37	22					9208		
23						1632		23	9492	9634	9776	9918	61	.203	36
24						2401			10.820345						
25						3171 3942		25 26					1772 2630		
27						4715		27					3489		
28	4844	4973	5102	5231	536o	5489	31	28	3776	3920	4063	4207	435o	4494	31
29						6264		29	4638						
30 31						7041		30					6078 6944		
32						7818 8598		31 32					7812		
33	8728	8858	8988	9118	9248	9378	26	33					8681		
34	9508	9639	9769	9899	29	.160	25	34	8971						
	10.780290	0421	0551	0682	0812	0943	24	35					.425		
36 37						1727 2513		30	10.830716				2175		
38						3300		38					3053		
39	3432	3563	3695	3826	3957	4089	20	39					3933		
40	4220	4352	4484	4615	4747	4879	19	40					4814		
41						5670		41					5697 6582		
43						6463 7257		42 43					7468		
44	7389	7522	7654	7787	7919	8052	15	44	7764	7912	8060	8208	8356	85o4	15
45	8185	8317	8450	8583	8716	8849	14	45					9246		
46						9647		46					.138		
47 48	9780 10.790580	9913	08/17	0080	1114	1247	12 []	47	10.840435 1320	1470	1628	1777	1926	2076	12
49	1381	1515	1648	1782	1916	2050	10	49	2225	2375	2524	2674	2823	2973	10
50	2183	2317	2451	2585	2719	2853	9	50	3123	3272	3422	3572	3722	3872	9
51	2987	3122	3256	3390	3524	3658		51					4623		8
52 53	1600	3927 4734	4860	4196	4331	5223	7	52 53					5525 6429		7
54	5408	5543	5678	5812	5047	6082	5	54					7335		5
55	6218	6353	6488	6623	6758	6893	4	55	7637	7789	7940	8091	8243	8394	4
56	7029	7164	7299	7435	7570	7706	3	56	8546	8697	8849	9001	9152	9304	3
5 ₇ 58	7841	7977	8112	8248	8384	8519	2	57	9456	9608	9760	9912	64	.216	2
59	0/17	8791 9607	07/3	0870	9199	9333	0	59	10.850368				0977 1892		I 0
- 79	60"	50"	40"	30"	20"	10"		39	60"	50"	40"	30"	20"	10"	
		ngen					Min.		Co-ta				1		Min.
-		-			2	87 9		-						8" 9	
P.	$. \operatorname{Part} \left\{ \begin{array}{l} 1'' & 5 \\ 13 & 5 \end{array} \right.$	6 39	52	65 78	91 1	103 1	16	Ρ.	Part \ \ \begin{pmatrix} 1'' & 2' \\ 14 & 2! \end{pmatrix}	9 43	58 79	2 86	101 1	15 1	30

ď	S	ine of	82]	Degre	es.			d	s	ine o	f 83	Degre	208		Т
Min.	0"	10"	20"	30"	40″	50"		Min.	0"	10"	20"	30"	40"	50"	-
0	9.995753							0	9.996751	6753	6756	6758	6761	676/	50
1	5771	5773	5776	5779	5782	5785	58	1	6766	6769	6771	6774	6777	6770	158
2	5788	5791	5794	5797	5800	5803	57	2	6782	6784	6787	6789	6792	16705	157
3				5815				3	6797	6800	6802	6805	6807	6810	156
4 5	58/1			5832 5850				4	60-0	6815	6818	6820	6823	6825	55
6	5850	5862	5864	5867	5870	5873	53	5	68/3	6830	60/0	6835	6838	6841	54
7	5876	5870	5882	5885	5888	5801	50	6	6858	6846 6861	6863	6966	686	6856	53
8				5902				8	6874	6876	6850	6881	6887	6006	52
9				5920				9	6880	6891	6804	6806	6800	6000	51
10	9.995928	5931	5034	5037	5040	5043	40	10	9.996904	6006	6000	6012	601/	6017	100
11	5946	5949	5952	5954	5957	5960	48	11	6919	6922	6024	6027	6020	6032	148
12	5963	5966	5969	5972	5975	5978	47	12	6934	6937	6939	6042	6044	6047	47
13	5980	5983	5986	5989	5992	5995	46	13	6949	6952	6954	6957	695g	6062	46
14	5998	6001	6003	6006	6009	6012	45	14	6964	6967	6969	6972	6974	6977	45
15	6015	6018	6021	6023	6026	6029	44	15	6979	6982	6984	6987	6989	6992	44
16				6041				16	6994	6997	6999	7002	7004	7007	43
17				6058				17	7009	7011	7014	7016	7019	7021	42
18	6-00	0009	0072	6075	6078	6081	41	18	7024	7026	7029	7031	7034	7036	41
19	0000	67.03	66	6092	0095	6098	40	19		7041					
20		6100	6100	67.06	6700	6.2	39		9.997053	7056	7058	7061	7063	7066	39
21				6126 6143				21	7008	7071	7073	7070	7078	7080	38
23				6160				22 23	7003	7085	7000	7090	7093	7095	37
24				6177				24	7090	7100	7102	7100	7107	7110	35
25	6185	6188	6101	6193	6106	6100	3/	25	7112	7115 7129	7117	7120	7122	7124	3%
26	6202	6205	6207	6210	6213	6216	33	26	71/1	7144	71/6	71.40	7157	7139	33
27				6227				27	7156	7158	7161	7163	7166	7154	30
28	6235	6238	6241	6244	6246	6240	31	28	7170	7173	7175	7178	7180	7182	31
29	6252	6255	6257	6260	6263	6266	30	29	7185	7187	7100	7102	710/	7107	30
36	g · 996269	6271	6274	6277	628o	6282	20		9.997199	7202	7204	7206	7200	7211	20
31	6285	6288	6291	6293	6296	6299	28	31	7214	7216	7218	7221	7223	7226	28
32	6302	6305	63o7	631 0	6313	6316	27	32	7228	7230	7233	7235	7238	7240	27
33	6318	6321	6324	6327	6329	6332	26	33	7242	7245	7247	7249	7252	7254	26
34	6335							34	7257	7259	7261	7264	7266	7268	25
35	6351	6354	6357	6359	6362	6365	24	35	7271	7273	7276	7278	7280	7283	24
36	6368	6370	6373	6376	6379	6381	23	36	7285	7287	7290	7292	7294	7297	23
37	6384							37	7299	7301	7304	7306	7309	7311	22
38	6400							38	7313	7316	7318	7320	7323	7325	21
39	6417	6/36	6/38	6//1	6444	6445	20	39	7327	7330	7332	7334	7337	7339	20
0	9 996433							41	9.997341	7359	7360	7340	7365	7333	19
2	6465	6468	6/171	6/17/	6/176	6/170	17	42	7360	7358 7372	737/	7376	7300	7307	10
13	6482	6484	6487	6400	6402	6405	16	43	7383	7386	7388	7300	7303	7305	16
14	6498							44	7307	7399	7402	7404	7406	7400	15
15	6514							45	7411	7413	7416	7418	7420	7423	14
16	653o							46	7425	7427	7429	7432	7434	7436	13
17	6546	6549	655ı	6554	6557	6559	12	47	7439	7441	7443	7445	7448	7450	12
18	6562	6565	6567	6570	6573	6575	11	48	7452	7455	7457	7459	7461	7464	11
19	6578	658o	6583	6586	6588	6591	10	49	7466	7468	7471	7473	7475	7477	10
ol	9.996594	6596	6599	6602	6604	6607	9		9.997480	7482	7484	7487	7489	7491	9
I	6610						8	51	7493	7496	7498	7500	7502	7505	8
2	6625						7	52		7509					7
53	6641						6	53		7523					6
54	6657						5	54	7034	7536	7039	7541	7343	7040	5
56	6673						4 3	55 56	7547	7550 7563	7552	7556	7550	7559	4
57	6688						- 11	57	7301	7563	7505	7500	7570	7572	
58	6704						2	58		7577					2 I
59	6720 6735	6738	67/20	67/27	5730	67/8	0	59	7500	7590 7603	7592	7594	7597	7599	0
7	60"	50"	40"	30"	20"	10//		- 9	60"	7003	40"	30"	20"	10"	
-					1	10,	Min.	1						10.	Min.
				Degre						-sine				!	-
	Part $\begin{cases} 1'' & 2 \\ 0 & \end{cases}$	3	4'	5" 6'	7"	8" 9)"		$\operatorname{Part} \left\{ \begin{array}{l} 1'' \\ 0 \end{array} \right\}$	2" 3"	4"	5" 6	" 7"	8	9''

g l	Tan	gent	of 82	Degr	rees.			.ġ	Tan	gent	of 83	Deg	rees.		
Min	0"	10"	20"	30"	40"	50"		Min	0"	10"	20"	30"	40"	50″	1
0	10.852197	2350	2503	2656	2809	2962	59	0	10.910856	1030	1205	1379	1553	1727	5
1			3421					1				2426			
2	4034	4188	4341	4495	4649	4802	57	2	2950	3125	3300	3475	365o	3825	5
3	4956	5110	5263	5417	5571	5725	56	3				4527			
4			6187					4				5581			
5	6804	6958	7113	7267	7422	7576	54	5	6109	6285	6461	6638	6814	6990	5
6			8041					6				7697			
7	866o	8815	8970	9125	9280	9436	52	7	8227	8404	8581	8759	8936	9113	5
8	9591	9746	9902	57	.212	.368	51	8	9290	9468	9645	9823	• • • •	.178	15
9	10.860524	0679	0835	0991	1146	1302	50	9	10.920356						
01			1770					10				1959			
I			2708		l	. <i>' '</i>		II				3031			
12			3647					12				4105			
13			4588					13				5183			
[4]			5531					14				6262			
[5]			6476					15				7345			
6			7423					16				843o			
7			8372					17				9517			
8			9324					18	10.930062						
19	`9959							19	1154	1336	1518	1700	1883	2065	14
0	10.870913							20	2248	2430	2613	2796	2979	3162	13
1:	1870	2029	2189	2349	2508	2668	38	21	3345	3528	3711	3894	4078	4261	13
22			3148					22	4444						
:3			4109					23				6099			
:4			5073					24	6652	6836	7021	7205	7390	7575	3
:5	5716	5877	6o38	6199	636o	6522	34	25				8315			
6			7006					26	8870	9056	9241	9427	9612	9798	13
37	7652	7813	7975	8137	8299	8461	32	27				.541			
8	8623	8785	8947	9109	9271	9433	31	28	10.941100	1286	1472	1659	1845	2032	3
29	9596	9758	9921	83	.246	.408	30	29				2779			
Bo	10.880571	0734	0896	1059	1222	1385	29	30	3341	3528	3715	3902	4090	4277	2
31			1874					31	4465	4653	4841	5028	5216	5404	2
32			2855					32	5593	5781	5969	6157	6346	6534	2
33	3509	3673	3837	4001	4165	4329	26	33	6723	6912	7100	7289	7478	7667	2
34	4493	4657	4821	4985	5150	5314	25	34	7856	8045	8234	8424	8613	88o3	2
35	5479	5643	5808	5972	6137	6302	24	35				9561			
36			6796					36	10.950131						
37			7787					37				1845			
88			8781					38				2991			
39			9776					39				4141			
ίο	10.890441							40				5293			
11	1440	1606	1773	1940	2107	2274	18	41	5870	6063	6255	6448	6641	6834	. 1
12			2775					42	7027	7220	7413	7606	7800	7993	I
13			3779					43	8187	8380	8574	8768	8961	9155	1
4			4786					44	9349	9544	9738	9932	.126	.321	1
[5]	5458	5626	5795	2963	6131	6300	14		10.960515	0710	0905	1099	1294	1489	1
6			6866					46				2270			
7	7481	7650	7819	7988	8157	8326	12	47				3443			
8	8496	8665	8834	9004	9173	9343	II	48	4031	4227	4424	4620	4816	5013	1
19	9513	9683	9852	22	.192	.362		49	5209	5406	5603	5800	5997	6194	1
	10.600532	0702	0873	1043	1213	1384	9	50 51	6391	6588	6785	6983	7180	7377	
I	1554	1724	1895	2066	2236	2407			7575	7773	7971	8169	8367	8565	
2	2578	2749	2920	3091	3262	3433	7	52	8763 9954	8961	9159	9358	9556	9755	
3	3605	3776	3947	4119	4290	4462		53	9954	.152	.351	.550	.749	.948	1
4	4633	4805	4977	5149	5320	5492	5		10.971148	1347	1546	1746	1945	2145	
55			6009				4	55	2345	2545	2745	2945	3145	3345	1
6			7043				3	56	3545	3746	3946	4147	4347	4548	
7			8080				2	57	4749	4950	5151	5352	5553	5755	
8	8772	8946	9119	9292	9466	9639	1	58	5956	6157	6359	6561	6762	6964	
59	9813	9987	.161	.334	.508	.682	o	59	7166	7368	7570	7773	7975	8177	1
4	60"	50"	40"	30"	20"	10"	_	—	60"	50"	40"	30"	20"	10"	┰
1	Co-ta						Min.		Co-ta						1
		// 3//		" 6"		8" 9		 				" 6"		8" 9)"
	Part $\begin{cases} 1'' & 2 \\ 16 & 3 \end{cases}$														

Min.				Degre				Min.	L				Degre			
	0"	10"	20"	30"	40"	50"		!!	L	0"	10"	20"	30"	40"	50′′	
0	9.997614	7617	7619	7621	7623	7625	59	0	9.	998344	8346	8348	8350	8352	8353	50
I	7628	7630	7632	7634	7636	7639	58	1	İ	8355	8357	8359	8361	8363	8364	5
2	7641	7643	7645	7647	7650	7652	57	2		8366	8368	8370	8372	8374	8375	5
3	7654	7656	7658	7661	7663	7665	56	3		8377	8379	8381	8383	8385	8386	5
4	7667	7669	7672	7674	7676	7678	55	4		8388	8390	8392	8394	8395	8307	5
5		7682	7685	7687	7689	7691	54	5		8399	8401	8403	8404	8406	8408	15
6	7693	7696	7698	7700	7702	7704	53	6		8410	8412	8413	8415	8417	8410	5
7	7706	7700	7711	7713	7715	7717	52	7		8421	8422	8424	8426	8/28	8/30	5.
8	7710	7722	7724	7726	7728	7730	5 r	8		8431	8433	8/35	8437	8/130	8440	5
9		7735	7737	7739	7741	77/13	50	9	1	8/1/2	8////	8446	8448	8440	8/51	5
	9.997745	77/17	7750	7752	7754	7756	10	10	0.	998453	8/55	8456	8/58	8/60	8/60	1
11	7758	7760	7762	7765	7767	7760	18	11	3.	8/6/	8465	8465	8469	8/51	8470	14
12	7700	7700	7705	7777	7707	7709	40	!! !	1	8454	8/76	8/-8	8479	8/8-	0 / 02	149
13	7771	7775	7773	7777	7700	7702	47	12		9/95	8/8-	0470	0479	0401	0403	4
	7704	7760	7700	7790	7792	7794	40	13	1	0400	0407	0400	8490	0492	0494	40
14	7797	7799	7001	7803	7803	7007	45	14	ı	8495	0497	8499	8501	8502	8504	45
15	7809	7811	7814	7816	7818	7820	44	15	1	8506	8508	8509	8511	8513	8515	44
16	7822	7824	7826	7828	7830	7833	43	16	ļ				8522			
17	7835	7837	7839	7841	7843	7845	42	17		8527	8529	853o	8532	8534	8535	42
18	7847	7849	7852	7854	7856	7858	41	18		8537	8539	8541	8542	8544	8546	41
19	7860	7862	7864	7866	7868	7870	40	19		8548	8549	8551	8553	8554	85 5 6	40
	9.997872	7875	7877	7870	7881	7883	30			998558	856o	8561	8563	8565	8566	30
21	7885	7887	7880	7891	7803	7805	38	21	'	8568	8570	8572	8573	8575	8577	38
22				7904				22		8578	8580	8580	8584	8585	8587	3.
23				7916				23					8594			
24																
				7929				24					8604			
25	7933	7937	7929	7941	7943	7940	34	25					8614			
26	7947	7949	7951	7953	7955	7957	33	26					8624			
27	7959	7961	7963	7965	7967	7970	32	27					8634			
28	7972	7974	7976	7978	7980	7982	3ı	28		8639	8641	8643	8644	8646	8648	31
29	7984	7986	7988	7990	7992	7994	30	29		8649	865ı	8653	8654	8656	8657	Зс
	9.997996	7998	8000	8002	8004	8006	20		9.	998659						
3:				8014				31	′	18669	8671	8672	8674	8676	8677	28
32				8026				32		8679	868 r	8682	8684	8686	8687	27
33				8038				33		8689	8600	8602	8604	8605	8607	06
34				8050				34		8699	8700	8700	8704	8705	8707	25
35	8056	8058	8060	8062	8064	0034	23	35								
								1 1		8708						
36				8074				36		8718						
37				8086				37					8733			
38				8098				38		8738						
39				8110				39		8747	8749	8750	8752	8754	8755	20
ío	9.998116	8118	8120	8122	8124	8126	19	40	9.	998757	8758	8760	8762	8763	8765	19
11				8133				41	-	8766	8768	8760	8771	8773	8774	18
12	8139	8141	8143	8145	8147	8149	17	42		8776	8777	8779	8781	8782	8784	17
13	8151	8153	8155	8157	8150	8161	16	43		8785	8787	8788	8700	8702	8703	16
14				8168				44		8795	8706	8708	8700	8801	8863	15
5	817/	8176	8178	8180	8182	8184	1/	45		8804	8806	8807	8800	8810	8812	1/
6				8192				46		8813						
								1 1		8823	880%	8826	8805	8800	883-	10
7	0197	2199	0201	8203	9205	0207	12	47		8832						
8				8215				48		8841						
9				8226			- 11	49								- :
	9.998232						9		9.	98851						9
I	8243	8245	8247	8249	8251	8253	8	51		886o						8
2	8255	8257	8258	8260	8262	8264	7	52		8869						7
3	8266	8268	8270	8272	8273	8275	6	53		8878						6
54	8277	8279	8281	8283	8285	8287	5	54		8887	8889	8890	8892	8893	8895	5
55				8294			4	55		8896	8898	8899	8901	8902	8904	4
6				8305			3	56		8905						3
7				8316			2	57		8914						2
8				8328			ı	58		8923						1
9	8333	8335	833-	8339	83/+	83/0	- 11	1		8932						o
'4							0	59								_
-	60"	50"	40"	30"	20"	10"	Min.			60"	50"	40"		20"	10"	Min.
		sine	of 5.	Degre	es.		Z	- 1		Co-	sine	of 4	\mathbf{Degree}	ees.		M
	$Part \begin{cases} 1'' \end{cases}$	2" 3"	4"	5" 6	" 7"	8" \$)"			. (1" 5	2" 3"	4"	5" 6	3" 7"	8"	9"
	Part 3 0	0 1	1	1 1	ı İ		2	P. 1	1'01	·T / "	0 0	î	1		1	1

Г.I	Tand	rant 4	of 84			THE				Tan		of 85	Dea	rees		ī
Min	0"	10"	20"	30"	40"	50"		Min	-	0"	10"	20"	30"	40"	50"	i
0	10.978380							-0	11	.058048						
I						.613		1						.480		
3	10.980817							3		.060968				3416		
4	3268	3472	3677	3882	4087	3063 4293	55	4	1					4891		
5	4498	4703	4909	5114	5320	5526	54	5		5384	563 I	5877	6124	6371	6619	54
6	5732	5938	6144	635o	6556	6763	53	6						7857		
7	6969	7176	7382	7589	7796	8003	52	7						9347		
8	8210	0662	0860	8831	9039	9240 •493	50	8	тт	9043 071342.				23/3		
10	10.990702	0010	1118	1327	1535	1744	40	10	1					3848		
11						2998		ΙφΙ		4351	46o3	4855	5107	5359	5611	48
12						4256		12	ĺ					6875		
13	4466 5728							13	Į					8396		
15	6993	7205	7416	7627	7830	8051	43	14	11	.080432				9922		
16	8262	8474	8686	8898	9111	9323	43	16						2991		
17	9535	9748	9960	.173	.386	.599	42	17	ĺ	3505	3762	4019	4276	4534	4791	42
1	11.000812							18		5049	5307	5565	5823	6082	6340	41
19	2092 3376							19		8754	8/1/	7117	7370 8037	7635 9194	7894 0454	30
20 21	4663							20 21		0715	0075	.236	.407	.758	1020	38
22						7034			11	.091281						
23	7250	7466	7682	7899	8115	8332	36	23						3904		
24	8549	8765	8982	9199	9417	9634	35	24						5485		
25	9851 11.011158							25 26						7072 8665		
27	2468							27		0107	0463	0730	0006	.263	.530	32
28						4881			II	.100797	1065	1332	1600	1868	2136	31
29						6202		29		2404	2672	2940	3209	3478	3747	3o
30	6423							30						5094		
31	7749 9079							31 32						6716 8344		
	11.020414							33						9978		
34	1752	1975	2199	2422	2646	2870	25		11	.110524	0798	1071	1345	1618	1892	25
35	3094							35	l	2167	2441	2715	2990	3265	3540	24
36 37	4440							36						4917		
38						6919 8277		3 ₇ 38		7131	7408	7686	7063	6576 8241	8520	21
39	8504	8731	8958	9185	9412	9640	20	39						9913		
40	9867	95	.322	.550	•778	1006	19		11	. 120471	0751	1031	1311	1591	1871	19
	11.031234	1462	1691	1919	2148	2377	18	41	1					3275		
42 43						3752 5131		42 43						4966 6663		
44	5361	5502	5822	6053	6284	6514	15	44	ĺ					8367		
45	6745	6977	7208	7439	7671	7902	14	45		8936	9221	9506	9792	77	.363	14
46	8134	8366	8598	883o	9062	9295	13		II	.130649	0935	1221	1508	1794	2081	13
47	- 9527	9760	9992	225	.458	.691	12	47						3518		
49	11.040925 2326	2561	2705	3020	326/	3498	II	48						5249 6987		
50	3733	3968	4203	4438	4673	4908	9	50		7567	7858	8140	8440	8731	9023	9
51	5144	5379	5615	5851	6087	6323	8	51		9314	9606	9898	.190	.483	.775	8
52	6559	6795	7032	7268	7505	7742	7		II	.141068	1361	1654	1947	2241	2535	7
53					8928 .356		5	53 54						4007 5779		6 5
	11.050832	1071	1310	1540	1788	2027	4	55						7559		4
56	2266	2506	2745	2985	3225	3465	3	56		8154	8452	8750	9048	9346	9645	3
57	3705	3945	4185	4426	4666	4907	2	57		9943	.242	.542	.841	1141	1440	2
58					6112		1	58	II	.151740						
59		50"	7079	-		7806		59	-					4752		-
	60" Co-ta	1		5 Do	20"	10"	Min.		-	60"	50"	40"	30"	20"	10.7	Mm.
-	Co-ta					OII '	_	-		Co-ta	ingen	t of 4		$\frac{\text{grees.}}{7''}$	ou r	
P	$.\operatorname{Part}\left\{ \begin{array}{l} 1^{\prime\prime} \ 2^{\prime} \\ 22 \ 4 \end{array} \right.$	4 66	88 11	0 132	154	8" ! 177 1	9″ 99	Ρ.	. Pa	$\operatorname{art} \left\{ \begin{array}{l} 1'' \ 2' \\ 27 \ 5' \end{array} \right.$	3 4 1 81 1	08 13)'' 42

ä	Si	ne of	`86]	Degre	es.			i		Si	ne of	87]	Degre	es.		
Min	0"	10"	20"	30"	40"	50"		Min.		0"	10"	20"	30"	40"	50′′	
0	9.998941							0	9.	999404	9406	9407	9408	9409	9410	59
I				8954				I		9411	9412	9413	9414	9415	0416	158
2				8963				2		9418	9419	9420	9421	9422	9423	57
3				8971				3		9424	9425	9426	9427	9428	9430	56
4 5				8980				5		9431	9432	9433	9434	9435	9436	55
6				8989 8997				6		9437	9430	9439	9440	9441	9442	54
7	0993	0003	0005	9006	0007	0000	50	7		0/50	0/51	0/50	0447	0456	9449	50
8	0100	9000	0013	9015	0016	9009	5 T	8		0/156	0/157	0/158	0/150	0/60	9461	5.
9				9023				9		0463	0464	0465	0466	0467	9468	50
10	9.999027	9029	9030	9032	0033	9034	49	10	9	999469	9470	9471	9472	0473	0474	40
11	9036	9037	9039	9040	9041	9043	48	11	_	9475	0476	9477	0478	0470	lo480	48
12	9044	9046	9047	9048	9050	9051	47	12		9481	9482	9483	9484	9485	9486	47
13	9053	9054	9055	9057	9058	9059	46	13		9487	9488	9489	9490	9491	9492	46
14				9065				14		9493	9495	9496	9497	9498	9499	45
15				9073				15		9500	9501	9502	9503	9504	9505	44
16				9082				16		9506	9507	9508	9509	9510	9511	43
17	9080	9087	9088	9090	9091	9092	42	17		9512	9513	9514	9515	9516	9517	42
18	9094	9090	9097	9098	9099	9101	41	18		9518	9519	9520	9521	9522	9523	41
19	9.999110	9103	9103	9106	9107	9109	30	19		9524	9525	9520	9527	9327	9528	40
21				9114				21	9.	999529 9535	0536	0537	0538	0530	05/0	39
22	0126	0128	0120	9130	0132	0133	37	22		9541						
23	0134	0136	0137	9138	01/0	0141	36	23		9547	0548	0540	0550	0551	0552	36
24	0142	9143	0145	9146	0147	0140	35	24		9553	0554	0555	0556	0557	0557	35
25	9150	9151	91 5 3	9154	9155	9157	34	25		9558	9559	9560	9561	9562	0563	34
26	9158	9159	9161	9162	9163	9165	33	26		9564	9565	9566	9567	9568	9569	33
27	9166	9167	9168	9170	9171	9172	32	27		9570	9571	9572	9573	9573	9574	32
28	9174	9175	9176	9178	9179	9180	31	28		9575	9576	9577	9578	9579	9580	31
25	9181	9183	9184	9185	9187	9188	30	29		9581	9582	9583	9584	9585	9586	30
30	399189	9190	9192	9193	9194	9196	29	30	9.9	99586	9587	9588	9589	9590	9591	29
31	9197	9198	9199	9201	9202	9203	28	31		9592						
32	9205	9206	9207	9208	9210	9211	27	32		9597						
33				9216				33		9603	9004	9005	9000	9606	9607	26
34	9220							34		9608	9009	9010	9011	9012	9013	25
35 36	9227	9229	9230	9231	9232	9234	24	35 36		9614	9014	9013	9010	9017	9010	24
37	9235	9230	9237	9239	9240	9241	23	37		9619 9624	0625	0606	0622	0608	9023	20
38	9242							38		9629	0630	0631	0632	0633	063/	22
39	9257							39		9635	0635	0636	0637	0638	0630	20
10	9.999265	0266	0267	0268	0270	0271	10		0.0	99640						
41	9272	0273	0274	9276	0277	9278	18	41	, ,	9645						
42	9279	9280	9282	9283	9284	9285	17	42		9650	9651	9652	9653	9653	9654	17
43	9287	9288	9289	9290	9291	9293	16 l	43		9655	9656	9657	9658	9658	9659	16
44	9294	9295	9296	9297	9299	9300	15	44		9660	9661	9662	9663	9663	9664	15
45	9301	9302	9303	9305	9306	9307	14	45		9665	9666	9667	9668	9668	9669	14
46	9308	9309	9310	9312	9313	9314	13	46		9670	9671	9672	9672	9673	9674	13
47	9315	9316	9318	9319	9320	9321	12	47		9675						
48	9322							48		9680	9081	9081	9082	9083	9084	11
49	9329						- ()	49	^	9685						
50 g	9 999336 9343	03//	9339	03/2	9341	03/6	8	51	9.5	999689 9694						9
52	9350	0351	0353	035/	0355	0356	7	52		9699	9700	9700	0701	0702	0703	
53	9357	0358	0350	0361	0362	0363	6	53		9704						7 6
54	9364	0365	0366	0367	0360	0370	5	54		9708						5
55	9371	9372	9373	9374	9375	9377	4	55		9713	9714	9714	9715	9716	9717	4
56	9371 9378	9370	9380	9381	9382	9383	3	56		9717	9718	9710	9720	9720	9721	3
57	9384	9385	9387	9388	9380	9 390	2	57		9722	9723	9723	9724	9725	9726	2
58	9391	9392	9393	9394	9396	9397	1	58		9726	9727	9728	9729	9729	9730	I
59	9398						0	59		9731	9732	9732	9733	9734	9735	0
1	60"	50"	40"	30"	20"	10"	-			CO"	50"	40"	30"	20"	10"	j
Γ	Co-	sine	of 3	Degre	es.		Min.	Ī		Co-	sine	of 2	Degr	ees.		Min.
- 1																011
	$\operatorname{Part}\left\{ egin{array}{ll} 1^{\prime\prime} & 2 \\ 0 & \end{array} ight.$	2" 3"	4"	5" 6	" 7"	8" !	9"	P. 1	n	. 5 1" 5	2" 3"	4"	5" (5" 7 "	8''	9"

				l O G	ARI	TH	M I	υ 	1	ANGE	N T S.					1
Min.	Tang	gent	of 86	Degr	rees.			Min.			gent	of 87	Deg	rees.		
_	0"	10"	20"	30"	40"	50"				0"	10"	20"	30"	40"	50"	
	11.155356							1	11	.280604						
I				8088				I							5058	
2	11.160837	9300	7/50	9919	206/	2371	56	3		7017	8326	8737	01/17	0558	7507 9970	56
4				3603						.290382	0794	1206	1610	2033	2446	55
5	4520	4838	5147	5457	5766	6076	54	5							4937	
6	6387	6697	7008	7318	7629	7941	53	6							7442	
7				9188				7							9962	
	11.170126	0439	0752	1000	1379	1693	50	1 1	II	.300383						
9	3807	42 I 3	4520	2951 4845	5162	5/178	/in	9		5/71	5807	6325	6752	7180	5044 7608	10
11	5705	6112	6430	6747	7065	7383	48	11		8037	8466	8896	9326	9756	.187	48
12	7702	8020	8339	8658	8977	9797	47		11	.310619	1050	1483	1915	2348	2782	47
13				.577				13							5392	
	11.181539							14		5828	6265	6702	7140	7578	8017	45
15				4440 6384				15		8430					.659	
16	7350	7685	8011	8337	8663	8000	43	17	11						5990	
18				.299				18		5437	6885	7333	7782	8231	8680	41
	11.191283	1611	1940	2269	2598	2928	40	19		9130	9581	32	.483	.935	1387	40
20	3258	3588	3918	4249	4579	4910	39	20	11	.331840	2293	2747	3201	3656	4111	39
21				6237				21							6852	
22				8235				22		7311	7770	8229	8689	9150	9611	37
23	9237			.241				24	11	.340072	3316	3781	1439	1923	5180	35
25				4282				25		5648	6116	6584	7053	7522	7992	3/1
26	5299	5638	5977	6317	6657	6997	33	26		8463	8933	9405	9877	.349	.822	33
27				836i				27	11	.\$51296	1770	2244	2719	3195	3671	32
28	9387	9729	72	.415	.758	1102	3 r	28							6538	
	11.211446							29		7018	7498	7979	8460	8942	9424	30
30 31	5500	5030	6085	4552 6635	6083	3243	29	30							2329	
32				8728				32	**	.362816 57/1/	623/	672/	7215	7707	8199	27
33				.831				33		8692	9185	9679	.173	.668	1164	26
34	11.221886							34	11	.371660	2156	2654	3151	3650	4149	25
35				5068				35		4648	5148	5649	6150	6652	7154	24
36	6134	6489	6845	7202	7558	7915	23	36		7657	8161	8665	9170	9675	.181	23
37	0273 11.230422			9346				38	11	.380687						
39				3667				39		. 6811					6298 0388	
40				5843				40							2501	
41				8030					11	.393022	3544	4066	4589	5113	5637	18
42				.229				42		6161	6687	7213	7740	8267	8795	17
	11.241332							43							1976	
44 45				4659 6891				44	II	.402508					8409	
46				9134				46		8040	0/100	32	57/	7309	1661	13
	11.250260	0636	1012	1389	1766	2143	12	47	11	.412205	2751	3296	3843	4300	4038	12
48	2521	2899	3277	3656	4034	4414	11	48		5486	6036	6586	7136	7688	8240 1566	11
49	4793	5173	5553	5934	6315	6696	10	49		8792	9346	9900	455	1010	1566	10
50	7078	7460	7842	8224	8607	8991	9			.422123	2681	3240	3799	4358	4010	Q
51 52	9374 11.261683	9758	142	.527	3000	1297	8	51 52		2480 2262	0042	0005	7108	7733	8298	
53				5169						.432273	28/3	9997 3/15	308	1133	5134	7
54	6337	6727	7117	7508	7800	8201	5	54		5700	6284	6860	7437	8015	8503	5
55	8683	9075	0467	0860	.254	647	4	55	1	9172	9752	.333	.915	1497	2080	4
56	11.271041	1435	1830	2225	2620	3016	3	56	11	.442664	3248	3834	4420	5007	5505	3
57	3412	3809	4206	4603	5000	5398	2	57	1	6183	6773	7363	7954	8546	9138	2
58	5796	0195	0594	6993	7393	7793	I	58		9732	326	.921	1517	2113	2711	I
59	60"	50"	8990	9397			0	39	11	.453309	3908					o
				30"	20"	10"	Min.		-			40"	30"	20"	10"	Min.
	Co-ta	ıngen	LOI	Deg	rees.	2//		_		Co-ta						
P	. Part $\begin{cases} 1'' & 2' \\ 35 & 69 \end{cases}$	″3″ 0.10∉	4" 5)" 6" 73 905	7"	8″ (ค76 ว)″ 11	P.	.Pa	$\operatorname{trt} \left\{ egin{array}{l} 1^{\prime\prime} & 2^{\prime} \\ 48 & 97 \end{array} ight.$	′3″ ′1./**	4″ 5 10วก	" 6" 49. 90	7"	397 4	35
	(00 0	J 104	100 1	10 201	<i>i</i> -1:0	~10 0				(40 9)	140	100 2	± 230	, ,,,,,,	001 4	

1 2 3 4 5 6 7 8 9 10 11 12 13 14	9·999735 9740 9744	10"	20"	30"			1 1	Min.		ne of					
1 2 3 4 5 6 7 8 9 10 11 12 13 14	9740	9736			40"	50"		L	0′′	10"	20"	30"	40"	50"	
2 3 4 5 6 7 8 9 10 11 12 13	9740 9744	12-1-	9737	9738	9738	9739	59		9.999934	9934	9935	9935	9935	9936	59
3 4 5 6 7 8 9 10 11 12 13		9740	9741	0742	0743	9743	57	1 2	9930	9930	9937	9937	9937 9940	9938	58
5 6 7 8 9 10 11 12 13 14	9748	9749	9750	9751	9751	9752	56	3	9940	9941	9939	9941	9940	9940	56
6 7 8 9 10 11 12 13 14	0753	0753	0754	0755	0756	9756	55	4	9942	9943	9943	9943	9944	9944	55
7 8 9 10 11 12 13 14	9757	9758	9758	9759	9760 9764	9760	54	5	9944	9945	9945	9945	9946	9946	54
9 10 11 12 13 14	9761	9702	9703	9763	9704	9700	53	6	9946	9947	9947	9947	9948	9948	53
9 10 11 12 13 14	0760	9700	9707	0772	9768 9772	9779	51	7 8					9950 9952		
10 11 12 13 14	9774	9774	9775	9776	9776	9777	5o i	9	9952	9953	9953	9953	9953	9954	50
11 12 13 14	9.999778	9778	9779	9780	9780	9781	40	10	9.999954	9954	9955	9955	9955	9956	40
13 14	9782	9782	9783	9784	9784	9785	48	ΙΙ	9956	9956	9956	9957	9957	9957	48
14	9700	9700	9707	9700	9788 9792	9709	47	12 13					9959 9961		
	9794	9794	9795	9792	9796	9797	45	14					9962		
15	9797	9798	9799	9799	9800	9801	44	15	9963	9963	9963	9964	9964	9064	44
16	9801	9802	9803	9803	9800 9804	9804	43	16	9963 9964	9965	9965	9965	9965	9966	43
17	9805	9806	9800	9807	9808	9808	42	17	9966	9966	9967	9967	9967	9967	42
18	9813	0813	0814	081/	9811 9815	0816	41	18	9900	0060	9900	9900	9969 9970	9909	41
20	9.999816	9817	9817	9818	9819	9819	39		9.999971						
21	9820	9820	9821	9822	9822	9823	38	21	9972	9972	9973	9973	9973	9973	38
22	9824	9824	9825	9825	9826	9827	37	22	9973	9974	9974	9974	9974	9975	37
23	9827	9828	9828	9829	9829	9830	36	23	9975	9975	9975	9976	9976	9976	36
24 25	083/	0835	0835	0836	9833 9836	0837	3/	24 25	9970	0078	9977	9977	9977 9978	9977	3/
26	9838	9838	9839	9839	9840	9840	33	26					9980		
27	9841	9842	9842	9843	9843	9844	32	27	9980	9980	9980	9981	9981	9981	32
28					9847			28	9981	9981	9982	9982	9982	9982	31
29	9848	9848	9849	9849	9850	9851	30	29	9982	9983	9983	9983	9983	9983	30
31	9.999851 0854	0855	0856	0856	9857	0857	28	31	9.999983 9085	0085	0085	0085	9985	0085	28
32	9858	9858	9859	9859	9860	9860	27	32	9986	9986	9986	9986	9986	9986	27
33	9861	9861	9862	9863	9863	9864	26	33	9987	9987	9987	9987	9987	9987	26
34	9864	9865	9865	9866	9866	9867	25	34					9988		
35 36	9807	0871	0871	9809	9869 9872	0873	24	35					9989 9990		
37					9875			37					9991		
38	9876	9877	9877	9878	9878	9879	21	38	9991	9991	9991	9992	9992	9992	2 I
39	9879	9880	9880	9881	9881	9882	20	39	9992	9992	9992	9992	9992	9993	20
40 41	9.999882	9883	9883	9884	9884	9883	19	40	9.999993						
42	0888	0880	0880	0800	9890	0801	17	42	9993	0004	0004	0004	9994 9994	0005	17
43	0801	0802	9892	0802	9893	9893	16	43	9995	9995	19995	9995	9995	19995	10
44	9894	9894	9895	9895	9896	9896	15	44	9995	9995	9995	9996	9996	9996	15
45	9897	9897	9898	9898	9898	9899	14	45					9996		
46 47	9099	9900	9900	9901	9901 9904	9902	10	46 47	9990	9990	9997	9997	9997 9997	9997	12
48	9902	9905	9906	9906	9904	9907	11	48	9997	9997	9997	lagas	laggo	9998	II
49	9907	9908	9908	9909	9909	9910	10	49	9998	9998	9998	9998	9998	9998	10
50	9.999910	9910	9911	9911	9912	9912	9	50	9-999998	9998	9998	9998	9998	9998	9
51 52	9913	9913	9913	9914	9914	9915	8	51 52	,,,,				9999		
53	9913	9913	9910	9910	9917 9919	9917	7 6	53					9999 9999		
54	9920	9920	9921	9921	9922	9922	5	54	9999	9999	9999	9999	9999		5
55	9922	9923	9923	9924	9924	9924	4		0.000000	0000	0000	0000	0000	0000	4
56	9925	9925	9926	9926	9926	9927	3	56					0000		
57 58	9927	9927	9928	9928	9929 9931	9929	2. I	5 ₇ 58					0000		
59	9929	9930	9930	9931	9933	9933	0	59					0000		
	60"	50"	40"	30"	20"	10"			. 60"	50"	40"	30"	20"	10"	-
	Co	o-sine	of 1	·	ree.		Mın.			-sine	of 0	Degr	ee.		Min.
10	Part § 1"	2" 3'	4"		5" 7"	8"	9"	n		2" 3	'' 4''	5"	6" 7	8"	9"
r.	$\operatorname{Part} \left\{ \begin{array}{l} 1^{\prime\prime} \\ 0 \end{array} \right.$	0 0	0	0	0 0	0	1	r.	$\operatorname{Part} \left\{ \begin{array}{l} 1^{\prime\prime} \\ 0 \end{array} \right.$	0 (0	0	0 0	0	0

	,		GARITH	1110 111	NGENTS.			11:
Mis.				88 Degrees		F.011		P. Part to 1".
	0"	10"	20"	30"	40"	50"	<u></u>	
0	460553		11.458125 461773	11.458731 462383	11.459338 462995	11.459945 463608	59 58	60.6
1 2	464221	461163 464836	465451	466067	466684		57	61.1 61.6
3	467920	468540	469160	469782	470404	471027	56	62.2
	471651	472276	472902	473528	474156	474785	55	62.7
4 5	475414	476044	476676	477308	477941	478575	54	63.3
6	479210	479846	480482	481120	481759	482398	53	63.8
7 8	483039	48368o	484323	484966	485611	486256	52	64.4
	486902	487549	488198	488847	489497	490148	51	65.0
9	490800	491453	492107	492762	493418	494075	50	65.5
IO	11.494733	11.495392	11.496052	11.496713	11.497375	11.498038	49	66.1
11	498702	499367	500033	500700	501368	502037	48	66.8
12	502707	503378	504051	504724	505398	506073	47	67.4
13	506750	507427	508106	508785	509466	510148	46	68.0
14	510830 514950	511514 •515640	512199 516331	512885 517024	513572 517717	514260 518412	45 44	68.6 69.3
16	519108	519805	520503	521202	521903	522604	43	70.0
17	523307	524010	524715	525421	526128	526837	42	70.7
18	527546	528257	528969	529682	530396	531111	41	71.3
19	531828	532545	533264	533984	534765	535428	40	72.7
20	11.536151	11.536876	11.537602	11.538330		11.539788	39	72.8
21	540519	541251	541984	542719	543455	544192	38	73.5
22	544930	545670	546411	547153	547896	548641	37	74.3
23	549387	550134	550883	551632	552384	553136	36	75.0
24	553890	554645	555401	556159	556918	557678	35	75.8
25	558440	559203	559967	560733	561500	562268	34	76.6
26	563o38 567685	563809 568464	564581	565355	566130 570811	566907	33 32	77.5
27 28	572382	573170	569245 573959	570027 574750	575542	571596 576336		78.3
29	577131	577928	578726	579525	580326	581128	30	80 n
30	11.581932	11.582737	11.583544	11.584353	11.585163	11.585974	29	80.9
3 r	586787	587601	588417	589235	590054	590874	28	81.8
32	591696	592520	593345	594172	595000	595830	27	82.8
33	596662	597495	598330	599166	600004	600844	26	83.7
34	601685	602528	603372	604218	605066		25	84.7
35	606766	607619	608474	609330	610187	611047	24	85.7
36 37	611908 617111	612771	613636 618860	614502	615370 620615	616240	23	86.7
38	622378	617985 623262	624147	619737 625035	625924	621496 626815	22	81.8 88.8
39	627708	628603	629500	630399	631299	632201	20	89.9
40	11.633105	11.634012	11.634919	11.635829	11.636741	11.637655	19	91.1
41	638570	639488	640407	641329	642252	643177	18	92.2
42	644105	645034	645965	646899	647834	648771	17	93.4
43	649711	650652	651595	652541	653488	654438	16	94.6
44	655390	656343	657299	658257	659217	660179	15	95.9
45	661144	662110	663079	664050	665023	665998	14	97.2
46	666975	667055	668936	669920	670907	671895	13	98.5
47 48	672886	673879 679885	674874 680894	675871	676871	677873	12	99.8
49	684954	685975	686998	681905 688024	682919 689052	683935 690083	11	101.3
50		1				,		
5 i	697366	11.692151 698417	11.693189 699470	700526	701584	11.696318 702645	8	104.2
52	703708	704774	705843	706914	707988	709065	7	105.7
53	710144	711226	712311	713398	714488	715581	6	108.0
54	716677	717775	718876	719980	721087	722196	5	110.5
55	723309	724424	725542	726663	727787	728914	4	112 2
56	730044	731176	732312	733451	734592	735737	3	114.0
57 58	736885	738035	739189	740346	741506	742669	2	115.8
58 59	743835 750898	745004 752087	746177	747352	748531	749713	I	117.7
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	10	4.685574	4.685576	15.314424	50					15.314365	
66o		574	576	424		4260			637		
720	- 1	574	577	423	48	4320		543	638	362	2/2
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500		571	583	417		5100					
1560		571	583	417	34	5160		530			
1620		570	584	416		5220		529			
168o		570	584	416		5280		527	670	330	
740		570	585	415		5340		526	672		
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186o		569	587	413		546o		524		324	
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2640		563	599	401		6240		509	707	293	
2700		562	600			6300		507	710	290	
2760	46	562	601	399		636o		5o 6	713	287	
2820		561	602	368	13	6420		505	715	285	
2880	48	561	6o3	397	12	6480	48	503	718	282	
2940		560	604	396	11	6540		502	720	280	
3000	50			15.314395	1 1	1				15.314277	1
306o		559	607	393	9	6660		499	726	274	
3120		558	608	392	8	6720		498	729	271	
3180		558	609	391	7 6	6780		497	731	269	
3240		557	611	389		6840		495	734	266	
3300		556	612	388	5	6900		494	737	263	
336o		556	613	387	4	6960		492	740	260	
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53 691175 701641 712365 723360 734641 746223 6 54 758122 770357 782946 795911 809275 823063 5 55 837304 852027 867267 883061 899452 916485 4 56 934214 952697 972002 992206 13.013395 13.035671 3 57 13.050153 13.083976 13.110305 13.138334 168297 200482 2 58 235244 273032 314425 360183 411335 469327 1 59 536274 615455 712365 837304 14.013395 14.314425 0 60" 50" 40" 30" 20" 10" 6									
54 758122 770357 782946 795911 809275 823063 5 55 837304 852027 867267 883061 899452 916485 4 56 934214 952697 972002 992206 13.013395 13.035671 3 57 13.0505153 13.083976 13.110305 13.138334 168207 200482 2 58 235244 273032 314425 360183 411335 469327 1 59 536274 615455 712365 837304 14.013395 14.314425 0 60" 50" 40" 30" 20" 10" 6								7	
55 837304 852027 867267 883061 899452 916485 4 56 934214 952697 972002 992206 13.013395 13.035671 3 57 13.059153 13.083976 13.110305 13.138334 168297 200482 2 58 235244 273032 314425 360183 411335 469327 1 59 536274 615455 712365 837304 14.013395 14.314425 0 60" 50" 40" 30" 20" 10" file									
56 934214 952697 972002 992206 13.013395 13.035671 3 57 13.059153 13.083976 13.110305 13.138334 168297 200482 2 58 235244 273032 314425 360183 411335 469327 1 69 536274 615455 712365 837304 14.013395 14.314425 0								5	
57 13.059153 13.083976 13.110305 13.138334 168297 200482 2 58 235244 273032 314425 360183 411335 469327 1 59 536274 615455 712365 837304 14.013395 14.314425 0 60" 50" 40" 30" 20" 10" fi					_	899452			1
58 235244 273032 314425 360183 411335 469327 1 59 536274 615455 712365 837304 14.013395 14.314425 0 60" 50" 40" 30" 20" 10"	5-								
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0	000000	017452	034899	052336	069756	087156	104528	121869	139173	156434	6
1	0291	7743	5190	2626	070047	7446	4818	2158	9461	6722	5
2	0582	8034	5481	2917	0337	7735	5107	2447	9749	7009	
3	0873	8325	5772	3207	0627	8025	5396		140037	7296	5
4	1164	8616	6062	3498	0917	8315	5686	3024	0325	7584	5
5	1454	8907	6353	3788	1207	8605	5975	3313	0613	7871	5
6	1745	9197	6644	4079	1497	8894	6264	3601	0901	8158	5
7	2036	9488	6934	4369	1788	9184	6553	3890	1189	8445	
8	2327	9779	7225	466o	2078	9474	6843	4179	1477	8732	
9	2618	020070	7516	4950	2368	9763	7132	4467	1765	9020	
10	002909	020361				090053	107421		142053		
II	3200	0652	8097	5531	2948	0343	7710	5045	2341	9594	
12	3491	0942	8388	5822	3238	0633		5333	2629	9881	
3		1233	8678	- 1	35 ₂₈		7999 8289	5622		160168	4
- 1	3782			6112		0922			2917		
[4]	4072	1524	8969	6402	3818	1212	8578	5910	3205	0455	
5	4363	1815	9260	6693	4108	1502	8867	*6199	3493	0743	
6	4654	2106	9550	6983	4399	1791	9156	6488	3780	1030	4
7	4945	2397	9841	7274	4689	2081	9445	6776	4068	1317	4
8	5236	2687	040132	7564	4979	2371	9734	7065	4356	1604	4
19	5527	2978	0422	7854	5269		110023	7353	4644	1891	4
20	005818	023269	040713	058145	075559	092950	110313	127642	144932	162178	4
1 2	6109	3560	1004	8435	5840	3239	0602	7930	5220	2465	3
22	6399	3851	1294	8726	6135	3529	0891	8219	5507	2752	3
23	6690	4141	1585	9016	6429	3819	1180	8507	5795	3039	3
24	6981	4432	1876	9306	6719	4108	1469	8796	6o83	3326	
25	7272	4723	2166	9597	7009	4398	1758	9084	6371	3613	
26	7563	5014	2457	9887	7299	4687	2047	9373	6659	3900	3
37	7854	5305	2748		7589	4977	2336	9661	6946	4187	
8	8145	5595	3038	0468	7879	5267	2625	9949	7234	4474	3
- 1	8436	5886	3329	0758	8169	5556	2014	130238	7522	4761	3
29		026177				095846			147809	165048	
30	008727			061049			2/200				
31	9017	6468	3910	1339	8749	6135	3492	0815	8097 8385	5334 5621	
32	9308	6759	4201	1629	9039	6425	3781	1103			ı
33	9599	7049	4491	1920	9329	6714	4070	1391	8672	5908	2
34	9890	7340	4782	2210	9619	7004	4359	1680	8960	6195	
35	010181	7631	5072	2500	9909	7293	4648	1968	9248	6482	
36	0472	7522	5363		080199	7583	4937	2256	9535	6769	2
37	0763	8212	5654	3081	0489	7872	5226	2545	9823	7056	
38	1054	8503	5944	3371	0779	8162	5515	2833	150111	7342	2
39	1344	8794	6235	3661	1069	8451	5804	3121	0398	762')	2
40	011635	029085	046525	063952	081359	098741	116093	133410	150686	167916	2
41	1926	9375	6816	4242		9030	6382	3698	0973	8203	
42	2217	9666	7106			9320	6671	3986	1261	8489	I
43	2508	9957	7397	4823		9609		4274	1548	8776	I
44	2799		7688	5113	1	9899	7249	4563	1836	9063	
45	3090	0539	7978	54e3			7537	4851	. 2123	9350	
46	338o	0829	8269			0477	7826	5139	2411	9636	
		1120	8559	5984		0767	8115	5427	2698	9923	
47 48	3671										
48	3962	1411	8850			1346		6004		0496	
49		1702	9140	6564	3968	1040	110000	136292	15356-	1 0 0 0 0 0	1
50		031992			004238	101635					
51	4835			7145	4547		9270	6580			
52			050012								
53						2503					
54							120137				
55											
56	6289		1174	8596	5997	3371	0714	8021			
57							1003	8309	5572		
58						3950	1292		586o	3075	1
59	,						1581				
	89°	88°	87°	86°	8 5 °	84°	83°	82°	81°	80°	†
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D.	D	1	1	1	1	T	1	1	· ·	T	+
۳.	P. 4 85	4.85	4.84	4.84	4.83	4.83	4.82	4.81	4.80	4.78	1

				NATU	RAL	ANG	ENTS.				11
Min	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	
0	000000	017455	034921	052408	069927	087489	105104	122785	140541	158384	
1	0291	7746	5212	2699	070219	7782	5398	3080	0837	8683	
2	0582	8037	5503	2991	0511	8075	5692	3375	1134	8981	
3	0873	8328	5795	3283	0804	8368	5987 6281	3670	1431	9279 9577	56
4 5	1164	8619	6086 6377	3575 3866	1096 1389	8661 8954	6575	3966 4261	1728 2024	9377 9876	55
6	1454	8910 9201	6668	4158	1681	9248	6869	4557		160174	
1	2036	9492	6960	4450	1973	9541	7163	4852	2618	0472	53
7 8	2327	9783	7251	4742	2266	9834	7458	5147	2915	0771	52
9	2618		7542	5033	2558	090127	7752	5443	3212	1069	51
IÓ	002909	020365		055325	072851	090421	108046	125738	143508	161368	50
II	3200	o656	8125	5617	3143	0714	8340	6034	3805	1666	
12	3491	0947	8416	5909	3435	1007	8635	6329	4102	1965	48
13	3782	1238	8707	6200	3728	1300	8929	6625	4399	2263	
14	4072	1529	8999	6492	4020	1594	9223	6920	4696	2562	
15	4363	1820	9290	6784	4313	1887	9518	7216	4993	2860 3159	
16	4654 4945	2111	9581 9873	7076 7368	46o5 4898	2180	9812	7512 7807	5290 5587	3458	
17	5236	2693	040164	7660	5190	2767	0401	8103	5884	3756	
19	5527	2984	0456	7951	5483	3061	0695	8399	6181	4055	
20	005818		040747		075775			128694		164354	
21	6109	3566	1038	8535	6068	3647	1284	8990	6776	4652	
22	6400	3857	1330	8827	6361	3941	1579	9286	7073	4951	38
23	6691	4148	1621	9119	6653	4234	1873	9582	7370	5250	
24	6981	4439	1912	9411	6946	4528	2168	9877	7667	5549	
25	7272	4731	2204	9703	7238	4821	2463	, ,	7964	5848	
26	7563	5022	2495	9995	7531	5115	2757	0469	8262	6147	
27	7854	5313	2787	060287	7824	5408	3052	0765	8559	6446	
28	8145 8436	5604 5895	3078 3370	0579 0871	8116 8409	5702 5995	3346 · 3641	1061 1357	8856 9154	6745 7044	
30	008727	026186	0/3661	061163	078702			131652	149451	r67343	30
31	9018	6477	3952	1455	8994	6583	4230	1948	9748	7642	
32	9309	6768	4244	1747	9287	6876	4525		150046	7941	28
33	9600	7059	4535	2039	9580	7170	4820		o343	8240	
34	9891	7350	4827		9873	7464	5114	2836	0641	8539	26
35	010181	7641	5118		080165	7757	5409	3132	0938	8838	25
36	0472	7933			0458	8051	5704	3428	1236	9137	
37	0763	8224		3207	0751	8345	5999	3725	1533	9437	
38	1054	8515	5993	3499	1044	8638	6294	4021	1831	9736	
39	1345	8806	6284	3791	1336	8932	6588		2129	170035	
40	011636	9388	046576 6867	4375	081629	099226 9519	7178	134613 4909		170334 0634	
42	1927 2218		7159	4667	1922 2215	9319	7473	5205	2724 3022	0034	
43	2509	96 7 9 9970	7450		2508		7768	5502	3319		
44	2800		7742	5251	2801	0401	8063	5798	3617	1532	
45	3091	0553	8033	5543	3094	0695	8358	6094		1831	
46	3382	0844	8325			0989		6390	4213	2131	14
47	3673	1135	8617	6128	3679	1282	8948	6687	4510		
48	3964		8908			1576		6983	4808		
49	4254		9200		4265	1870					
50				067004							1
51	4836								5702	3629	9
5 ₂ 53	5127		050075				0423				
54	5418 5709	1									
55	6 0 00										
56	6291								7192		
57	6582								7490		- 3
58									7788		
59						1 -	1	140244	8086		
	89°	88°	87°	86°	85°	84°	83°	82°	81°	80°	1
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P.	P. 4.85	4.85	4.86	4.87	4.88	4.89	4.91	4.93	4.96	4.98	1-
to .	[", 4000	1 7	1	4/	1 7	4.09	7.9.	4.90	4.90	4.90	1

Min.	10°	11°	12°	13°	14°	15°	16°	17°	18°	19°	
0	173648	190809	207912	224951	241922	258819		292372	309017	325568	60
I	3935	1095	8196	5234	2204	9100	5917	2650	9294	5843	59
2	4221	1380	8481	5518	2486	9381	6197	2928	9570		
3	4508	1666	8765	5801	2769	9662	6476	3206	9847	6393	
4	4794	1951	9050	6085	3051	9943	6756	3484		6668	
5	5080	2237		6368	3333		7035		0400	/	
6	5367	2522	9619	6651	3615	0505	7315			7218	
7	5653	2807	9903	6935	3897	0785	7594				
8	5939	3093			4179	1066	7874	4596	1229	7768	
9	6226	3378	0472	7501	4461	1347	8153	4874	1506	8042	51
10	176512	193664		227784				295152		328317	50
II	6798	3949	1040	8068 8351	5025 5307	1908 2189	8712	5430	2059	8592	49
13	7085	4234 4520	1325 1609	8634	558g		8991	5708	2335	8867	
14	737. 7657	4805	1893			2470	9270	5986	2611	9141	
15		50go	2178	8917	5871 6153	2751 3031	9550	6264	2888	9416	
16	7944 8230	5376	2462	9200 9484	6435	3312	9829 280108	6542 6819	3164 3440		
17	8516	5661	2746	9767	6717	3592	0388	7097	3716		44
18	8802	5946		230050	6999	3873	0667	7375	3992	0514	
19	9088	6231	3315	o333	7281	4154	0946	7653	4269	0789	42
20	179375		213599		247563			297930			
21	9661	6802	3883	0899	7845	4715	1504	8208	4821	1338	
22	9947	7087	4167	1182	8126	4995	1783	8486	5097	1612	
23	180233	7372	4451	1465	8408	5276	2062	8763	5373	1887	
24	0519	7657	4735	1748	8690	5556	2341	9041	5649	2161	36
25	0805	7942	5019	2031	8972	5837	2620	9318	5925	2435	
26	1091	8228	5303	2314	9253	6117	2000	9596	6201	2710	
27	1377	8513	5588	2597	9535	6397	3179	9873	6477	2984	
28	1663	8798	5872	2880	9817	6678		300151	6753		
29	1950	9083	6156	3163		6958	3736	0428	7029	3533	3 1
30	182236		216440	233445	250380	267238		300706	317305	333807	30
31	2522	9653	6724	3728	0662	7519	4294	0983	7580	4081	
32	2808	9938	7008		0943	7799	4573	1261	7856	4355	28
33	3094	200223	7292	4294	1225	8079	4852	1538	8132	4629	27
34	3379	0508	7575	4577	1506	8359	5131	1815	8408	4903	
35	3665	0793	7859	4859	1788	8640	5410	2093	8684		
36	3951	1078	8143	5142	2069	8920	5688	2370	8959		
37	4237	1363	8427	5425	2351	9200	5967	2647	9235	5726	
38	4523	1648	8711	5708	2632	9480	6246	2924	9511	6000	22
39	4809	1933	8995	5990	2914	9760	6525	3202	9786	6274	21
40	185095		219279					303479	320062		
41	5381	2502	9562	6556	3477	0320	7082	3756	0337	6821	
42	5667	2787	9846	6838	3758	0600	7361	4033	0613	7095	10
43	5952		220130	7121	4039		7639	4310	0889	7369	17
44 45	6238 6524	3357 3642	0414	7403 7686	4321 4602	1160 1440	7918 8196	4587 4864	1164	7643	-
46	6810	3927		7060 7 968	4883		8475		1439 1715	7917 8190	
47	7096	4211	1265	7900 8251	5165	2000	8753	5418			
48	7381	4496	1548	8533	5446	2280	9032	5695	1990 2266		
49	7667	4781	1832	8816	5727	256o	9310	5972	2541	9012	
50	187053	205065	222116	230008	256008		289589	3062/0	322816	330285	10
51	8238	5350		9381	6289	3120	9867	6526	3092	9559	
52	8524	5635	2683	9663	6571	3400	290145	•68o3	3367	9832	
53	8810	5920	2967	9946	6852	3679	0424			340106	
54	9095	6204		240228	7133	3959	0702	7357	3917	0380	
55	9381	6489	3534	0510	7414	4239	0981	7633	4193	0653	
56	9667	6773	3817	0793	7695	4519	1259	7910	4468	0927	
57	9952	7058	4101	1075	7976	4798	1537	8187	4743	1200	3
58	190238	7343	4384	` 1357	8257	5078	1815	8464	5018	1473	2
59	0523	7627	4668	164o	8538	5358	2094	8740	5293	1747	
	79°	78°	770	76°	75°	74°	73°	72°	71°	70°	
		,,	.,			Co-sine		12	, .		Min.
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to 1	P. ''.4.77	4.75	4.73	4.71	4.69	4.67	4.65	4.62	4.60	4.57	
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Mip	, <u>, , , , , , , , , , , , , , , , , , </u>	11°	12°	13°	14°	15°	16°	17°	18°	19°	
0	: -327	194380			249328	1		305731		344328	
I		4682		1175	9637	8261	7060	6049	5241	4653	59
2	6927		3165		9946	8573	7375	6367	5563	4978	58
3	7227	5286	3469	1788	250255	8885	7690	6685	5885	5304	
4		5588	3773	2094	o564	9197	8005	7003	6207		
5		5890	4077	2401	0873		8320	7322	6528	5955	55
j 6	3127	6192		2707	1183	9821	8635	7640	685o	6281	54
1 7		6494			1492	270133	8950	7959	7172	6607	53
8	9727	6796		3321	1801	0445	9266	8277	7494		52
9		7099		3627	2111	0757	9581	8596	7817	7259	5 r
10	·	197401	215500	233934			289896	308014	328139	347585	50
11	9628	7703	5903	4241	2729	1382		9233	8461	7911	
12	9928	8005		4548	3039	1694	0527	9552	8783	8237	48
13	70229			4855	3348	2006	0842	9871	9106	8563	
14	0529	8610		5162	3658	2310	1158	310189	9428	8889	46
15	0829	8912		5469	3968	2631	1473	0508	9751	9216	
16		9215		5776	4277	2944	1789	0827	330073	9542	
17	1430	9517		6083	4587	3256	2105	1146	0396	9868	//3
18	1731	9820		6390	4897	3569	2420	1465	0718		10
19	2031	200122		6697	5207	3882	2736	1784	1041	0522	
27	132332	200425			255516				331364		
21	2632		8950	7312	5826	4507	3368	2423	1687	1175	
22	2933	0727 1030		7619	6136	4820	3684	2742	2010	1502	
23	3234	1333	9559		6446	5133	4000	3062	2333	1829	
24	3534	1635		7926 8234		5446		3381	2656	2156	
25	3835		9864		6756		4316				
26		1938	220169	8541	7066	5759	4632	3700	2979	2483	
1	4136 4437	2241	0474	8848	7377	6072	4948	4020	3302	2810	
27 28		2544	0779	9156	7687	6385	5265	4340	3625	3137	
	4737	2847	1084	9464	7997	6698	5581	4659	3949	3464	
29	5038	3149		,977 ¹	8307	7011	5897	4979	4272	3791	31
30	.185339			240079	258618	277325		315299	334595		
31	5640	3755	2000	0386	8928	7638	6530	5619	4919	4446	29
32	5941	4058		0694	9238	7951	6846	5939	5242	4773	
33	6242	4361	2610	1002	9549	8265	7163	6258	5566	5101	
34	6543	4664			9859	8578	7480	6578	5890		
35	6844	4967		1618	260170	8891	7796	6899	6213	5756	
36	7145	5271	3526	1925	o48o	9205	8113	7219	6537	6084	
37	7446	5574	3832	2233	0791	9519	8430	7539	6861	6412	
38	7747	5877		2541	1102	9832	8747	7859	7185	6740	
39	8048	6180	4443	2849	1413	280146	9063	8179	7509	7068	21
40	188349				261723	280460		318500	337833	357396	20
41	865 r	6787	5054	3466	2034	0773	9697	8820	8157	7724	
42	8952	7090	536o	3774	2 345	1087	300014	9141	8481	8052	18
43	9253	7393	5665	4082	2656		0331	9461	8806	838o	
44	9555	7697	5971	4390	2967	1715	0649	9782	9130	8708	
45	9856	8000	6277	4698	3278	2029	0966	320103	9454	9037	
46	190157	8304	6583	5007	3589	2343	1283	0423	9779	9365	
47	0459	8607	6889	5315	3900	2657	1600	0744	340103	9694	13
48	0760	891 i	7194	5624	4211	2971	1918	1065	0428	360022	12
49	1062	9214	7500	5932	4523	3286	2235	1386	0752	o351	
50	191363	209518	227806		264834	283600	302553	321707	341077	360679	
51	1665	9822	8112	6549	5145	3914	2870	2028	1402	1008	9
52	1966		8418	6858	5457	4229	3188	2349	1727	1337	
53	2268	0429	8724	7166	5768	4543	3506	2670	2052	1666	7
54	2570	0733	9031	7475	6079	4857	3823	2991	2377	1995	
55	2871	1037	9337	7784	6391	5172	4141	3312	2702	2324	
56	3173	1341	9643	8092	6702	5487	4459	3634	3027	2653	
57	3475	1645	9949	8401	7014	5801	4777	3955	3352	2982	
58	3777	1949		8710	7326	6116	5095	4277	3677	3312	2
59	4078	2253	0562	9019	7637	643 r	5413	4598	4002	3641	r
-	79°	78°	77°	76°	75°	74°	73°	72°	71°	70°	
	13	,0	,,					12	11	70	Min.
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P. 1	P	ا ہے ہے	, 1	- <u>-</u>	_	_ 1	_				
to 1	5.01	5.05	5.69	5.13	5.17	5.22	5.27	5.33	5.39	5.46	
1	1							1			

	000	0.0	0.50	000	0.0	0.50	000	05.0			-
Min.	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	
0	342020	358368 864o			406737 7002	422618 2882	438371 8633	. ,,	469472	484810	
1 2	2293 2567	8911	4876 5146	0999 1267	7268	3145	8894		9728 9 985	5064 5318	
. 3	2840	9183	5416	1534	7534		9155		470242	5573	
4	3113	9454	5685	1802	7799	3673	9417		0499	5827	56
5	3387	9725	5955	2070	8065	3936	9678	5286	0755	6081	
6	366o	9997	6224	2337	8330	4199	9939		1012	6335	
7	3933		6494	2605		4463		5804	1268	6590	53
8	4206	0540	6763	2872		4726	0462	6063	1525	6844	52
9	4479 344752	0811 361082	7033 377302	3140		4990 425253	0723		1782	7098	
11	5025	1353	7571	3675	9658	5516		6839	2294	487352 7606	
12	5298	1625	7841	3942	9923	5779	1506	7098	2551		
13	5571	1896	8110		410188	6042	1767	7357	2807		
14	5844	2167	8379	4477	0454	6306	2028	7615	3063	8367	
15	6117	2438	8649	4744	0719	6569	2289	7874	3320	8621	45
16	6390	2709	8918	5011	0984	6832	2550	8133	3576	8875	
17	6663	2980	9187	5278		7095	2810	8391	3832	9129	
18	6936	3251	9456	5546	1514	7358	3071	8650	4088	9382	
19	7208 347481	35 22 363793	9725	5813	1779	7621	3332	8908	4344	9636	41
20 21	7754	4064	379994 380263	6347	2310	427884 8147	3853	459166 9425	474000	499399	30
22	8027	4335	0532	6614	2575	8410	4114	9683	5112	0397	
23	8299	4606	0801	6881	2840	8672	4375	9942	5368	0650	37
24	8572	4877	1070	7148	3104	8935		460200	5624	0904	
25	8845	5148	1339	7415	3369	9198	4896	o458	588o	1157	
26	9117	5418	1608	7682	3634	9461	5156	0716	6136	1411	
27	9390	5689	1877	7949	3899	9723	5417	0974	6392	1664	33
28	9662	5960	2146	8215	4164	9986	5677	1232	6647	1917	32
29	9935 350207	6231	2415	8482	4429	430249	5937	1491	6903	2170	31
3ο 3τ	0480		382683 2952		414093		6458	461749	7414		
32	0752	6772 7042	3221	9016 9283	5223	0774 1036	6718	2007 2265	7670	2677 2930	
33	1025	7313	3490	9549	5487	1299	6979	2523		3183	
34	1297	7584	3758	9816	5752	1561	7239	2780	8181		
35	1569	7854		400082	6016	1823	7499	3038	8436	3689	
36	1842	8125	4295	0349	6281	2086	7759	3296	8692		
37	2114	8395	4564	0616	6545	2348	8019		8947	4195	
38	2386	8665	4832	0882	6810	2610	8279	3812	9203	4448	
39	2658 352931	8936	5101 385369	1149	7074	2873	8539			4700	
40 41	3203	9476	5638	1681	7603	433135 3397	9059	4584	9968	5206	
42	3475	9747	5906	1948	7867	3659	9319		480223	5459	18
43	3747		6174	2214		3921	9579	5100	0479		
44	4019	0287	6443	2480	8396	4183	9839	5357	0734	5964	16
45	4291	0557	6711	2747	8660		450098	5615	0989	6217	15
46	4563	0828	6979	3013		4707	0358	5872	1244	6469	
47	4835	1098	7247	3279	9188	4969		6129		6722	
48	5107 5379	1368	7516	3545	9452	5231	0878		1754	6974	
49 50	35565+	1638	7784 388052	3811	9716	5493 435755	1137 451307	466001	2009 182263	7226 497479	
50 51	5g23	2178	8320	404070	419900	6017	1656	7158	2518	7731	
51 52	6194			4610		6278				7983	8
53	6466			4876	ı			7673	3028	8236	
54	6738	2988	9124	5142					3282	8488	6
55	7010	3258	9392					8187	3537	8740	
56	7281	3528	9660	5673					3792	8992	
57	7553	3797							4046		
58	7825	4067				7848 8110			4301 4555	9496 9748	2 I
59	8096	4337	0463		2355	(9215			1
	69°	68°	67°	66°	65°	64°	63°	62°	61°	60°	Min.
7	D		T		Natural	Co-sine	g.	I		· · · · ·	-
P. to 1	P. 4.54	4.51	4.48	4 45	4.41	4.38	4.34	4.30	4.26	4.22]

	1			NATU	KAL		ENTS.				
Min.	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	
. 0	363970	383864		424475	445229	466308		509525	531709	554309	60
1	4300	4198	4365	4818	5577	6662	8093 8453	9892 510258	2083 2456	4689 5070	59
3	4629 4959	4532 4866	4703 5042	5162 5505	5926 6275	7016 7371	8813	0625	2829	5450	
4	5288	5200	5380	5849	6624	7725	9174	0992	3203	5831	
5	5618	5534	5719	6192	6973	8080	9534	1359	3577	6212	
6	5948	5868	6058	6536	7322	8434	9895	1726	3950	6593	54
7	6278	6202	6397	6880	7671	8789		2093	4324	6974	
8	6608	6536	6736	7224	8020	9144	0617	2460	4698	7355	
9	6938	6871 387205	7075	7568	8369	9499 469854	0978 491339	2828 513195	5072 535446	7736 558118	
10	367268 7598	7540	7753	427912 8256	9068	470200	1700	3563	5821	8499	
12	7928	7874	8092	8601	9418	0564	2061	3930	6195	8881	
13	8259	8209	8432	8945	9768	0920	2422	4298	6570	9263	
14	8589	8544	8771	9289	450117	1275	2784	4666	6945	9645	
15	8919	8879	9111	9634	0467	1631	3145	5034	7319		
16	9250	9214	9450	, 9979	0817	1986	3507	5402	7694	0409	
17	9581	9549		430323	1167	2342	3869	5770 6138	8069 8445	0791	
18	9911 370242	9884 390219	410130	0668	1517 1868	2698 3054	4231 4593	6507	8820	1174	42
19	370573		410810			473410		516875	539195		
21	0904	0889	1150	1703		3766	5317	7244	9571	2322	39
22	1235	1225	1490	2048	2919	4122	5679	7613	9946	2705	38
23	1566	156o	1830	2393	3269	4478	6042	7982	540322	3088	
24	1897	1896	2170	2739	3620	4835	6404	8351	0698	3471	
25	2228	2231	2511	3084	3971	5191	6767	8720	1074	3854	
26	2559 2890	2567	2851 3192	3430 3775	4322 4673	5548 5905	7130 7492	9089 9458	1450 1826	4238 4621	
27 28	3222	2903 3239	3532	4121	5024	6262	7855	9828	2203	5005	
29	3553	3574	3873	4467	5375	6619		520197	2579	5389	
30	373885	393910	414214		455726			520567	542956		30
31	4216	4247	4554	5158	6078	7333	8945	0937	3332	6157	
3z	4548	4583	4895	5504	6429	7690	9308	1307	3709	6541	
33	4880	4919 5255	5236	5850	6781	8047	9672	1677	4086	6925	
35	5211 5543	5592	5577 5919	6197 6543	7132 7484	8405 8762	500035 0399	2047 2417	4463 4840	7310 7694	
36	5875	5928	6260	6889	7836	9120	0763	2787	5 ₂₁₈	8079	
37	6207		6601	7236	8188	9477	1127	3158	5595	8464	
38	6539	6601	6943	7582	8540	9835	1491	3528	5973	8849	
39	6872	6938	7284	7929	8892		1855	3899	635o	9234	21
40	377204		417626		459244					569619	20
41	7536		7967	8622	9596	0909		4641	7106	570004	
42	7869 8201	7948 8285	8309 8651	8969 9316	9949 460301	1267		5012 5383	7484 7862	0390 0776	
44	8534		8993	9663	0654			5 ₇ 54	8240	1161	
45	8866	1	9335	440011	1006	1		6125	8619	1547	
46	9199		9677	0358	1359		4406	6497	8997	1933	14
47	9532		420019	0705	1712	3060	4771	6868	9376	2319	
48	9864		0361	1053	2065			7240	9755	2705	
49				1400			5502	7612			II
50	0863	400646 0984	1389					527984 8356	550513 		(
52								8728		_	
53									1650		
54	1863	1997	2417		4185	5574	7329	9473	2030	5026	6
55				3487	4538			9845	2409		5
56								530218			
57	2863 3197		1					0591	3169		ł
59											
1 59	69°	680	67°	66°	65°	64°	63°	62°	61°	60°	1
	09-	1 00	07-					02	01.	60-	Min.
				Na	tural C	o-tange	nts.				Z
P.	P. 5.53	5.60	5.68	5.76	5.85	5.95	6.05	6 16	6.28	6.40	
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4	963	0.10	060	000	0.10	0.50	0.00	050	000	000	1
Min	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	
0		515038	529919	544639	559193 9434	573576	587785 8021		615661	629320	
1 2	0252 0504	5287 5537	530166 0413	4883 5127	9434	3815 4053	l .	2047 2280	5891 6120	9546 9772	
3	0756	5786		5371	9916	4291	8491	2512	6349	9998	57
4	1007	6035		5615		4529				630224	
5	1259	6284	1152	5858	0398	4767	8961	2976	6807	0450	55
6	1511	6533	1399	6102	0639		9196		7036	0676	
7	1762	6782	1645	6346		5243	9431	3440	7265	0902	
8	2014	7031	1891 2138	6589 6833	1121 1361	5481	9666	3672	7494	1127	
9	2266 502517	7280 517529				5719 575957	9901 500136	3904 604136	7722 617051	631578	
11	2769	7778	2630	7320	1843	6195	0371	4367	8180	1804	40
12	3020	8027	2876	7563	2083	6432	0606	4599	8408	2020	
13	3271	8276	3122	7807	2324	6670	0840	483í	8637	2255	
14	3523	8525	3368	8050	2564	6908	1075	5062	8865	2480	
15	3774	8773	3615	8293	2805	7145	1310	5294	9094	2705	
16	4025	9022	3861	8536	3045 3286	7383	1544	5526	9322	2931	
17	4276 4528	9271 9519	4106 4352	8780 9023	35 ₂ 6	7620 7853	1779 2013	5757 5988	9551	_3156 3381	
19	4779	9768	4598	9266		8095	2248		9779 620007	3606	
20	505030	520016	534844	549509			592482		620235		
21	5281	0265	5090	9752	4247	8570	2716	6682	o464	4056	
22	5532	0513	5335	9995	4487	8807	2951	6914	0692	4281	
23	578 3	0761	5581	550238	4727	9044	3185	7145	0920	4506	
24	6034	1010	5827	0481	4967	9281	3419	7376		4731 4955	
25 26	6285 6535	1258 1506	6072 6318	0724 0966	5207 5447	9518 9755	3653 3887	7607 7838	1376 1604	518o	
27	6 ₇ 86	1754	6563	1200		9992	4121	8069	1831	5405	
28	7037	2002	6809	1452	5927		4355	8300	2059	5629	
29	7288	2251	7054	1694	6166	o466	4589	8531	2287	5854	31
30	5.07538	522499	537300	551937		580703				636078	
31	7789	2747	7545	2180	6646	0940	5057	8992	2742	6303	
32	8040	2995	7799	2422	6886	1176	5290	9223	2970	6527	
33	8290 8541	3242	8035 8281	2664	7125 7365	1413 1650	5524 5758	9454 9684	3197 3425	6751 6976	
35	8791	3490 3738	8526	2907 3149	7604	1886	5991	9915	3652	7200	
36	9041	3986	8771	3392	7844	2123	6225		388o	7424	
37	9292	4234	9016	3634	8083	2359	6458	0376	4107	7648	23
38	9542	448 r	9261	3876		2596	6692	0606	4334	7872	
39	9792	4729	9506	4118		2832	6925	0836	4561	8096	
40	510043	524977	539751			583069 3305	597159		624789 501 6	638320 8544	
41 42	0293 0543	5224 5472	9996 540240	4602 4844	9040 9280	3541	7392 7625	1297 1527	5243	8768	
43	0793	5719	0485	5086	9519	3777	7858	1757	5470	8992	
44	1043	5967	0730	5328	9758	4014	8092	1987	5697	9215	
45	1293	6214	0974	5570	9997	4250	8325	2217	5923	9439	
46	1543	6461	1219	5812	570236	4486	8558	2447	6150		
47	1793	6709	1464	6054	0475	4722	8791	2677	6377	9886	
48	2043	6956	1708	6296	0714	4958	9024	2907 3137	66o4 683o	640110 o333	
49 50	2293	7203	1953 542197	6537	0952	585/20	9256 500/80	61336			
51	2792	7697	2442	7021	1430	5665	9722	3596	7284	0780	9
52	3042	7944	2686	7262	1669	5901	9955	3826	7510	1003	
53	3292	8191	2930	7504	1907		600188	4056	7737	1226	7
54	3541	8438	3174	7745	2146	6372	0420	4285	7963	1450	
55	3791	8685	3419	7987	2384	6608	0653	4515	8189	1673	
56	4040	8932	3663	8228	2623	6844	0885	4744	8416 8642	1896 2119	
57 58	4290 4539	9179	3907 4151	8469 8710	2861 3100	7079 7314	1118 1350	4974 5203	8868	2342	
59	4789	9426 9673	4395	8952	3338	7550	1583	5432	9094	2565	
-	59°	58°	57°	56°	55°	54°	53°	52°	51°	50°	
	0.0	9 0	01			Co-sines		0.5	· ·		Min.
P. 1	P. ,	4 - 2	4 00					3.85	3.80	3.74	
to 1	P. 4.18	4.13	4.09	4.04	4.00	3.95	3.90	3.63	3.00	0.74	

			4	NATU	KAL	IANG	ENTS.				12
Min	30°	31°	32°	33°	34°	35°	36°	37°	38°	39°	
0	577350	600861	624869	649408	674500	700208	726543	753554	781286	809784	60
I	7738	1257	5274	9821	4932	0641	6987	4010	1754	810266	
2	8126	1653	5679	650235	5355	1075	7432	4467	2223	0748	58
3	8514	2049	6083	0649	5779	1509	7877	4923	2692	1230	
	8903	2445	6488	1063	6203	1943	8322	538o	3161	1712	56
. 4	9291	2842	6894	1477	6627	2377	8767	5837	3631	2195	55
6	9680	3239	7299	1892	7051	2812	9213	6294	4100	2678	
7	580068	3635	7704	2306	7475	3246	9658	6751	4570	3161	53
8	0457	4032	8110	2721	7900	3681		7209	5040	3644	52
9	o846	4429	8516	3136	8324	4116	0550	7667	5510	4128	51
ΙÓ	581235	604827	628921	65355 г	678749	704551	730996	758125	785981	814612	5e
11	1625	5224	9327	3966	9174	4987	1443	8583	6451	5096	
12	2014	5622	9734	4382	9599	5422	1889	9041	6922	558o	48
13	2403	6019		4797	680025	5858	2336	9500	7394	6065	47
14	2793	6417	o546	5213	0450	6294	2783	9959	7865	6549	46
15	3183	6815	0953	5629	0876	6730	3230	760418	8336	7034	
16	3573	7213	136o	6o45	1302	7166	3678	0877	8808	7519	44
17	3963	7611	1767	6461	1728	7603	4125	1336	.9280	8005	
18	4353	8010	2174	6877	2154	8039	4573	1796	9752	8491	
19	4743	8408	2581	7294	2580	8476	5021	2256	790225	8976	
20	585134	608807	632088	657710					790697		
21	5524	9205	3396	8127	3433	9350	5917	3176	1170	9949	
22	5915	9604	3804	8544	386o	9788	6366	3636	1643		
23	6306	610003	4211	8961	4287	710225	6815	4097	2117	0922	
24	6697	0403	4619		4714	0663	7264	4558	2500	1409	
25	7088	0802	5027	9796	5142	1101	7713	5019	3064	1897	
26	7479	1201	5436		5569	1539	8162	5480	3538	2384	
- 1	7479	1601	5844	0631	5997		8611	5941	4012	2872	
27 28	8262		6253		6425	1977	9061	6403	4486	336o	
- 1	8653	2001		1049		2416 2854					
29		2401 612801	6661	661886	6853		9511	6865	4961	3848	
30	589045					713293			795436	024330	30
31	9437	3201	7479	2304	7709	3732		7789	5911	4825	
32	9829	3601	7888	2723	8138	4171	0862	8252	6386		
33	590221	4002	8298	3141	8567	4611	1312	8714	6862	5803	
34	0613	4402	8707	356o	8595	5050	1763	9177	7337	6292	
35	1006	4803	9117	3979	9425	5490		9640	7813	6782	1 .
36	1398	5204		4398	9854	5930		770104	8290		
37	1791	5605	9937		690283	6370	3117	0567			
38	2184	6006		5237	0713	6810	3569	1031	9242		
39	2577	6408	0757	5657	1143	7250		1495	9719	8743	
40	592970	616809	641167	666077	691572		744472		800196		
41	3363	7211	1578	6497	2003	8132	4925	2423	0674	9725	
42	3757	7613		6917	2433	8573	5377	2888	1151	830216	1
43	4150	8015		7337	2863	9014	5830	3353	1629		
44	4544	8417	2810	7758	3294	9455	6282	3818	2107	1199	
45	4937	8819	3222	8179	3725	9897	6735	4283	2585	1691	
46	5331	9221	3633	8599		720339	7189	4748	3063		
47	5725	9624	4044	9020	4587	0781	7642	5214	3542	2676	
48	6120		4456	9442	5018	1223	8096	5680	4021	3169	
49	6514	0429	4868	9863	5450	1665	8549	6146	4500		
50	596908	620832	645280						804979	834155	
51	7303	1235		0706	6313		9458	7078	5458	4648	
52	7698	1638		1128	,	2993	9912	7545	5938	5142	
53	8093	2042	i	1550			750366	8012	6418		
54	8488	2445		1972	7610			8479	6898	6130	
55	8883	2849		2394		4323		8946	7379		
56	9278	3253		2817		4766		9414	7859	7119	4
57	9674	3657		3240		5210		9881	8340	7614	3
58			8581	3662	9341	5654	2642		8821	8109	
59	o465	4465	8994	4085		6098	3098	0817	9303		
	5 9°	58°	57°	56°	55°	54°	53°	52°	51°	50°	
			1		l	o-tange			-01	1	Win.
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P. to 1	P. 6.53	6.67	6.82	6.97	7.14	7.31	7.50	7.70	7.92	84	

Min.	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	
0	642788	656059	1		694658		<u> </u>	1			160
1	3010			2211	4868	7312	9542	1552	3339	754710	1 .
2	3233			2424		7518		1750			
3	3456				5286		1 77.53	1949	3728		
4	3679			2849			720148	2147	3923	5472	56
5	3901	7156	670211	3061	5704		0349	2345	4117		
6	4124	7375	0427	3274	5913	8340	0551	2543	4312		
7	4346			3486	6122	8545	0753	2741	4506		
8	4569	7814	0858	3698	633o	8750		2939	4700	6234	
9	4791	8033	1074	3911	6539	8956		3137	4894		
01	645013		671289	684123		709161			745088		
11	5236	8471	1505	4335	6957	9366	1550	3532	5282	6805	60
12	5458	8689	1721	4547	7165	9571	1760	3730	5476	6995	
13	568o	8908	1936	4759	7374	9776	1962	3927	5670	7185	40
14	5902	9127	2151	4971	7582	9981	2163	4125	5864	7375	
15	6124	9346	2367	5183	7790	710185	2364	4323	6057	7565	45
16	6346	9565	2582	5395	7999	0390	2565	4520	6251	7755	
17	6568	9783	2797	5607	7999 8207	0595	2766	4717	6445	7 945	
18	6790		3013	5818	8415	0799	2967	4915	6638	8134	45
19	7012	0220	3228	6030	8623	1004	3168	5112	6832	8324	42
20	647233			686242			72336g			758514	41
21	7455	0657	3658	6453	9040	1413	3570	5506	747025		
22	7677	0875	3873	6665	9248	1617		5703	7218 7412	8703	
23	7898	1094	4088	6876			3771			8893	
24	8120	1312	4302	7088	9455 9663	1822	3971	5900	7605	9082	
25	8341	1530	4517	• •		2020	4172	6097	7798	9271	
26	8563	(7299	9871		4372	6294	7991	9461	
27	8784	1748	4732		700079	2434	4573	6491	8184	9650	
28		1966	4947	7721	0287	2639	4773	6687	8377	9839	
- 1	9006	2184	5161	7932	0494	2843	4974	6884	8570	760028	
29 30	9227	2402	5376	8144	0702	3047	5174	7081	8763	0217	
31	649448		675590	688355	700909	713250	725374		748956	760406	
- 1	9669	2838	5805	8566	1117	3454	5575	7474	9148	0595	
32	9890	3056	6019	8776	1324	3658	5775	7670	9341	0784	
	650111	3273	6233	8987	1531	3862	5975	7867	9534	0972	
34	0332	3491	6448	9198	1739	4066	6175	8063	9726	1161	
35	0553	3709	6662	9409	1946	4269	6375	8259	_9919	1 350	25
36	0774	3926	6876	9620	2153	4473	6575	8455	750111	1538	24
37	0995	4144	7090	9830	2360	4676	6775	865 r	0303	1727	
38	1216	4361	7304	690041	2567	4880	6974	8848	0496	1915	
39	1437	4579	7518	0251	2774	5083	7174	9043	o688	2104	
	#1657	664796	677732	690462		715286		739239	750880		
41	1878	5013	7946	0672	3188	5490	7573	9435	1072	2480	
42	2098	5230	8160	0882	3395	5693	7773	9631	1264	2668	
43	2319	5448	8373	1093	3601	5896	7972	9827	1456	2856	
44	2539	5665	8587	1303	3808	6099		740023	1648	3044	
45	2760	5882	8801	1513	4015	6302	8371	0218	1840	3232	
46	2980	6099	9014	1723	4221	6505	8570	0414	2032	3420	
47	3200	6316	9228	1933	4428	6708	8769	0609	2223	3608	
48	3421	6532	9441	2143	4634	6911	8969	0805	2415	3796	12
49	3641	6749	9655	2353	4841	7113	9168	1000	2606	3984	11
50	a53861	666966	679868	692563	705047	777316	729367	741195	752798	764171	10
110	4081	7183	680081	2773	5253	7519	9566	1391	2989	4359	
52	4301	7399	0295	2983	5459	7721	9765	1586	3181	4547	9 8
53	4521	7616	0508	3192	5665	7924	9963	1781	3372	4734	7
54	4741	7833	0721	3402	5872		730162	1976	3563	4921	7 6
55	4961	8049	0934	3611	6078	8329	0361	2171	3755	5109	5
56	5180	8265	1147	3821	6284	8531	o56o	2366	3946	5296	4
57	5400	8482	1360	4030	6489	8733	5870	2561	4137	5483	3
58	5620	8698	1573	4240	6695	8936	0957	2755	4328	5670	2
59	5839	8914	1786	4449	6901	9138	1155	2950	4519	5857	Ι,
	49°	48°	47°	46°	45°	44°	43°	42°	41°	40°	
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					atural	Co-sines	·				
P. I	3.69	3.63	3.57	3.52	3.46	3.40	3.34	3.27	3.21	3.15	
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Min	40°	41°	42°	43°	44°	45°	46°	47°	48°	49°	
0	839100	869287	900404	932515	965689	1.00000			1.11061	1.15037	
I	9595	9798	0931	3059	6251	0058	3613	7299	1126	51c4	
2	840092	870309	1458	36o3	6814	0116	3674	7362	1191	5172	58
3	0588	0820	1985	4148	7377	0175	3734	7425	1256	5240	57
4	1084	1332	2 513	4693	7940	0233	3794	7487	1321	5308	56
5	1581	1843	3041	5238	8504	0291	3855	7550	1387	5375	55
6	2078	2356	3569	5783	9067	o35o	3915	7613	1452	5443	
	2575	2868	4098	6329	9632	0408	3976	7676	1517	5511	
78	3073	3381	4627	6875	970196	0467	4036	7738	1582	5579	
- 1	3571	3894	5156	7422	0761	0525	4097	7801	1648	5647	5 T
9	9//060	874407			0701			T 07864		1.15715	50
			6215	8515	1802		4218			5783	1/0
II	4567	4920				0642		7927	1778	5851	49
12	5066	5434	6745	9063	2458	0701	4279	7990	1844	5051	
13	5564	5948	7275	9610	3024	0759	4340	8053	1909		
14	6063	6462	7805		3590	0818	4401	8116	1975	5987	40
15	6562	6976	8336	0706	4157	0876	4461	8179	2041	6656	
16	7062	7491	8867	1255	4724	0935	4522	8243	2106	6124	44
17	7562	8006	9398	1803	5291	0994	4583	8306	2172	6192	43
18	8062	8521	9930	2352	5859	1 o 5 3	4644	8369	2238	6261	42
19	8562	0037	910462	2902	6427	1112	4705	8432	2303	6329	41
		879553	910994							1.16398	160
21	9563		1526	4001	7564	1229	4827	8559	2435	6466	30
- 1	850064	0585	2059	4552	8133	1288	4888	8622	2501	6535	
23	0565		2592	5102	8703	1347		8686	2567	6603	
	- 1	1102					4949				
24	1067	1619	3125		9272	1406	5010	8749	2633	6672	
25	1568	2136	3659	5204	9842	1465	5072		2699	6741	
26	2070	2653	4193		980413	1524	5133		2765	6809	
27	2573	3171	4727		0983	1583	5194	, ,	2831	6878	
28	3075	3689	5261	7859	1554	1642	5255	9003	2897	6947	3:
29	3578	4207	5796	8412	2126	1702	5317	9067	2963	7016	31
30	854081	884725	916331	948965	982697	1.01761	1.05378	1.09131	1.13029	1.17085	30
31	4584	5244	6866	9518	3269	1820	5439	9195	3096	7154	
32	5087	5763	7402		3842	1879	5501	9258	3162	7223	
33	5591	6282	7938	0624	4414			9322	3228	7292	:
34	6095	6802	8474	1178	4987	1998		9386	3295	7361	
35	6599	7321	9010	1733	5560	2057				7430	
36		7842	9547	2287	6134	2117	5747	9514	3428	7500	
37	7104										
	7608		920084	2842	6708				3494		
38	8118		0621	3397	7282				3561	7638	
39	8619	9403	1159	3953	7857	2295	5932	9706	3627	7708	21
40	859124		921697							1.17777	
41	9630			5064	9007	2414	6056	9834	3761	7846	
42	860136	0967	2773	5621	9582		6117	9899	3828	7916	
43	0642	1489	3312	6177	990158	2533	6179	0963	3894	7986	ľ
44	1148			6734	0735			1.10027		8055	
45	1655	2534			1311	2653	6303	0001	4028		
46	2162	3057	4930		1888	2713	6365	0156	4095		
47	2669		5470		2465	2772					
48	3177	4103	6010		3043	2832	6489	0285	4229		
49	3685		6551	9524		2892	6551	0349	4296		
50									1.1/363	1.18474	
5 i											
	4701										
52	5209										
53	5718	1					1			1	
54	6227								4632		
55	6736	1 1 1 1 1									
56			930342								
57	7756							0867			
58			1428	4565	8837	3433	7112	0931	4902		
59	8776			1 2	1						
	49°	48°	470	46°	45°	440	43°	42°			
	49	48	4/	40	40	44	43	42	41°	40°	Min
				_	_						
				N	atural (Co-tange	nts.				Z
Р.	P. 8.38	8.64	8.92	9 21	9.53	Co-tange	nts.	1.06	1.10	1.15	Z

1	59° 857167 7317 7467	60
I	7317	160
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3 6605 7695 8548 9160 9536 9652 9525 9146 8510 5 6979 8060 8905 9510 9871 9985 9462 8818 6 7165 8243 9084 9685 810042 820152 830012 9620 8972 7 7352 8426 9263 9859 0212 0318 0174 9778 9125 8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 78979 9620 0208 0553 0651 0499 840044 9433 10 767911 789793 789798 800383 810723 820817 830661 840251 84566 9279 11 8097 9156 9977 0557 0894 0983 0823 04094 9433 13 8470 9520 0333 0906 1234 1315 1146 0724 85066	7/1671	
4 6792 7878 8727 9335 9700 9819 9688 9304 8664 5 6979 8060 8905 9685 810042 820152 830012 9620 8718 7 7352 8426 9263 9859 0212 0318 0174 9778 9125 8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 8791 9620 0208 0553 0651 0499 840094 9433 10 767911 778973 789798 800383 810723 820817 830661 840251 849586 11 8097 9156 9977 0557 0894 0983 0823 0409 9739 12 8284 9338 790155 0731 1064 1149 0984 0567 9893 13 8470 9520 05333 0906		
5 6979 8060 8905 9510 9871 9985 9850 9462 8818 7 7352 8426 9263 9859 0212 0318 0174 9778 9125 8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 8791 9620 0208 0553 0651 0499 840094 9433 10 767911 778973 789798 800383 810723 820817 830661 840251 849586 11 8097 9156 9977 0557 0894 0983 0823 0409 9739 12 8284 9338 790155 0731 1064 1149 0984 0567 9893 13 8470 9520 0531 1080 1404 1481 1308 0882 0199 15 8842 9884 0690 1254 <td< td=""><td>7616</td><td></td></td<>	7616	
6 7165 8243 9684 9685 810042 820552 830012 9620 8972 7 7352 8426 9263 9859 0212 0318 0174 9778 9125 8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 8791 9620 0208 0553 0651 0499 9433 10 767911 778973 789798 800383 810723 820817 830661 840251 84556 11 8097 9156 9977 0557 0894 0983 0823 06251 0409 9739 12 8284 9338 790155 0731 1064 1149 0984 0567 9893 13 8470 9520 0333 0906 1234 1315 1146 0724 850046 14 8656 9702 0511 1080	7766	5.6
7 7352 8426 9263 9859 0212 0318 0174 9778 9125 8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 8791 9620 0208 0553 0651 0499 840094 9433 10 767911 778973 789798 80383 810723 820817 830661 840251 84586 11 8097 9156 9977 0557 0894 0983 0823 0400 9739 12 8284 9338 790155 0731 1064 1149 0984 0567 9893 13 8470 9520 0333 0906 1234 1315 1146 0724 85046 14 8656 9702 0511 1080 1404 1481 1308 0882 0109 15 8842 9884 0690 1254 <td< td=""><td>7915 8065</td><td>5</td></td<>	7915 8065	5
8 7538 8608 9441 800034 0383 0485 0337 9936 9279 9 7725 8791 9620 0208 0553 0651 0499 840094 9433 10 767911 778973 789798 800383 810723 820817 830661 840251 846568 840586 11 8097 9156 9977 0557 0894 0983 0823 0409 9739 12 8284 9338 790155 0731 1064 1149 0984 0567 9893 13 8470 9520 0333 0906 1234 1315 1146 0724 850046 14 8656 9702 0511 1080 1404 1481 1308 0882 0199 15 8842 9884 0690 1254 1574 1647 1470 1039 0352 17 9214 0249 1046	8214	
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20 769771 780794 791579 802123 812423 822475 832277 841825 851117 9957 21 9957 0976 1757 2297 22592 2641 2438 1982 1269 22 770142 1157 1935 2470 2762 2866 2599 2139 1422 23 0328 1339 2112 2644 2931 2971 2760 2296 1575 24 0513 1520 2290 2817 3101 3136 2921 2452 1727 25 0699 1702 2467 2991 3270 3302 3082 2609 1879 26 0884 1883 2644 3164 3439 3467 3243 2766 2032 27 1069 2065 2822 3337 3688 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3079 3366 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 78268 79335	9852	
21 9957 0976 1757 2297 2592 2641 2438 1982 1269 22 770142 1157 1935 2470 2762 2806 2599 2139 1422 23 0328 1339 2112 2644 2931 2971 2760 2296 1575 24 0513 1520 2290 2817 3101 3136 2921 2452 1727 25 0699 1702 2467 2991 3270 3302 3082 2609 1879 26 0884 1883 2644 3164 3439 3467 3243 2766 2032 27 1069 2065 2822 3337 3608 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3079 2336 29 1440 2427 3176 3684 3947		
22 770142 1157 1935 2470 2762 2806 2599 2139 1422 23 0328 1339 2112 2644 2931 2971 2760 2296 1575 24 0513 1520 2290 2817 3101 3136 2921 2452 1727 25 0699 1702 2467 2991 3270 3302 3082 2609 1879 26 0884 1883 2644 3164 3439 3467 3243 2766 2032 27 1069 2065 2822 3337 3608 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3079 2336 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640	860149	40
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25 0699 1702 2467 2991 3270 3302 3082 2609 1879 26 0884 1883 2644 3164 3439 3467 3243 2766 2032 27 1069 2065 2822 3337 3608 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3079 2336 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640	0594	
26 0884 1883 2644 3164 3439 3467 3243 2766 2032 27 1069 2065 2822 3337 3608 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3679 2336 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640	0890	
27 1069 2065 2822 3337 3608 3632 3404 2922 2184 28 1254 2246 2999 3511 3778 3797 3565 3079 2336 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640	1038	
28 1254 2246 2999 3511 3778 3797 3565 3679 2336 29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640 8	1186	
29 1440 2427 3176 3684 3947 3961 3725 3235 2488 30 771625 782608 793353 803857 814116 824126 833886 843391 852640 8	1334	
30 771625 782608 793353 803857 814116 824126 833886 843391 852640 8	1481	31
	861629	30
31 1810 2789 3530 4030 4284 4291 4046 3548 2792	1777	
32 1995 2970 3707 4203 4453 4456 4207 3704 2944	1924	
33 2179 3151 3884 4376 4622 4620 4367 3860 3096	2072	27
34 2364 3332 4061 4548 4791 4785 4527 4016 3248	2219	
35 2549 3513 4238 4721 4959 4949 4688 4172 3399	2366	
36 2734 3693 4415 4894 5128 5113 4848 4328 3551	2514	
37 2918 3874 4591 5066 5296 5278 5008 4484 3702 38 3103 4055 4768 5230 5465 5442 5168 4640 3854	2661	
	2808	
39	2955	
41 3656 4596 5297 5756 5969 5934 5648 5106 4308	3249	
42 3840 4776 5473 5928 6138 6098 5807 5262 4459	3396	
43 4024 4957 5650 6100 6306 6262 5967 5417 4610	3542	17
44 4209 5137 5826 6273 6474 6426 6127 5573 4761	3689	
45 4393 5317 6002 6445 6642 6590 6286 5728 4912	3836	15
46 4577 5497 6178 6617 6809 6753 6446 5883 5063	3982	
47 4761 5677 6354 6788 6977 6917 6605 6038 5214	4128	
48 4944 5857 6530 6960 7145 7081 6764 6193 5364	4275	
49 5128 6037 * 6706 7132 7313 7244 6924 6348 5515	4421	II
56 775312 786217 796882 807304 817480 827407 837683 846503 855665 8	864567	
51 5496 6396 7057 7475 7648 7571 7242 6658 5816	4713	
52 5679 6576 7233 7647 7815 7734 7401 6813 5966	4860	
53	5006	
54 6046 6035 7584 7990 8150 8060 7719 7122 6267 55 6230 7114 7759 8161 8317 8223 7878 7277 6417	5151 5297	C
	5443	4
56 6413 7294 7935 8333 8484 8386 8036 7431 6567 57 6596 7473 8110 8504 8651 8549 8195 7585 6718	5589	
58 6780 7652 8285 8675 8818 8712 8354 7740 6868	5734	
59 6963 7832 8460 8846 8985 8875 8512 7894 7017	5880	
39° 38° 37° .36° 35° 34° 33° 32° 31°	30°	F
Natural Co-sines.	- 50	Min.
	1	-
P P: 3.08 3.02 2.95 2.88 2.81 2.75 2.68 2.60 2.53	2.46	

				NATU	KAL	LANG	ENTS.				1 4
Min.	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	
_	1.19175	1.23490	1.27994	1.32704	1.37638	1.42815	1.48256	1.53986	1.60033	1.66428	
I	9246	3563	8071	2785	7722	2903	8349	4085	0137	6538	50
2	9316	3637	8148	2865	7807	2992	8442	4183	0241	6647	58
3	9387	3710	8225	2946	7891	3080	8536	4281	o345	6757	5
4	9457	3784	8302	3026	7976	3169	8629	4379	0449	6867	
5	9528	3858	8379	3107	8060	3258	8722	4478	o553	6978	
6	9599	3931	8456	3187	8145	3347	8816	4576	0657	7088	5.
78	9669	4005	8533		8229	3436	8909	4675	0761	7198	
8	9740	4079	8610		8314	3525	9003	4774	o865	7309	
9	9811	4153	8687	3430	8399	3614	9097	4873	0970	7419	5
0		1.24227		1.33511	1.38484	1.43703		1.54972	1.61074	1.67530	5
п	9953	4301	8842	3592	8568	3792	9284	5071	1179	7641	
2	1.20024	4375	8919	3673	8653	3881	9378	5170	1283	7752	
3	0095	4449	8997	3754	8738	3970	9472	5269	1388	7863	
4	0166	4523	9074	3835		4060	9566	5368	1493	7974	
5	0237	4597	9152	3916	8909	4149	9661	5467	1598	8085	
6	o3o8	4672	. 9229	3998	8994	4239	9755	5567	1703	8196	4
7	0379	4746	9307	4079	9079	4329	9849	5666	1808	8308	
8	0451	4820	9385	4160	9165	4418	9944	5766	1914	8419	4
9	0522	4895	0463	4242	9250	4508	1.50038	5866	2019	8531	
ó	1.20593	1.24969	1.29541	1.34323	1.39336	1.44598	1.50133	1.55966	1.62125	1.68643	4
1	o665	5044	9618	4405	9421	4688	0228	6065	2230	8754	3
2	0736	5118	9696	4487	9507	4778	0322	6165	2336	8866	3
3	0808	5193	9775	4568	9593	4868	0417	6265	2442	8979	3
4	0879	5268	9853	465o	9679	4958	0512	6366	2548	9091	
5	0951	5343	9931	4732	9764	5049	0607	6466	2654		
6	1023		1.30009	4814	9850	5139	0702	6566	2760	9316	
7	1094	5492	0087	4896	9936	5229	0797	6667	2866	9428	
8	1166	5567	0166	4078	1.40022	5320	0893	6767	2972	9541	
9	1238	5642	0244	5060	0100	5410	0988	6868	3079	9653	3
0	1.21310					1.45501	1.51084		1.63185		
I	1382	5792	0401	5224	0281	5592	1179	7069	3292	9879	
2	1454	5867	0480	5307	0367	5682	1275	7170	3398	9992	
3	1526	5943	0558	5389	0454	5773	1370	7271		1.70106	
4	1598	6018	0637	5472	0540	5864	1466	7372	3612	0219	
5	1670	6093	0716	5554	0627	5955	1562	7474	3719	0332	
6	1742	6169	0795	5637	0714		1658	7575	3826		
7	1814	6244	0873			6137	1754	7676	3934		
8	1886	6319	0952	5802	0887	6229	1850	7778	4041	0673	
9	1959	6395	1031	5885	0974	6320	1946	7879	4148	0787	
	1.22031	1 26/71				1.46411	1.520/3	1.57081			
I	2104	6546	1190	6051	1148	6503	2139	8083	4363	1015	
2	2104	6622	1269	6134		6595	2235	8184		1129	
3	2249	6698	1348	6217		6686	2332	8286	4579	1244	
4	2321		1427	6300	I .	1	2429	8388	4687	1358	
5	2394	6774 6849	1507	6383		6870	2525	8490	4795	1473	
6	2394	6925	1586			6962	2622	8593	4793		
7	2539	7001	1666				2022	8695	5011	1702	
8	2612		1745	6633	1759		2816	8797	5120		
	2685	7077 7153	1825				2913	8900			
9					1047	1.47330	T 53070	7 50000			
I	2831	7306	1.31904				3107	9105			
2	2904			1			3205				1
3							3302		5663		
4							3400		1 -		
5	3123		2224 2304				3497		5881		
6											
						7885	3595	9620	5990		
7	3270			1 .			3693	9723			
8					2638		3791	9826			
59			2624				3888		6318		L
	39°	38°	37°	36°	35°	34°	33°	32°	31°	30°	1
				Na	atural C	o-tanger	nts.		·	<u> </u>	, Line
	P. 1.20	1.25	1.31	1.37	1.44	1.51	1.59	1.68	1.78	1.88	Γ
٠.		i	1		I	l	•		'	١٠	1

Min	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	1
0	866025	874620	882948	891007	898794	906308	913545	920505	927184	933580	60
1	6171	4761	3084			6431	3664		7293	3685	50
2	6316	4902		1270			3782		7402	3789	58
3	6461	5042		1402				o846	7510	3893	57
4	6607			1534	9304		4018	0959	7619	3997	
5	6752	5324		1666	9431		4136	1072	7728	4101	
6	6897	5465		1798	9558		4254		7836	4204	
7	7042			1929	9685		4372	1299	7945	4308	
8	7187	5746		2061	9812		4490	1412	8053	4412	
9	7331	5886		2192	9939	7411	4607	1525	8161	4515	
10	867476			892323	,					934619	
11	7621 7765	6167 6307	4445 4581	2455 2586	0192	7655	4842	1750	8378	4722	
13		6447			0319	7777	4960	1863	8486	4826	
14	7910 8054	6587	4717 4852	2717 2848	0445 0572	7899 8021	5077	1976 2088	8594	4929 5032	
15	8199	6727	4988		0572	8143	5194 5311	2000	8702 8810	5135	
16	8343	6867	5123	2979 3110	0825	8265	5429	2313	8917	5238	
17	8487	7006	5258	3241	0951	8387	5546	2426	9025	5341	
18	8632	7146	5394	3371	1077	8508	5663	2538	9133	5444	
19	8776	7286	5529	3502	1203	863o	5779	2650	9240	5547	11
20	868920	877425			901329	908751		922762		935650	10
21	9064	7565	5799	3763	1455	8872	6013	2875	9455	5752	
22	9207	7704	5934	3894	1581	8994	6130	2986	9562	5855	
23	9351	7844	6060	4024	1707	9115	6246	3098	9669	5957	
24	9495	7983	6204	4154	1833	9236	6363	3210	9776	6060	
25	9639	8122	6338	4284	1958	9357	6479	3322	9884	6162	
26	9782	8261	6473	4415	2084	9478	6595	3434	9990	6264	
27	9926	8400	6608	4545	2200	9599	6712	3545		6366	
28	870069	8539	6742	4675	2335	9720	6828	3657	0204	6468	32
29	0212	8678	6876	4805	2460	9841	6944	3768	0311	6570	3 r
30	870356	878817	887011	894934	902585	909961	917060	923880	930418	936672	30
31	0499	8956	7145	5064	2710	910082	7176	3991	0524	6774	29
32	0642	9095	7279	5194	2836	0202	7292	4102	o631	6876	28
33	0785	9233	7413	5323	2961	0323	7408	4213	0737	6977	27
34	0928	9372	7548	5453	3o86	0443	7523	4324	0943	7079	
35	1071	9510	7681	5582	3210	0563	7639	4435	0950	7181	1
36	1214	9649	7815	5712	3335	0684	7755	4546	1056	7282	
37	1357	97 ⁸ 7	7949	5841	3460	0804	7870	4657	1162	7383	
38	1499	9925	8083	5970	3585	0924	7986	4768	1268	7485	
39	1642	880063	8217	6099	3709	1044	8101	4878	1374	7586	
40	871784	880201		896229	903834		918216	924989		937687	
41	1927	0339	8484	6358	3958	1284	8331	5099	1586	7788	
42 43	2069	0477	8617	6486	4083	1403	8446	5210 5320	1691	7889	
	2212	0615	8751	6615		1523 1643	8561 8676	5430	1797 1902	7990 8091	
44 45	2354 2496	0753	8884	6744 6873	4331 4455	1762	8791	5541	2008	8191	
46	2490 2638	0891	9017	7001	4579	1881	8906	5651	2113	8292	
47	2780	1166	9283	7130	4579	2001	9021	5761	2219	8393	
48	2922	1303	9203	7258	4827	2120	9135	5871	2324	8493	
49	3064	1441	9549	7387	4951	2230	9250	5980	2429	8593	
50			889682			912358		926090			
51	3347	1716	9815	7643	5198	2477	9479	6200	2639	8794	
52	3489	1853	9948	7771	5322	2596	9593	6310	2744	8894	8
53	3631		890080	7900	5445	2715	9707	6419	2849	8994	7
54	3772	2127	0213	8028	5569	2834	9821	6529	2954	9094	7 6
55	3914	2264	o345	8156	5692	2953	9936	6638	3ó58	9194	5
56	4055	2401	0478	8283	5815	3072	920050	6747	3163	9294	4
57	4196	2538	0610	8411	5939	3190	0164	6857	3267	9394	3
58	4338	2674	0742	8539	6062	3369	0277	6966	3372	9493	2
59	4479	2811	0874	8666	6185	3427	0391	7075	3476	9593	I
	29°	28°	27°	26°	25°	24°	23°	22°	21°	20°	,
j l											Min.
				Ŋ	vatural	Co-sines	.				
P. 1	P. 2	0 2.	0.04	0 -6	0.00	1	3	7 86	T 78	7.70	
to 1	2.39	2.31	2.24	2.16	2.09	2.01	1.93	1.86	1.78	1.70	

d W	30°	61°	62°	63°	64°	65°	66°	67°	68°	69°	1
0	1.73205	1.80405	1.88073	1.96261	2.05030	2.14451	2.24604	2.35585	2.47509	2.60509	60
I	3321		8205	6402	5182	4614	4780	5776	7716	0736	5 59
2	3438						4956	5967	7924		
3	3555	0777								,	
4	3671	0901	8602						8340	1418	
5	3788	1025	8734				5486			1646	
6	3905		8867	7111	5942		5663				
7 8	4022		9000	7253	6094	5596				1	
1	4140		9133	7395 7538	6247	5760	6018		9177	2332	
9	4257	1524	9266	7550	6400	5925	6196		9386	2561	
10		1.81649	9533	7823	6706	6255	6552	7697	9807		160
11	4492 4610	1774	9667	7966	686o	1	6730	7097	2.50018	3252	
13	4728	2025	9801	8110			6909	8084			140
14	4846	2150	9935	8253	7167	6751	7088	8279			
15	4964		1.90069	8396	7321	6917	7267	8473			
16	5082	2402	0203	854o	7476	7083	7447	8668			
17	5200	2528	0337	8684	7630	7249	7626	8863		4410	
18	5319	2654	0472	8828		7416	7806	9058			13
19	5437	2780	0607	8972	7939	7582	7987	9253	1502	4875	
20		1.82906		1.00116	2.0800/			2.30440	2.51715		
21	5675	3033	0876	9261	8250	7916	8348	9645	1929	5342	30
22	5794	3159	1012	9406	8405	8084	8528	9841	2142	5576	38
23	5913	3286	1147	9550	856o	8251		2.40038	2357	5811	
24	6032	3413	1282	9695	8716	8419	8891	0235	2571	6046	
25	6151	3540	1418	9841	8872	8587	9073	0432	2786		
26	6271	3667	1554	9986		8755	9254	0629			
27	6390	3794	1690	2.00131	9184	8923	9437	0827	3217		
28	6510	3922	1826	0277	9341	9092	9619	1025	3432	6989	
29	663o	4049	1962	0423	9498	9261	9801	1223	3648	7225	31
30	1.76749	1.84177	1.92098	2.00569	2.09654	2.19430	2.29984	2.41421	2.53865		
31	6869	4305	2235	0715	9811	9599	2.30167	1620	4082	7700	29
32	6990	4433	2371	0862	9969	9769	o351	1819		7937	28
33	7110	4561	2508		2.10126	9938	o534	2019	4516	875	2)
34	7230	4689	2645	1155		2.20108	0718	2218	4734	8414	
35	7351	4818	2782	1302	0442	0278	0902	2418	4952	8653	
36	7471	4946	2920	1449	0600	0449	1086	2618	5170	8892	
37	7592	5075	3057	1596	0758	0619	1271	2819		9131	
38	7713	5204	3195	1743	0916	0790	1456	3019	5608	9371	
39	7834	5333	3332	1891	1075	0961	1641	3220	5827	9612	21
	1.77900	1.85462									
41	8077	5591	3608	2187	1392	1304	2012	3623		2.70094	
42	8198	5720	3746	2335	1552	1475	2197 2383	3825	6487	o335	
43	8319	585o	3885	2483 2631	1711	1647	2570	4027	6707	0577	
44	8441 8563	5979	4023	2780	1871	1819		4230	6928	0819	
46	8685	6109	4162 4301		2030	1992 2164	2756 2943	4433 4636	7150 7371	1062 1305	
47	8807	6369	4440	2929 3078	2190 2350	2337	3130	4839	7593	1548	
47	8929	6499	4579	3227	2511	2510	3317	5043	7393	1792	
49	9051	6630	4718	3376	2671	2683	3505	5246	8038	2036	
50	1.7017/	1.86760	1.0/858	2.03526	2.12832	2.22857	2.33603	2.45451	2.58261	2.72281	10
51	9296	6891	4997	3675	2993	3030	3881	5655	8484	2526	
52	9419	7021	5137	3825	3154	3204	4069	5860	8708	2771	
53	9542	7152	5277	3975	3316	3378	4258	6065	8932	3017	
54	9665	7283	5417	4125	3477	3553	4447	6270	9156	3263	
55	9788	7415	5557	4276	3639	3727	4636	6476	9381	3509	
56	9911	7546	5698	4426	3801	3902	4825	6682	9606	3756	
57	1.80034	7677	5838	4577	3963	4077	5015	6888	9831	4004	
58	0158	7809	5979	4728	4125	4252	5205		2.60057	4251	
59	0281	7941	6120	4879	4288	4428	5395	7302	0283	4499	
	29°	28°	27°	26°	25°	24°	23°	220	210	20°	
							1	~~	~1	~~	Min
				Na	tural C	o-tangen	ts.			,	**
P.	P			7			0 - 1	2.5	1		
	- ^ ^	2.13	2.27	2.44	2.62	2.82	3.05	3.31	3.61	2 0 5	1
to 1	2.00	2.10	2.2/	2.44	2.02	2.02	0.00	0.01	3.01	3.9 5	

Min.	70°	71°	72°	73°	74°	75°	76°	77°	78°	7 9°	
0	939693	945519	951057	956305	961262	965926	970296	974370	978148	981627	60
1	9792	5613	1146	6390	1342	6001	~ ò366	4435	8208	1683	50
2	9891	5708	1236	6475	1422	6076	o436	4501	8268	1738	
3	9991	5802	1326	656o	1502	6151	0506	4566	8329	1793	57
4	940090	5897	1415	6644	1582	6226	0577	4631	8389	1849	56
5	0189	5991	1505	6729	1662	6301	0647	4696	8449	1904	
6	0288	6085	1594	6814	1741	6376	0716	4761	8509	1959	54
7 8	0387	6180	1684	6898	1821	6451	0786	4826	8569	2014	53
1	0486	6274	1773	6983	1901	6526	0856	4891	8629	2069	
9	0585	6368	1862	7067	1980	6600	0926	4956	8689	2123	
10	940684	946462	951951					975020	978748	982178	50
II	0782	6555	2040	7235	2139	6749	1065	5085	8808	2233	49
12	0881	6649	2129	7319	2218	6823	1134	5149	8867	2287	48
13	0979	6743	2218	7404	2297	6898	1204	5214	892-	2342	
14	1078	6837	2307	7487	2376	6972	1273	5278	8986	2396	
15	1176	6930	2396	7571	2455	7046	1342	5342	9045	2450	
16	1274	7024	2484	7655	2534	7120	1411	5406	9105	2505	
17	1372	7117	2573	7739	2613	7194	1480	5471	9164	2559	43
- 1	1471	7210	2661	7822	2692	7268	1549	5535	9223	2613	42
20	1569 941666	7304 947397	2750	7906	2770	7342	1618	5598 975662	9282 979341	2667	
21	1764	7490					971687	973002 5726		982721	
21	1862	7490 7583	2926 3015	8073 8156	2928 3006	7489 7562	1755		9399 9458	2774 2828	
23	1960	7503	3103	8239	3084	7502 7636	1824 1893	5790 5853	9517	2882	
24	2057	7768	3191	8323	3163	7709	1961	5917	9575	2935	36
25	2155	7861	3279	8406	3241	7782	2029	5980	9634	2989	
26	2252	7954	3366	8489	3319	7856	2008	6044	9692	3042	
27	2350	8046	3454	8572	3397	7929	2166	6107	9750	3096	
28	2447	8139	3542	8654	3475	8002	2234	6170	9809	3149	
29	2544	8231	3629	8737	3553	8075	2302	6233	9867	3202	
30	942641	948324	953717		963630		972370	976296	979925	983255	
31	2739	8416	3804	8902	3708	8220	2438	6359	9983	3308	
32	2836	8508	3892	8985	3786	8293	2506	6422	980041	3361	
33	2932	8600	3979	9067	3863	8366	2573	6485	0098	3414	27
34	3029	8692	4066	9150	3941	8438	2641	6547	o156	3466	26
35	3126	8784	4153	9232	4018	8511	2708	6610	0214	3519	25
36	3223	8876	4240	9314	4095	8583	2776	6672	0271	3571	24
37	3319	8968	4327	9396	4173	8656	2843	6735	0329	3624	23
38	3416	9059	4414	9478	4250	8728	2911	6797	o386	3676	22
39	3512	9151	4501	9560	4327	8800	2978	6859	0443	3729	21
40	943609	949243	954588	959642		968872	973045	976921	980500	983781	
41	3705	9334	4674	9724	4481	8944	3112	6984	0558	3833	19
42	3801	9425	4761	9805	4557		3179	7046	0615	3885	
43	3897	9517	4847	9887	4634	9088	3246	7108	0672	3937	17
44	3993	9608	4934	9968	4711	9159	3313	7169	0728	3989	
45	4089	9699		960050	4787	9231	3379	7231	0785	4041	
46	4185	9790	5106	0131	4864	9302	3446	7293	0842	4092	
47	4281	-9881	5192	0212	4940	9374	3512	7354	0899	4144	
48	4376	9972	5278	0294	5016	9445	3579 3645	7416	0955 1012	4196 4247	
49	4472 944568	950063	5364	0375	5093	9517	3645	7477		984298	
51	4663	0244	955450 5536	0537	5245	9659	973712 3778	7600	1124	4350	
52	4003 4758	0335	5622	0537	5321	9730	3844	7661	1124	4401	
53	4854	0333	5707	0698		9801	3044	7722	1237	4452	
54	4949	0516				9872		7783		4503	
55	5044					9943	4042	7844		4554	
56	5139	0696				970014		7905		4605	
57	5234				5700	0084		7966			
58	5329	0877	6134	1101	5775			8026	1		
59	5424		6220		5850			8087			1
	19°	18°	- 0220	16°	15°	14°	13°	12°	11°	10°	-
	13	10	1/	L				12	11	1	Min.
				I	Natural	Co-sine	s.				1
P.	P c.		- 16	- 20		1	2	, as	0.05	0.88	
to I	P. 1.62	1.54	1.46	1.38	:.30	1.21	1.13	1.05	0.97	0.00	
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				NATU	AAL	1 A . G	ENTS.				1 3
M.p.	70°	71°	72°	73°	74°	75°	76°	77°	7 8°	79°	
0	2.74748	2.90421	3.07768	3.27085	3.48741	3.73205	4.01078	4.33148	4.70463		
1	4997	0696	8073	7426	9125	3640	1576	3723	1137		
2	5246	0971	8379	7767	9509	4075	2074	4300			58
3	5496	1246	8685					4879			
4	5746	1523	8991	8452	3.50279			5459	3170		
5	5996	1799	9298		0666	5388	3578	6040		848o	55
6	6247	2076	9606	9139	1 1053		4081	6623	4534	9293	54
7	6498	2354	9914	9483	1441	6268	4586	7207	5219	5.20107	53
8	6750	2632	3.10223		1829	6709	5092	7793	5906	0925	
9	7002	2010		3.30174	2219		5599	8381	6595	1744	
10	2.77254	2.03180	3.10842	3.30521	3 52600	3.77505	4.06107	4.38060	4.77286	5.22566	50
II	7507	3468	1153	0868		8040	6616	9560	7978	3391	40
12	7761	3748	1464			1 .		4.40152	8673	4218	
13	8014	4028	1775				7639		9370		
14	8269	4309	2087	1	1 . 1	9378			4.80068		
15	8523	4591	2400			9827	8666		0769	6715	
16	. 8778	4872	2713			3.80276	9182	2534	1471	7553	
	9033	5155	3027		5364				2175	8393	
17					5-67		4.10216		2882		
18	9289	5437	3341 3656	3317		1177					
19	9545	5721		3670	2 5 6 5 5	1630	0736	4338	3390	5.30080	41
		2.96004		3.34023			4.11256	4.44942		0.30920	40
	2.80059	6288	4288		6957		1778		5013	1778	
22	0316	6573	4605	1 2 -			2301	6155	5727	2631	1
23	0574	6858	4922	5087	7758		2825	6764	6444	3487	
24	o833		5240			3906	335o	7374	7162		
25	1091	7430	5558		8562	4364	3877	7986	7882		35
20	135o	7717	5877	6158	l 8966		4405	8600	8605		
27	1610		6197	6516	1 9370	5284	4934	9215	9330	6936	33
2Ś	1870	8292	6517	6875	9775	5745	5465	9832	4.90056	7805	32
29	2130	858o	6 838		3.60181	6208	5997	4.5ó451	0785	8677	31
3ó	2.82301	2.98868	3.17150	3.37594	3.60588	3.86671	4.16530	4.51071	4.91516	5.30552	30
31	26 53	9158	7481	7955	0996	7136	7064	1693		5.40429	
32	2914	9447	7804		1405		7600	2316	2984	1309	
3 3	3176	9738				8068	8137	2941	3721	2192	
34	3/30	3.00028	8451		2224			3568		3077	
35	3702	0319	8775				9215	4196	1 1	3966	
36	3965	0611	9100		3048		9756	4826	5945		
37	4229	0903		3.40136		94/4	4.20298	5458			
38	4494	1196	9752	0502		3.90417	0842	6091	7438	6648	
			3.20079						8188	7548	
39	4758					0890		6726			
							4.21933				
41	5289	2077	0734			1839	2481	8001	9695	9356	
42	5555	2372	1063		5538		3030		5.00451		
43	5822	2667	1392		5957		3580	,	1210	1176	
44	6089	2963	1722		6376		4132	9927		2090	
45	6356	3260	2053	3084	, ,		4685	4.60572	2734	3007	
46	6624	-3556	2384				5239	1219	3499	3927	14
47	6892	3854	2715	3829			5795	1868	4267	4851	
48	7161	4152	3048			5196	6352	2518	5037	5777	12
49	7430	4 450	3381	4576			6911	3171	5809	6706	ΙI
	2.87700	3.04749	3.23714	3.44951	3.68909	3.96165	4.27471	4.63825		5 57638	10
51	7970	5049	4049			6651	8032	4480	7360	8573	9
52	8240	5340	4383		9761	7139	8595	5138	8139	9511	8
53	8511	5649	4719		3.70188	7627	9159	5797		5.60452	
54	8783	5950	5055				9724	6458	9704	1397	
55	9055	6252	5392				4.30291		5.10490	2344	
56	9327	6554	5729		1476	9099		7786		3295	
57	9600		6067					8452	2060	42 48	
58	9873	7160	6406			4.00086	2001	9121	2862	5205	1
	2.90147	7464	6745				2573	•	3658	6165	
59						·		9791			I
	19°	18°	17°	16°	15°	14°	13°	12°	11°	10°	نہ ا
				Na	ıtural C	o-tanger	ıts.				Min.
P.	P. 4.35	4.82	5.36	6.01	6.79	7.73	8.90	10.35	12.20	14.60	T
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1	# 80° 81° 82° 83° 84° 85° 86° 87° 88° 80° T										
Min.	80°	81° !	62°	83°	84°	85°	86°	87°	880	89°	0
1 1	984808	987688	990268	992546		996195	997564	998630		999848	60
I	4858 4909	7734	o3o9 o349	2582 2617	4552 4583	6220 6245	7584 7604	8645 866o	9401	9853	
3	4959	7779 7824	0349	2652	4613	6270	7625	8675	9411	9358 9863	
4	5009	7870	0429	2687	4643	6295	7645	8690	9431	9867	
5	5059	7915	0469	2722	4673	6320	7664	8705	9441	9872	5 5
6	5109	7960	0509	2757	4703	6345	7684	8719	9450	9877	
7	5159	8005	0549	2792	4733	6370	7704	8734	9460	9881	53
8	5209	8050	0589	2827	4762	6395	7724	8749	9469	9886	
10	5259 985309	8094 988139	0629	2862	4792	6419 996444	7743 997763	8763	9479 999488	9890 999894	50
11	5358	8184	0708	2931	4851	6468	7782	8792	9497	9898	
:2	5408	8228	0748	2966	4881	6493	7801	8806	9507	9903	48
13	5457	8273	0787	3000	4910	6517	7821	8820	9516	9907	47
14	5507	8317	0827	3034	4939	6541	7840	8834	9525	9910	46
15	5556	8362	0866	3068	4969	6566	7859	8848	9534	9914	45
16	56o5 5654	8406 8450	0905 0944	3103 3137	4998 5027	6590 6614	7878	8862 8876	9542	9918 9922	44
17	5703	8494	0983	3171	5056	6637	7897 7916	8890	9551 9560	9922	43
19	5752	8538	1022	3205	5084	6661	7934	8904	9568	9929	41
20	985801	988582	991061	993238		996685		998917	999577	999932	40
21	5850	8626	1100		5142	6709	7972	8931	9585	9936	39
22	5899	8669			5170	6732	7990	8944	9594	9939	38
23	5947	8713	1177	3339	5199	6756	8008	8957	9602	9942	37
24	5996 6045	8756 8800	1216	3373 3406	5227 5256	6779 6802	8027 8045	8971	9610 9618	9945 9948	36
26	6093	8843	1292	3439	5284	6825	8063	8984 8997	9626	9940	3/
27	6141	8886	1331	3473	5312	6848	8081	9010	9634	9954	33
28	6189	8930	1369	3506	534o	6872	8099	9023	9642	9957	32
29	6238	8973	1407	3539	5368	6894	8117	9035	9650	9959	31
30		989016			995396	996917			999657	999962	30
31	6334	9059	1483	3605	5424	6940	8153	9061	9665	9964	
32	6381 6429	9102 9145	1521 1558	3638 3670	5452 5479	6963 6985	8170 8188	9073 9086	9672 9680	9967 9969	
34	6477	9187	1596	3703	5507	7008	8205	9098	9687	9909	26
35	6525	9230	1634		5535	7030	8223	9111	9694	9974	25
36	6572		1671	3768	5562	7053	8240	9123		9976	24
37	6620		1709		5589	7075	8257	9135	9709	9978	23
38	6667		1746		5617	7097	8274	9147		9980	22
39	6714		1783	3865	5644	7119	8291	9159		9981	21
40	6809	989442	1857	3929	5698	997141 7163	998368 8325	999171	999729 9736	999983 9985	10
42	6856		1894		5725	7185	8342	9194		9986	18
43	6903	1 /		3993		7207	8359	9206		9988	17
44	6950		1968			7229	8375	9218	9756	9989	16
45	6996		2005			1 '		9229		9990	15
46	7043						8408	9240		9992	14
47	7090					1 / /	8425 8441	9252 9263		9993 9994	13
48	7136 7183						8457	9203		. 9995	II
50	087220	989859	002187			007357	008473	999285	999793	999996	10
51	7275	9900		4245	5963	7378	8489	9296	9799	9997	9
52	7322	9942	2260	4276	5989	7399	8505		9804	9997	
53							8521				7 6
54	, , .	990024									1 -
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59							8614	9381			I
	9°	8°	70	6°	5°	4°	3°	2°	1°	00	4
		1		1	Natural	Co-sine	es.				Min.
P. to	P 1". 0.80	0.72	0.63	0.55	0.46	0.38	0.30	0.21	0.13	0.04	

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1 8094; 2566 3042 6388 4106 4685 3607; 1879 8771 58.2612 59 2 9064; 3761; 466; 7676; 6791 5072 4212 2950 291205-592655 58 3,5-9037; 4961 6071 8.2035 8390 9400 5461 4823 4051 3711 60-3058 57 4 1013; 6165; 7540 23441, 94020 5583 5438 5166 6245 61.3829 56 5 1992; 7374 9115 4345; 4935 6248 6059 6273 8823 62.4092 55 6 2974 8587, 7-2066; 6355 7680; 6645 6645 6685 7463 30-1446 63.6567 543 9 3064; 2253 5310 2446 6009; 7583 8596; 20-8072 5996 67-4019 51 105.76637 6.43248, 7-20873 83446 69.78817; 11.8262; 14.92442 0.0563 1.4416 63.6567 543 11 7936 4720 8442 6555 981641 8573 9898 3253 5284, 70-1533 49 12 8938 5961; 7-30018 8625 4482 9087; 15.0557 4465 82-057; 15164 13 9944 7206 1608 4.0705 8391 9923 1832 1832 1832 1832 1832 1832 1832 18	1				83°	1	: 1						
2					8.14435	9.51436		14.3007					
33.5,703.7; 4661. 6071 8,203.5a 9,400 5461 4823 4051 3711 60.305.5b 57 1001 7374 6165. 764 23.44) 62.505 553 5438 5156 62.56 61.38ap.56 20 2074 85891,20661 6355 7680 6655 6853 5438 5156 62.56 61.38ap.56 7 3960 9804 2204 83.76 9.7041 7045 7317 8546 4116 63.655 52 9.5074 23.44) 62.5076 7680 6655 6855 74.003 30.1466 63.656 75.50 9.5074 2253 5310 24.66 6009 7553 8596 20.85z 2599 67.4019 51 105.7693 6.43484 7.26873 8.3446 9.7851 11.8262 14.9244 20.2050 31.2416 68.7501 50 12.253 5310 24.66 6009 7553 8596 20.85z 2.5999 67.4019 51 12 89.38 5961 7.30018 8625 4482 9087 15.0557 4465 82.05 31.2416 68.7501 50 12 12 89.38 5961 7.30018 8625 4482 9087 15.0557 4465 82.05 71.6151 48 145.80053 8456 3100 2795 90.0011 9923 18.89 30 503 71.6151 48 145.80053 8456 3100 2795 90.0011 9923 18.89 30 503 71.6151 48 15.106 90.001 90					8370	6701							
1013 6165 7594 2344 06205 5853 5438 5156 6245 61.3829 566 51.0929 7374 2015 4345 4955 6458 6059 6273 8823 62.4993 550 7396 0804 2324 8376 0.7044 7045 7317 8466 4166 63.565 54 84049 6.4106 3.754 8.3046 6009 7853 8366 2.00872 9599 67.4019 51 17936 4720 8442 6059 7853 8366 2.00872 9599 67.4019 51 17936 4720 8442 6555 98164 8673 988 3233 3284 70.1533 4944 7206 1600 8.0705 7338 9504 72206 1600 8.0705 7338 9504 72206 1600 8.0705 7338 9504 72206 1600 8.0705 7338 9504 72206 1500 4766 4896 3101 12.0346 2571 8188 7303 76.3900 45 15 1966 0710 4766 4896 3101 12.0346 2571 8188 7303 76.3900 45 16 2823 6.50970 6389 7007 6007 0.128 8931 1221 3638 2049 6933 81.4470 4223 4777 4401 2234 7799 128 8931 1221 3638 3233 3834 7477 3660 7778 3504 4777 4401 2234 7799 128 8931 1201 3.0432 3.0538				6071	8.20352	0/00							
5 1992 7374 9125 4345 4935 6448 6059 6273 8823 62.4992 55 6 2974 85897.2666 6356 6355 7680 6645 6655 6737 8826 62.4992 55 7 3960 9804 2204 83764 70681 70481 7045 7317 8546 4116 64.8580 53 9 5941 2253 5310 2446 6099 7583 8596 20.0872 9599 67.4919 51 105.76637 6.43484 7.26873 8.34469 9.8817 11.8262 14.9244 20.2050 31.2416 68.7501 50 11 7936 4720 8442 6555 981641 8673 9898 3353 52847.01533 49 12 8938 5961 7.30018 8625 4482 9087 15.0557 4465 8206 71.6151 48 13 9944 7206 16.08 4.0705 7338 9504 1222 5691 32.1181 73.1390 47 14 3.80953 8456 3190 7070 7338 9504 1222 5691 32.1181 73.1390 47 15 1966 9710 4786 4896 3101 12.0346 2571 8188 7303 76.3900 45 17 4401 2234 7999 9128 8931 1201 3043 11.0747 3663 79.0434 43 16 5024 5353 9616 8.51259 10.0187 1632 4638 2049 6535 81.8470 42 15 5024 3503 9616 8.51259 10.0187 1632 4638 2049 6535 81.8470 42 15 5024 3503 9616 8.51259 10.0187 1632 4638 2049 6535 81.8470 42 15 1814 7339 4509 7718 1050 2946 6762 6056 7151 88.1363 32 15 1914 7339 4509 7718 1050 2946 6762 6056 7151 88.1363 33 15 90191 9921 7806 8.62078 1633 3838 8211 8813 4713 92.9085 37 24 1230 6.61219 9465 4878 1080 2946 6762 6056 7151 88.1363 32 2 9751 6627 6154 9833 1381 3390 7483 34749 34269 5968 50.4633 38 12 814 7339 4509 7718 1050 2946 6762 6056 7151 88.1363 32 2 9751 6827 6154 9833 1381 3390 7483 34749 34269 5968 50.4633 38 12 814 7339 4509 7718 1050 2946 6762 6056 7151 88.1363 32 2 9751 6827 6154 9838 8828 128 8831 8813 4713 92.9085 37 24 1230 6.61219 9465 8878 1683 8888 8211 8813 4713 92.9085 37 24 1230 6.61217 9488 8878 8878 8878 8878 8878 8878 887													
6	5									8823	62.4992	55	
8 46496.4.1026 3754 8.30406 3217 7448 7954 7902 6833 66.1055 52 9 5041 2253 5510 2446 6009 7583 8566 20.0872 9599 67.4019 510 5.76937 6.43484 7.26873 8.34496 9.78817 11.8262 14.9244 20.2056 31.2416 68.7501 50 12.8038 5651 7.30018 8825 4482 9087 15.0557 4465 8256 71.6151 48 13 9944 7206 1600 8.40705 7338 9504 1222 5501 32.1181 73.1390 47 44.58.9053 8456 3100 2795 9.90211 9923 1893 6932 4213 74.7922 74.1922		2974	8587	7.20661	1 1								
9 5641 2253 5310 2446 6000 7853 8566 20.0872 9599 67.4019 51 10 5.76937 6.43484 7.268738.34469 69.78817 11.8262 14.02461 20.2056 31.2446 68.7510 11 2 8938 55617.30018 8625 4482 9987 15.0557 4465 8205 71.6151 48 13 9944 7206 1600 8.40705 7338 9504 1222 55611 33.1181 73.1390 46 14 5.80953 8.456 3100 2795 9.0211 9923 1893 6.322 4213 74.7292 46 16 2982 6.50970 6389 7007 6007 0772 3244 9460 33.0452 78.1263 44 17 4001 2234 7999 9128 8931 1201 3943 1.0747 3662 79.0434 43 16 5024 3503 9616 8.51259 10.0187 1632 4638 2049 6935 81.8470 42 19 6051 4777 7.41240 3402 0483 2067 5340 3303 34.0273 83.8435 41 20 5.8780 6.56055 748287 18.55555 10.0780 112.505 15.6604 81.4704 34.3678 85.0393 82 21 8114 7339 4509 7718 1080 2946 6762 6056 7151 88.1436 33 23 5.9019 1 8027 6154 9893 1381 3330 7483 7463 55.0659 9.0463 33 23 5.9019 1 8027 6154 9893 1381 3330 7483 7483 65.0659 5.4633 33 23 5.9019 1 8027 6154 9893 1381 3300 7483 7483 65.0659 5.4633 33 23 5.9019 6.921 7806 8.62078 1683 3838 8211 8813 4313 92-9085 37 24 1336 6.61219 9465 4275 1988 4288 8945 22.0217 8066 95.4853 32 25 283 353 3831 2866 8701 2602 5199 16.0435 3081 5627 101.107 34 28 5448 6463 6176 3172 3224 6124 1952 6020 37.3579 101.023 32 29 50 5144 4487 8.79031 2913 5660 1190 4541 9560 104.171 18.540 29 610 7779 7872 5425 3338 6591 2722 77519 7686 110.892 31 38 6466 6.70450 7.6187 9964 4172 7536 4283 23.0577 61771 8.520 29 37 5430 8548 828 8254 8468 6862 5136 8981 6681 5321 9655 1321 273 320568 12.774 682 220 220 220 220 220 220 220 220 220 2	7												
16													
11	9	5 76037	6 43 48 4	m 068m3	8 34406	0009		74 0244	20.0072	31 2/16	68.7501	50	
12		7036			6555	0.816/1			3253	5284	70.1533	40	
13 9944 7266 1600 8.40705 7338 9504 1222 5691 32.1181 73.1300 47 14 5.80953 8456 3100 2795 9.00211 9923 1893 6932 4213 74.7292 46 15 1966 9710 4786 4896 3101 12.0346 2571 8188 7503 76.3290 45 16 2982 6.50970 6386; 7007 6007 0772 3254 9460 33.0452 78.1203 44 12 20 5.87080 6.56055 7.42871 8.514 20 160 1 4777 7.41240 3420 4683 3067 5340 33609 34.023 78.1845 41 20 5.87080 6.56055 7.42871 8.55555 10.0780 12.2505 15.6048 21.4704 34.3678 85.9398 40 22 9151 8627 6154 8993 1381 3309 7483 7426 350.6055 0.6656 715 188.1436 139 29 915 8627 6154 8993 1381 3309 7485 22.0217 8060 6.5636 745 188.1436 139 22 9151 8627 5665 10.0780 12.2505 15.6048 21.4704 34.3678 85.9398 40 12.2505 15.6048 21.2505 15.6048 21.4704 34.3678 85.9398 40 12.2505 15.6048 21.2505 15.6048 21.4704 34.3678 85.9398 40 12.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505 15.6048 21.2505									4465	8205	71.6151	48	
15 1 666 9710 4786 8896 3101 12.0346 2571 8188 7303 76.390 45 17					8.40705	7338			5691	32.1181	73.1390	47	
16 2928 (6.5097)	14	5.80953	8456			9.90211	9923	1893					
17	15			4786	4896	_	12.0346						
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Natural Co-secants.

		404		001	404	504		P. Part
Deg.	0'	10′	20′	30′	40′	50′		to 1'.
60	2.000000	2.010136	2.020393	2.030772	2.041276	2.051906	29	1044
61	062665	073556	084579	095739	107036	118474	28	1123
62	13co54	141781	153655	165681	177859	190195	27	1210
63	202689	215346	228168	241158	254320	267657	26	1308
64	281172	294869	308750	322820	337083	351542	25	1417
65	366202	381065	396137	411421	426922	442645	24	1539
66	458593	474773	491187	507843	524744	541896	23	1678
67	559365	576975	594914	613126	531618	650396	22	1835
68	669467	688387	708514	728504	748814	769453	21	2015
69	790428	811747	833419	855451	877853	900635	20	2222
7C	2.923804	2.947372	2.971349	2.995744	3.020569	3.045835	19	2461
71	3.071553	3.097736	3.124396	3.151545	179198	207367	18	2740
72	236068	265315	295123	325510	356490	388082	17	3068
73	420304	453173	486711	520937	555871	591536	16	3458
74	627955	665152	703151	741978	781660	822225	15	3925
75	863703	906125	943522	993929	4.039380	4.085913	14	4492
76	4.133565	4.182378	4.232394	4.283658	336215	390116	13	5190
77	445411	502157	560408	620226	681675	744821	12	6062
78	809734	876491	945169		5.088628	5.163592	11	7171
79	5.240843	5.320486	5.402633	487404	574926	665333	10	8612
80	5.758770	5.855392	5.955362	6.058858	6.166067	6.277193	9	
81	6.392453	6.512081	6.636329	6.765469	6.899794	7.039622	8	
82	7.185297	7.337191	7.495711	7.661298	7.834433	8.015645	7	
83	8.205509	8.404659	8.613790	8.833671	9.065151	9.309170	6	
84	9.566772	9.839123	10.12752	10.43343	10.75849	11.10455	5	
85	11.47371	11.86837	12.29125	12.74549	13.23472	13.76311	4	
86	14.33559	14.95788	15.63679	16.38041	17.19843	18.10262	3	
87	19.10732	20.23028	21.49368	22.92559	24.56212	26.45051	2	
88	28.65371	31.25758	34.38232	38.20155	42.97571	49.11406	I	
89	57.29869	68.75736	85.94561	114.5930	171.8883	343.7752	0	
	60′	50′	40′	30′	20′	10′	Deg.	
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Natural Co-secants.

LENGTHS OF CIRCULAR ARCS.

			Burar		01110011.11				
			Degrees.				Minutes.		Seconds.
0	.0174533	26	.4537856	51	.8901179	' I	.0002909	ľ	.0000048
2	.0349066	27	.4712389	52	.9075712	2	.0005818	2	.0000097
3	.0523599	28	.4886922	53	.9250245	3	.0008727	3	.0000145
1 4	.0698132	29	.5061455	54	.9424778	4	.0011636	4	.0000194
5	.0872665	30	.5235988	55	.9599311	5	.0014544	5	.0000242
6	.1047198	31	.5410521	56	.9773844	6	.0017453	6	.0000291
7	.1221730	32	.5585054	57	.9948377	7	.0020362	7	.0000339
8	.1396263	33	.5759587	58	1.0122910	8	.0023271	8	.0000388
1 9	.1570796	34	.5934119	59	1.0297443	9	.0026180	9	.0000436
10	.1745329	35	.6108652	60	1.0471976	10	.0029089	10	.0000485
11	.1919862	36	.6283185	65	1.1344640	II	.0031998	II	.0000533
12	.2094395	37	6457718	70	1.2217305	12	.0034907	12	.0000582
13	.2268928	38	.6632251	75	1.3089969	13	.0037815	13	.0000630
14	.2443461	39	.6806784	80	1.3962634	14	.0040724	14	.0000679
15	.2617994	40	.6981317	85	1.4835299	15	.0043633	15	.0000727
16	.2792527	41	.7155850	90	1.5707963	16	.0046542	16	.0000776
17	.2967060	42	.7330383	100	1.7453293	17	.0049451	17	.0000824
18	.3141593	43	.7504916	110	1.9198622	18	.0052360	18	.0000873
19	.3316126	44	.7679449	120	2.0943951	19	.0055269	19	.0000921
20	.3490659	45	.7853982	130	2.2689280	20	.0058178	20	.0000970
21	.3665191	46	.8028515	140	2.4434610	25	.0072722	25	.0001212
22	.3839724	47	.8203047	150	2.6179939	30	.0087266	30	.0001454
23	.4014257	48	.8377580	160	2.7925268	40	.0116355	40	.0001939
24	.4188790	49	.8552113	170	2.9670597	50	.0145444	50	0002424
25	.4363323	50	.8726646	180	3.1415927	60	.0174533	60	0002909

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30			9611	5740	9483	6959 7175	02	0 45
45		4 :	9561	5912	9451	7390		30
9 0 9877 1564 9754 312 9870 1607 9740 321 30 9863 1650 9726 330 45 9856 1693 9711 338 10 0 9848 1736 9696 347 15 0.9840 0.1779 1.9681 0.355 30 9833 1822 9665 364 45 9825 1865 9649 373 11 0 9816 1908 9633 381 15 9808 1951 9616 390 45 9799 1994 9598 398 45 9790 2036 9581 407 15 9772 2122 979 9563 415 9763 2164 9526 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466	11		9534	6085	9418	7606		15
15	11	1 : 1	9508	6257	9384	7822	81	0
30	11 -		9480	6430	9350	8037		45
45 9856 1693 9711 338 9696 347 9696 347 9696 347 9696 347 9696 347 9696 347 9696 347 9696 349 9696 349 9696 3696 3696 3			9451	6602	9314	8252		30
15 0.9840 0.1779 1.9681 0.355 30 9833 1822 9665 364 45 9825 1865 9649 373 11 0 9816 1998 9633 381 15 9808 1951 9616 390 45 9799 1994 9598 398 45 9790 2036 9581 407 12 0 9781 2079 9563 415 9772 2122 9545 424 956 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466		5080	9422	6774	9278	8467		15
30 9833 1822 9665 364 45 9825 1865 9649 373 9816 1908 9633 381 15 9808 1951 9519 9598 398 45 9799 1994 9598 398 45 9790 2036 9581 407 12 0 9781 2079 9563 415 9772 2122 9565 424 956 432 45 0,9753 0,2207 1,9507 0,441 15 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466	9544	5209	9392	6946	9240	8682	80	0
30 9833 1822 9665 364 45 9825 1865 9649 373 9816 1908 9633 381 15 9808 1951 9519 9598 398 45 9799 1994 9598 398 45 9790 2036 9581 407 12 0 9781 2079 9563 415 9772 2122 9565 424 956 432 45 0,9753 0,2207 1,9507 0,441 15 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466	2.9521		3.9362		4.9202	0.8897		45
45		5467	9330	7289	9163	9112		3о
15			9298	7461	9123	9326		15
30 9799 1994 9598 398 45 9790 2036 9581 407 12 0 9781 2079 9563 415 30 9763 2164 9526 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466	11		9265	7632	9081	9540	79	0
45 9790 2036 9581 407 12 0 9781 2079 9563 415 15 9772 2122 9545 424 33 9763 2164 9526 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466	9424	5853	9231	7804	9039	9755		45
12 o 9781 2079 9563 415 9772 2122 9565 424 9526 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466		5981	9197	7975	8996	9958		30
15 9772 2122 9545 424 30 9763 2164 9526 432 45 0.9753 0.2207 1.9507 0.441. 13 0 9744 2250 9487 449 15 9734 2292 9468 458. 30 9724 2334 9447 466			9162	8146 8316		0396 0396	_0	15
35 9763 2164 9526 432 45 0.9753 0.2207 1.9507 0.441 13 0 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466			9126	8487	8862	0609		45
45 0.9753 0.2207 1.9507 0.441. 13 0 9744 2250 9487 449. 15 9734 2292 9468 458. 30 9724 2334 9447 466			9052	8658	8815	9822		30
13 o 9744 2250 9487 449 15 9734 2292 9468 458 30 9724 2334 9447 466								
15 9734 2292 9468 458. 30 9724 2334 9447 466	2.9200	67/0	8975	8998	4.8707	1248		15 0
30 9724 2334 9447 466			8935	9168	8669	1460	17	45
	11 -	1	8895	9338	8618	1672		30
45 9713 2377 9427 475		1 ' ^	8854	9507	8567	1884		-5
45 9713 2377 9427 475 14 0 9703 2419 9406 483		امت ا	8812	9677	8515	2096		o
15 9692 2462 9385 492			8769	9846	8462	2308		.45
30 9681 2504 9363 500				1.0015	8407	2519		30
45 9670 2546 9341 509	11 -	7638	8682	0184	8352	2730		1 5
15 0 9659 2588 9319 517		7765	8637	o353	8296	2941	75	0
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0	15	5.9999	0.0262	6.0000	0.0305	7.9999	0.0349	8.9999	0.0393	9.9999	0.0436	89	45
1	30	9998	0524	9997	0611	9997	0698	9997	0785	9996	0873	1	30
	45	9995	0785	9994	0916	9993	1047	9992	1178	9991	1309		15
:	0	9991	1047	9989	1222	9988	1396	9986	1571	9985	1745	89	0
	15 30	9986	1309 1571	9983 9976	1527 1832	9981	1745 2034	9979 9969	1963 2356	9976 9966	2181 2618		45 30
	45	9979 9972	1832	9970	2138	9963	2443	9958	2748	9953	3054		15
2	0	9963	2094	9957	2443	9951	2792	9945	3141	9939	3490	88	0
	15	9954	2356	9946	2748	9938	3141	9931	3533	9923	3926		45
	30	9943	2617	9933	3053	9924	3490	9914		9905	4362		30
			0.2879						0.4318	9.9885		^	15
3	0	9918	3140	9904	3664	9890	4187	9877	4710	9863	5234	87	0
l	15 30	9904 9888	3402 3663	9887 9869	3968 4273	9871 9851	4535 4884	9855	5102 5494	9839	5669 6105		45 30
	45	9872	3924	9850	4578	9829	5232	9807	5886	9786	6540		15
4	o	9854	4185	9829	4883	9805	5581	9781	6278	9756	6976	86	0
	15	9835	4447	9808	5188	9780	5929	9753	6670	9725	7411		45
	30	9815	4708	9784	5492	9753	6277	9723	7061	9692	7846		30
_	45	9794	4968	9760	5797	9725	6625	9691	7453	9657	8281	0.5	15
5	0	9772	5229	9734	6101	9696	6972	9658	7844	9619	8716	00	0
	15 30		0.5490 5751	6.9706 9678		7.9664 9632	0.7320 7668	9586	0.8235 8626	9.9580 9540	9585		45 30
	45	9724 9698	6011	9648	6709 7013	9597	8015	9547	9017		1.0019		15
ď	0	9671	6272	9617	7317	9562	8362	9507	9408	9452	0453	84	0
ĺ	15	9643	6532	9584	7621	9525	8709	9465	9798	9406	0887		45
	3с	9614	6792	9550	7924	9486	9056		1.0188	9357	1320		30
_	45	9584	7052	9515	8228	9445	9403	9376		9307	1754	0.0	15
7	15.	9553 9520	7312	9478 9440	8531 8834	9404	9750	9329 9280	0968 1358	9255	2187 2620	83	45
	30	9487	7832	9440	9137	9316	0442	9230	1747	9200	المسما		30
İ	- 11				0.9440		1 1			9.9087	1 1		15
8	0	9416	8350	9319	9742	9221	1134	9124		9027	3917	82	0
	:5	9379	8610		1.0044	9172	1479	9069	1 1	8965	4349		45
1	30	9341	8869	9231	0347	9121	1825	9011	3303	8902	4781		30
	45	9302	9:27	9185	0649	9069	2170	8953		8836			15
9	0 15	9261 9220	9386 9645	9138	0950 1252	9015 8960		8892 8830		8769 8700		81	o 45
	30	9177	9903	9040		8903		8766					30
	45	9133		8989		8844		8700	1 4 . 1	8556	1 1		15
10	0	9088	0419	8937	2155	8785	3892	8633	5628	8481	7365	80	o
	15	5.9042	1.0677	6.8883	1.2456	7.8723	1.4235	8.8564	1.6015	9.8404	1.7794		45
	30	8995		8828	2756	8660		8493		8325			30
	45	8947	1191	8772				8421		8245	1		15
XI	15	8898 8847		8714 8655		8463	1	8346 8271	1	8163		79	45
	30	8795	1962	8595		8394				7992	1 1		30
	45	8743		8533			6291			7905	2.0364		15
12	0	8689	2475	8470	4554	8252	6633	8033	8712	7815	0791		o
	15	8634							9096	7723	1218		45
	30	8578		11	1	11	1 '				1 1		30
-0	45		1.3242	6.8274	1.5449	7.8027	1.7656	8.7781	1.9863		2.2070		15
13	0 15	846 <u>2</u> 8403		8206 8137				7604	0628			77	0
	30	8342									3345		45 30
	45	8281					9015	7421	1392	7134			15
14	0	8218	4515	7921	6935	7624	9354	7327	1773	7530	4192		0
	15	8154		11	1		1 / /		2154	6923			45
	3o 45	8089			7527		2.0030		. 1	11			30
15	40 0	8023 7956		7693 7615									15 0
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L		Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.		
15	15 30					2.8944 8909			1.0521 0690	4 823g			45 30
16	45 o	9613	2756	9249 9225	5513	8838	8260	8450	0858	8123			15
	15 30	9588	2798 2840	9201 9176	5680	8765	8395 8520						45 30
17	45 o	1	2882 2924		5764 5847			11		7879 7815	4410	- []	15
'	15 30	9550	2965 3007	9100 9074	5931	8651	8896	8201	1862	7751	4827		45 30
	45	0.9524	0.3049	1.9048	0.6097	2.8572	0.9146	3.8096	1.2195	4.7620	1.5243		15
13	15	9511 9497	3090 3132	8994		8491	9271 9395	8042 7988	2361 2527	7553 7485	5658	72	45
	3o 45	9483 9469	3173 3214	8939	6429	8408	9519 9643	7877	2858	7347	6072		30 15
19	o 15	9455 9441	3256 3297	8910 8882	6511 6594	8366 8323	9891	7764	3023 3188			71	o 45
	3o 45	9426	3338 3379	8853 8824		8235	0138	7706 7647	335 ₂ 35 ₁₇				30 15
20	o 15	9397 0.9382	3420	8794 1.8764	6840	8191 2.8146	0261	7588	368í 1.3845	6985	7101	70	o 45
	3o 45	9367 9351	35 ₀₂ 35 ₄₃	8733 8703	7004 7086	8100	0506 0629	7467	4008 4172	6834 6757	7510		30 15
21	0	9336	3584	8672	7167	8007	0751	7343	4335	6679			0
	30	9320	3624 3665	8640 8608	7249 7330	7960 7913	0873 0995	7217	4498 4660		8325		45 30
22	45 o	9288 9272	3706 3746	8576 8544	7411 7492	7816	1117	7087	4822 4984	6440 6359	8730	68	0
	15 30	9255	3786 3827	8511 8478	7573 7654	7766 7716	1359 1481	7022 6955	5146 5307	6277 6194	8932 9134		45 30
23	45 o	0.9222 9205	0.3867 3907	1.8444 8410	0.7734 7815	2.7666 7615	1.1601	3.6888 6820	1.5468 5629	4.6110 6025	1.9336 9537	67	15 0
	15 30	9188 9171	3947 3987	8376 8341	7895 7975	7564 7512	1842 1962	6752	5790 5950	5940 5853	9737	,	45 30
24	45	9153 9135	4027 4067	8306 8271	8o55 8135	7459 7406	2082 2202	1 1	6110		2.0137 0337	66	15 0
	:5 30	9118	4107 4147	8235 8199	8214 8294	7353 7299	2322 2441	6470 6398	6429 6588	5588 5498	o536 o735		45 30
25	45	9081	4187 4226	8163 8126	8373 8452	7244	2560 2679	6326 6252	6746	5407 5315	0933	65	15
23	15	0.9045	0.4266	1.8089	0.8531		1.2797	3.6178		4.5223	2.1328	0.3	45
	3o 45	9026 9007	43o5 4344	8052 8014	8610 8689	7078	2915 3033	6103 6028	7220 7378	5129 5035	1526 1722		30 15
26	o 15	8988 8969	4384 4423	7976 7937	8767 8846	6964 6906	3151 3269	5952 5875	7535 7€92	4940 4844	1919 2114	64	o 45
	3o 45	8949 8930	4462 4501	7899 7860	8924 9002	6848 6789	3386 35o3	5797 5719	7848 8004	4747 4649	2310 2505		30 15
27	o 15	8910 8890	4540 4579	7820 7780	9080 9157	6730 6671	3620 3736	5640 5561	816o 8315	4550 4451	2700 2894		o 45
	30	8870 c 8850	4617	7740	9235	6610 2.6550	3852	5480	8470	4351 4 .42 49	3087		30 15
28	15	8829 8809	4695 4733	7659 7618	9389 9466	6488 6427	4084 4200	5318 5236	8779 8933	4147 4045	3474 3666	62	45
	30 45	8788	4772 4810	7576	9543	6365 6302	4315	5153 506g	9086	3941 3836	3858 4049		30
29	О	8767 8746 8705	4848	7535 7492	9620 9696	6239	4430 4544	4985	9240 9392 9545	3731	4240 4431	61	0 45
	30 /5	8725 8704	4886	7450 7407	9772 9848	6175	4659 4773	4900 4814	9697	3625 3518	4621		30
30	45 0	8682 8660	4962 5000		9924	6046 5981	4886 5000		9849 2.0000	3410 3301	4811 5000	60	15 0
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15	15	5.7887	1.5782	6,7535	1.8/12	7.7183	2.10/12	8.6831	2.3673	0.6470	2.6303	° 74	45
	30	7818	6034	7454	8707	7090	1379	6727	4051	6363	6724	/-	30
	45	7747	6286	7372	9001	6996	1715	6621	4430	6246	1 1		1 5
16	0	7676	6538	· /	9295	6901	2051	6514	1 : 51	6126		74	0
	15 30	7603 7529	6790 7041	7203	9588 9881	6804 6706	2386 2721	1 - 1 1					45 30
	45	7454	7292		2.0174	6606			5938				15
17	0	7378	7542	6941	0466	6504			6313		1 1 1	73	0
	15	7301	7792	6851	0758	6402		5952		5502			45
	30	7223	8042	6760	1049	6297	4056	5835	7064		3.0071		30
18	45	7063	8541	6574	2.1341 1631	7.0192 6085	4721	5595	2.7438 7812	5106	0902	-	15
10	15	6982	8790	6479	1921	5976	5053			4970		72	o 45
	30	6899	9038	6383		5866	5384	5349		4832	1730		30
	45	6816	9286			5754	5715	5224					15
19	0	6731	9534	6186		5641	6045 6375		9301	4552	2557	71	0
	15 30	6645 6558	9781 2.0028	6086 5985		5527 5411	6705		9672 3.0043	4409 4264			45 30
	45	6471	0275	5882	3654	5294			0413	4118	3792		15
20	o	6382	0521	5778	3941	5175	7362	4572		3969	4202	70	0
	15	5.6291	2.0767	6.5673	2.4228	7.5055	2.7689	8.4437	3.1151	9.3819			45
	30	6200	1012	5567	4515	4934	8017	4300	1519	3667	5021		30
	45	6108 6015	1257 1502	5459	4800 5086	4811	8343 866g	4162		3514 3358	5429 5837	6.	15
۶I	0 15	5920	1746	5351	5371		8995	1 1	2253 2619		6244	109	o 45
	30	5825	1990	1 - '	5655	4433	9320			-3042			30
	45	5729	2233	5017	5939	4305	9645	3593		2881			15
22	0	5631	2476	4903	6222	4175	9969		3715			68	0
	15 30	5532 5433	2719 2961	4788 4672	6505 6788	3910	3.0292 0615	3299 3149	4078 4442	2554 2388	7865 8268		45 35
	- 1	5.5332		6.4554	' '	7.3776			3.4804	1			15
23	0	5230	3444	4435	7351	3640	1258	2845				67	0
	15	5127	3685	4315	7632	3503	1580	2691	5527	1879			45
	30	5024	3925	4194			1900	2535			1		30
24	45	4919 4813	4165	4072 3948	8192	3225 3084	2220 2539				4.0275 0674	66	15
24	15	4706	4404 4643	3823	8472 8750	2941	2858	2219 2059				66	o 45
	30	4598	4882	3697	9029	2797	3175	1897					30
_	45	4489	5120	3570		2651	3493	1733	7679				1 5
25	0	4378	5357	3442	9583	2505	3809		1	l l	2262	65	0
	15			6.3312	2.9860				3.8391				45
	3o 45	4155	5831 6067		3.0136 0411	2207	4441	1233	, , ,	0259			30 15
26	0	3928	6302		11		1 2 1			8.9879		64	0
	15	3812	6537	2781	0960	1750	5383	0719	9806	9687	4229	1	45
	30	3696	6772	2645		1595			4.0158		4620		30
27	45	35 7 9 3460	7006 7239	2509 2370	1507 1779	1438 1281	6008					63	15
27	15	3341	7472					0012			5787	03	45
	3о	3221	7705					7.9831		8701			30
	45	5.3099	2.7937	6.1949	3.2593	7.0799		7.9649	4.1905	8.8499	4.6561		15
28	0	2977	8168	I F	I i	0636		9465		11 - 2			0
	15 30		8399								7332		45
	45	2729 2604									7716 8099		30 15
29	0	2477		1223	3937	6.9970	8785	8716	3633				0
ĺ .	15	2350	9317	1075	4203	9800	9090	8525	3976	7250	8862		45
	30	2221						8332					30
30	45 o	2092	977 ³ 3.ocoo	0774			9697 4.0000			11	9622		15 0
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° 3°	15	0.8638	0.5038	1.7277	1.0075	2.5015	1.5113	3.4553	2.0151	4.3102	2 5180	50	45
017	30	8616	5075	7233	0151	5849	5226	4465	0302	3081	5377	39	30
	45	8594	5113	7188	0226	5782					5565		15
Sr	0	8572	5150		0301				1 -	11	1		0
	15	8549	5188	7098	0375	5647	5563		, ,				45
	3o 45	8526 8504	5225 5262							ll			30
32	45	8480	5299		0598		5898			11 -			15 0
	15	8457	5336	6915	0672								45
	30	8434	5373	6868	0746	5302	6119	3736		11	6865		30
	45	0.8410	0.5410	1.6821	1.0819	2.5231	1.6229	3.3642	2.1639	4.2052	2.7049		15
33	0	8387	5446	6773	0893	5160	6339	3547	1786	1934	7232	57	О
	15	8363	5483	6726	0966				. 1932	1 - :			45
	30	8339	5519 5556	6678	1039		6558	3355	2077	1694	7597		30
34	45 o	8315 8290	5592	6629 6581	1111	4944 4871	6667 6776	3259 3162	2223 2368	1573 1452	7779 7960	56	15
54	15	8266	5628	6532	1256	4798	6884		2512		8140	.,0	45
	30	8241	5664	6483	1328		6992	2965	2656		8320		30
	45	8216	5700	6433	1400	4649	7100		2800	1082	8500		15
35	0	8192	5736	6383	1472	4575	7207		2943	0958	8679	55	0
	15	0.8166	0.5771	1.6333	1.1543	2.4499	1.7314	3.2666	2.3086	4.0832	2.8857		45
	30	8141	5807	6282	1614	4423	7421	2565	3228	0706	9035		30
26	45	8116	5842	6231	1685	4347	7527	2463	3370		9212		15
36	0 15	8090 8064	5878	6180	1756	4271	7634	2361	3511		9389	54	0
	30	8039	5913 5948		1826 1896	4193	7739 7845	2258 2154	3 65 2		9565 9741		45 30
	45	8013	5983	6025	1966	4038	7950	2050	3933	0063	9916		15
37	o	7986	6018	5973	2036	3959	8054	1 .1		3.9932		53	0
•	15	7960	6053	5920	2106	3886	8159	1840	4212	9800	0265		45
	30	7934	6088	5867	2175	3801	8263	1734	4350	9668	o438		3о
	45	0.7907		1.5814		2.3721	1.8367	3.1628		3.9534			1 5
33	0	7880	6157	5760	2313	3640	8470	1520	4626	9403	0783	52	0
	15	7853	6191	5706	2382	3560	8573	1413	4764	9266	0955		45
	3o 45	7826	6225 6259	5652 5598	2450 2518	3478 3397	8675 8778	1304	4901 5037	9130 8994	1126 1296		30 15
39	0	7799 7771	6293	5543	2586	3314	8880	1086	5173	8857	1466	51	0
- 7	15	7744	6327	5488	2654	3232	8981	0976	5308	8720	1635		45
	30	7716	6361	5432	2722	3149	9082	o865	5443	8581	1804		30
_	45	7688	6394	5377	2789	3065	9183	0754	5578	8442	1972	_	15
40	0	7660	6428	5321	2856	2981	9284	0642	5712	8302	2139	50	0
			0.6461			2.2897	1.9384	3.0529		3.8162			45
	30	7604	6494	5208	2989	2812	9483	0416	5978	8020	2472		30
41	45 o	7576 7547	6528 6561	5151 5094	3055 3121	2727 2641	9583 9682	o3o3 o188	0110 6242	7878 7735	2638 2803	100	15 0
44.1	15	7518	6593	5037	3121	2555	9780	0074	6374	7592	2967	44	45
	30	7490	6626	4979	3252	2469	9879	2.9958	6505	7448	3131	Ì	30
	45	7461	6659	4921	3318	2382	9976	9842	6635	7303	3294		15
42	0	7431	6691	4863	3383		2.0074		6765		3457	48	0
	15	7402	6724	4804	3447	2207	0171	9609	6895	7011	3618		45
	30	7373	6756	4746	3512	2118	0268	9491	7024	6864	3780		30
12	11							2.9373		6568	4100	1	15
43	o 15	7314 7284	6820 6852	4627 4567	3640 3704	1941	o46o o555	9254	7280 7407	6419	4259	47	o 45
	30	7254	6884	4507	3767	1761	0651	9015	7534	6269	4418		30
	45	7224	6915	4447	3830	1671	0745	8895	7661	6118	4576		15
44	o	7193	6947	4387	3893	1580	0840	8774	7786	5967	4733		0
	15	7163	6978	4326	3956	1489	0934	8652	7912	5815	4890		45
	30	7133	7009	4265	4018	1398	1027	8530	8036	5663 5509	5045 5201		30 15
45	45 o	7102	7040 7071	4204 4142	4080 4142	1306 1213	1120	8407 8284	8161 8284	5355	5355	45	10
45		Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	75	
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30	15	5.1830	3.0226	6.0468	3.5264	6.9107	4.0302	7.7745	4.5340	8.6384	5.0377	59	45
	30	1698	0452	0314	5528	8930	0603	7547	5678	6163	0754		30
1	45	1564			5791	8753		7347	6016			_	15
31	0	1430			6053	8573		11	6353			59	0
1	15	1295 1158		5.9844 9685	6314	8393 8211	1502 1800	6942 6738	6690	5491 5264			45 30
	30 45	1021	1573	9525	6835	8028	ı	6532	7359		1		15
32	0	0883	1795		7094	11	2394	11		4805	2992	58	0
	15	0744	2017	9201	7353	7658	2689	6116					45
	30	0603	2238	9037	7611	7471	2984	5905	8357	4339			3 o
	45	5.0462		5.8873		6.7283			4.8688	8,4104	5.4097		15
33	0	0320	2678	8707	8125	7094	3571	5480	9018	3867	4464	57	0
	15	0177	2898	8540	8381	6903	3863	5266	9346	3629			45
	3o 45	0033 4.9888	3116 3334		8636 8890		4155 4446	5050 483a	9674 5.0001	3389 3147	5194 5557		30 15
34	40	9742	3552		9144		4735	4613	0327		5919	56	0
1	15	9595	3768	7861	9396	6127	5024		0652	2659	6280		45
	30	9448	3984	7689	9648	5930	5312	4171	0977	2413	6641		30
	45	9299	4200	7515	9900	5732	5600	3948	1300	2165	7000		15
35	0	9149	4415		4.0150	5532	5886	3724	1622	1915	7358	55	0
	15	1 - 5 5 1	3.4629			6.5331	4.6172	7.3498		8.1664			45
	30	8847	4842	6988	0649	5129	6456	3270 3042	2263	1412	8070		30
36	45	8694 8541	5055 5267	6631	0897 1145	4926	6740 7023	2812	2582 2901	1157	8425 8779	54	15 0
30	15	8387	5479	6451	1392	4516	7305	2580	3218	0644	9131	34	45
	30	8231	5689		1638	4309	7586	2347	3534	o386	9482		30
	45	8075	5899	6088	1883	4100	7866	2113	3849	0125	9832		15
37	0	7918	6109	5904	2127	3891	8145	1877	4163		6.0182	53	0
	15	7760	6318	5720	2371	3680	8424	1640	4476	9600	0529		45
	30	7601	6526	5535	2613	3468	8701	1402	4789	9335	0876		30
20	45			5.5348				7.1162		7.9069	6.1222		:5
38	0 15	7281 7119	6940 7146	5161	3096 3337	3041 2825	9253 9528	0921	5410 5718	8801 8532	1506	52	3 45
	30	6956	7351	4972 4783	3576	2609	9801	0435	6026		1909 2251		30
	45	6793	7555	4592	3815		5.0074	0190	6333	7988	2592		15
39	0	6629	7759	4400	4052	2172		6.9943	6639	7715	2932	51	o
'	15	6464	7962	4207	4289	1951	0616	9695	6943	7439	3271		45
	30	6297	8:65	4014	4525	1730	0886	9446	7247	7162	3608		30
40	45	6131 5963	8366 856 ₇	3819 3623	4761	1507	1155	9196	7550 7851	6884 6604	3944	50	15
40	0				4995	1 1		6 9602			4279	30	0
	15 30	4.5794 5624	8967	5.3426 3228	5461	0.1059	1956	6.8691 8437	8450	7.63 2 3 6041	4945		45 30
i	45	5454	9166	3030	5693	0605	2221	8181	8748	5756	5276	-	15
41	0	5283	9364	2830	5924	0377	2485	7924	9045	5471	5606	40	0
	15	5110	9561	2629	6154	0147	2748	7666	9341	5184	5935	1	45
1	30	4937	9757	2427	6383	5.9916	3010	7406	9636	4896	6262		3 o
1	45	4763	9953		6612	9685	3271	7145	9929	4606	6588	100	15
43	o 15		4.0148	2020	7066	9452	353o 3789		0513	4314 4022	6913 7237	48	0 45
1	30	4413 4237	o342 o53 5	1815	7000	9217 8982	4047	6355	0803	3728	7559		45 30
-	l l			5.1403						7.3432			15
43	45	3881	0920	1195	7740	8508	4560	5822	1380	3135	8200	107	0
1	15	3702	1111	0986	7963		4815	5553	1666	2837		*/	45
	30	3522	1301	0776	8185	8030	5068	5284	1952	2537	8835		30
	45	3342	1491	0565	8406	7789	5321	5013	2236	2236	9151		15
44	0	3160	/	0354	8626	7547	5573	4741	2519	1934	9466	46	0
	15 30	2978 2795	1867	0141 4.9928	8845 9064	7304 7060	5823 6073	4467 4193	2801 3082	1630	9779 7.0091		45
	45	2611	2241	9713	9281	6815	6321	3917	3361	1019	0401		30 15
45	0	2426	2426	9497	9497	6569	6569	3640	3640	0711		45	0
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LATITUDE. 8° 90 40 50 60 70 10° 11° 12° 664.1 65.1 22.1 82.6 43.3 01.4 61.7 04.1 23.1 05.1 62.7 83.6 44.3 02.4 66.1 63.7 03.4 24.1 84.6 45.3 06.1 67.1 64.7 25.1 85.6 46.3 04.4 07.1 68.2 05.4 65.7 26.1 86.6 47.3 08.2 69.2 48.3 06.4 66.7 87.6 27.1 00.2 70.2 28.1 88.6 07.4 67.7 49.3 10.2 71.2

Min.

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240.2 300.4 360.7 421.1 481.6 542.2 603.1 0.0 60.0 180.1 725.3 120.0 81.1 1.0 61.0 41.2 26.3 I 21.0 I 42.2 82.1 27.4 2 2.0 62.0 22.0 83.1 3.0 43.2 3 63.o 23.0 28.4 3 - 4 5 4 4.0 64.0 24.0 84.1 44.2 29.4 5 5.0 65.0 25.0 85.1 45.2 30.5 6 6 86.1 31.5 6.0 66.0 26.0 46.2 87.1 32.5 7.0 8.0 67.0 27.0 47.2 78 78 68.0 88.1 48.2 68.7 50.3 33.5 28.0 08.4 29.1 80.6 11.2 72.2 80.1 30.1 51.4 73.3 34.5 9.0 69.0 20.0 49.2 09.4 69.7 90.7 12.2 9 9 130.0 190.1 250.2 310.4 370.7 431.1 491.7 552.4 613.2 674.3 735.6 10.0 70.0 10 ΙO 75.3 71.0 92.7 тт 11.0 31.0 91.1 51.2 11.4 71.7 32.1 53.4 14.2 36.6 11 92.1 76.3 72.0 52.2 33.1 93.7 54.4 15.3 37.6 12 12.0 32.0 12.4 72.7 73.0 93.1 13.4 55.4 77.3 13 13.0 33.0 53.2 73.7 34.2 94.7 16.3 38.6 **13** 74.0 95.7 78.4 54.2 14:4 35.2 56.4 17.3 39.6 :4 14 14.0 34.0 94.1 74.7 75.0 15 15 55.2 75.7 36.2 96.7 57.4 18.3 15.0 35.0 95.1 15.4 79.4 40.7 76.8 16 16.0 76.0 36.0 96.1 56.2 16.4 37.2 58.4 19.3 80.4 41.7 16 97.7 38.2 59.4 20.3 42.7 37.0 57.2 17.5 77.8 98.7 81.4 17 17.0 77.0 97.1 17 43.7 78.0 98.1 78.8 18 18.0 38.0 58.2 18.5 39.2 99.8 60.5 21.3 82.4 18 83.5 44.8 39.0 59.2 19.5 40.2 500.8 61.5 22.4 19 19 19.0 79.0 99.1 79.8 140.0 200.1 260.2 320.5 380.8 441.2 501.8 562.5 623.4 684.5 745.8 80.0 20 20 20.0 63.5 24.4 85.5 46.8 61.3 21.5 81.8 42.2 02.8 21 21 21.0 81.0 41.0 01.1 64.5 86.5 62.3 82.8 43.2 03.8 25.4 47.8 22 22 22.0 82.0 42.0 02.1 22.5 65.5 23 83.0 43.0 03.1 63.3 23.5 83.8 44.2 04.8 26.4 87.5 48.9 23 23.0 84.8 45.2 05.8 66.6 27.4 88.6 49.9 24 44.0 04.1 64.3 24.5 24 24.0 84.0 85.8 06.8 67.6 28.5 89.6 50.9 25 65.3 25.5 46.3 25 25.0 85.ol 45.0 05.1 68.6 29.5 90.6 51.9 26 26 66.3 26.5 86.8 47.3 07.8 26.0 86.0 46.0 06.1 69.6 30.5 27 27.0 87.0 47.0 07.1 67.3 27.5 87.8 48.3 08.9 91.6 53.0 37 28 68.3 28.5 88.8 49.3 70.6 31.5 92.6 54.0 28 28.0 88.0 48.0 08.1 09.9 93.6 55.o 71.6 32.5 89.0 09.1 69.3 29.5 89.8 50.3 10.9 29 29.0 49.0 29 150.0 210.1 270.3 330.5 390.8 451.3 511.9 572.6 633.5 694.7 756.0 30 30 30.0 90.0 31 71.3 31.5 91.8 52.3 12.9 73.7 34.6 95.7 57.1 31 31.0 91.0 51.0 II.I 13.9 96.7 58.1 32 52.0 12.1 72.3 32.5 53.3 74.7 35.6 32 32.0 92.9 92.0 14.9 73.3 93.0 53.1 13.1 33.5 93.9 54.3 75.7 36.6 59.1 33 33 33.0 97.7 15.9 98.7 34.5 55.3 76.7 37.6 34 34 34.0 94.0 54.1 14.1 74.3 94.9 75.3 16.9 35 35.o 95.0 55.1 15.1 35.5 95.9 56.3 77.7 38.6 99.8 61.1 35 78.7 36 36 36.0 56.1 16.1 76.3 36.5 96.9 57.3 0.81 39.6 700.8 62.2 96.0 37 77.3 37.5 97.9 98.9 58.4 19.0 40.7 01.8 63.2 37 37.0 57.1 17.1 97.0 79.7 80.8 38 38.0 08.0 78.3 38.5 02.8 64.2 38 58.1 18.1 59.4 20.0 41.7 59.1 79.3 39.6 60.4 21.0 81.8 42.7 03.8 39 39 39.0 19.1 99.0 99.9 40.0 | 100.0 | 160.1 | 220.2 | 280.3 | 340.6 | 400.9 | 461.4 | 522.0 | 582.8 | 643.7 | 704.9 | 766.3 40 40 23.0 83.8 44.7 05.9 67.3 41 41 41.0 01.0 61.1 21.2 81.3 41.6 01.9 62.4 06.9 42 82.3 63.4 24.0 84.8 45.8 68.3 42 42.0 02.0 62.1 22.2 42.6 02.9 03.9 64.4 25.0 85.8 46.8 07.9 69.3 43 83.3 43.6 43 43.0 03.0 63.1 23.2 86.8 47.8 84.3 44.6 04.9 65.4 26.0 09.0 70.4 44 44.0 04.0 64.1 24.2 44 87.9 71.4 45 85.3 05.9 66.4 27.1 48.8 10.0 45 45.0 05.0 65.1 25.2 45.6 88.9 28.1 72.4 46 46 46.0 06.0 66.1 26.2 86.3 46.6 07.0 67.4 49.8 11.0 73.4 47 87.3 89.9 5ó.8 12.0 67.1 27.2 47.6 08.0 68.4 29.1 47 47.0 07.0 51.9 13.1 74.5 48 30.1 90.9 48 08.0 68.1 28.2 88.3 48.6 09.0 69.5 48.0 52.9 75.5 31.1 49 70.5 91.9 14.1 49 49.0 09.0 69.1 29.2 89.3 49.6 10.0 50 50 50.0 110.0 170.1 230.2 290.3 350.6 411.0 471.5 532.1 592.9 653.9 715.1 776.5 77.5 51 51 12.0 72.5 33.1 93.9 54.9 16.1 31.2 91.3 51.6 51.0 11.0 71.1 55.9 52 95.0 78.6 13.0 73.5 34.1 17.1 52 72.1 32.2 92.4 52.6 52.0 12.0 74.5 53 73.1 96.0 18.2 79.6 80.6 53 53.0 13.0 33.2 93.4 53.6 14.0 35.1 57.0 58.0 54 54 54.0 74.1 34.2 94.4 54.6 15.0 75.5 36.2 97.0 19.2 14.0 55 76.5 98.0 81.7 55 15.0 55.6 37.2 59.0 20.2 55.0 75.1 35.2 95.4 16.0 82.7 56 56 38.2 60.0 21.2 56.0 16.0 76.1 36.2 96.4 56.6 17.0 77.5 99.0 83.7 57 58 78.5 39.2 600.0 22.3 57 37.2 18.0 61.0 57.0 17.0 77.1 97.4 57.6

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Min.	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	Min.
0	786.8		910.5			1098.2		1225.1	1289.2				0
I	87.8 88.8	49.5 50.5	11.5	73.8 74.8	36.3	99.3 1100.3	62.5 63.6	26.2 27.3	90.3	54.8 55.8	19•7 20·8	85. ₂ 86. ₃	1 2
3	89.9	51.6	13.6	75.9	38.4	01.4	64.7	28.3	92.4	56.9	21.9	87.3	3
4 5	90.9	52.6	14.6	76.9	39.5	02.4	65.7	29.4	93.5	58.0	23.0	88.4	4
6	91.9	53.6 54.7	15.7	78.0 79.0	40.5 41.6	o3.5 o4.5	66.8 67.8	30.4 31.5	94.5 95.6	59.0 60.1	24·1 25·1	89.5 90.6	5 6
	94.0	55.7	17.7	80.0	42.6	05.6	68.9	32.6	96.7	61.2	26.2	91.7	7
7 8	95.0	56.7	18.8	81.1	43.7	06.6	70.0	33.6	97.8	62.3	27.3		
9	96.0		19.8	82.1	44.7	07.7	71.0	34.7	98.8	63.4	28.4	, ,	
10	797.0 98.1	858.8 59.8	920.8	983.2	46.8		73.1	1235.8 36.8	1299.9 1301.0	1364.5 65.6	30.6	1495.0 96.1	
11	99.1	60.9	22.9	85.2	47.9	10.8	74.2	37.9		66.6	31.7		
	800.1	61.9	23.9	86.3	48.9		75.2	39.0	03.1	67.7	32.8	98.3	13
14		62.9 64.0	25.0 26.0	87.3 88.4	49·9 51·0	12.9	76.3 77.4	40.0 41.1	04.2 05.3	68.8 69.9	33.9	99.4	
16	_		27.0	89.4	52.0		78.4	42.2	06.3	70.9	36.0		
17		66.0	28.1	90.4	53.1	16.1	79.5	43.2	07.4	72.0		02.7	
18	1	67.1	30.1	91.5 92.5	54.1 55.2	17.1	80.5 81.6	44.3 45.4	08.5 09.6	73.1 74.2	38.2 39.3		
-	807.3							1243.4	1		_		1
21	1		32.2	94.6	57.3	20.3	83.7	47.5	11.7	76.4			
22		, ,	33.3	95.6	58.3	1	84.8	48.6	12.8	77.4		08.2	22
23 24	1 .	72.2 73.2	34.3 35.3	96.7 97.7	59.4 60.4	22.4	85.8 86.9	49.6 50.7	13.8 14.9	78.5 79.6	43.7 44.8		1 .
25		74.3		98.8	61.4	24.5	88.0	51.8	16.0	80.7			
26		75.3	37.4	99.8	62.5	25.5	89.0	52.8	17.1	81.8			1
27 28		76.3 77.4		8.0001	63.5 64.6	26.6 27.6	90.1	53.9 55.0	18.1	82.8			
29	0.0	1 / / .		02.9	65.6		92.2	56.0	20.3				
					1066.7	1129.7		1257.1					
3 ₁		l	42.6	05.0	67.7 68.8	30.8 31.8	94.3	58.2 59.2	22.5 23.5				
33				07.1	69.8				24.6		1 -		
34				08.1	70.9			61.4	25.7				
35				09.2	72.0 73.0		98.5	62.4 63.5	26.7 27.8		56.7		
37		86.7	48.8	11.3	74.1	37.2	1200.7	64.6	28.9	93.7	58.9		
38	1		49.9	12.3	75.1			65.6	30.0	94.8 95.8	60.0		
39	1	1	1		76.2	1 1		1267.8	1	-	1	1 1	1
40					78.3	41.4		68.8					
42	29.9	91.8	54.0	16.5	79.3	42.4	06.0	69.9		99.1	64.4	30.2	42
43				17.5	80.4 81.4			71.0		01.3			43
45								1 ' ^	37.5		1 -	33.5	44
46		96.0	58.2	20.6	83.5	1	10.2	74.2	38.6	03.4	68.8	34.6	46
47						47.7			39.7			1 1	47
49													
				1024.8	1087.7			1278.5			1473.1		
51						1				1	·		
53	41.3	03.2	65.5	28.0		54.1	17.7	81.7	46.1	11.0		42.3	53
54									47.2		77.5	43.4	54
55					93.0		1	1	48.3				
5	45.4	07.4	69.6	32.2	95.1	58.3	21.9	86.0	50.4	15.4	80.8	46.7	57
58						1 -		1					58
50	47.5	09.4	71.7	34.3	97.2	60.4	24.1	88.1	52.6	17.5	83.0	48.9	109

	LATITUDE.											
Min.	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	Min.
0		1616.5										0
I 2	51.1 52.2	17.6 18.7	84.6 85.8	52.3 53.4	20.6 21.7	89.5	59.2 60.4		2100.7			
3	53.3	19.8	86.9	54.6	22.9	91.9			03.1		48.0	
4	54.4	20.9	88.0	55.7	24.0	93.0	62.7	33.1	04.3			
5	55.5	22.0	89.1	56.8	25.2	94.1	63.9					
6	56.6 57.7	23.2 24.3	90.3 91.4	58.0 59.1	26.3 27.5	95.3 96.5	65.0 66.2	35.5 36. ₇				1
7 8	58.8	25.4	92.5	60.2	28.6	97.6		37.8	09.1			7 8
9	59.9	26.5	93.6	61.4	29.7	98.8	68.5	39.0	10.3	82.4	55.3	
10	1561.0 62.1	1627.6 28.7	1694.8 95.9	1762.5 63.6	1830.9	1899.9	1969.7	2040.2 41.4		2183.6 84.8	2256.5 57.8	10
11	63.2	29.8	97.0	64.8		02.3						
13	64.4	31.0	98.1	65.9	34.3	03.4						
14	65.5	32.1	99.3	67.0		04.6						
15	66.6		1700.4	68.2	36.6	05.7						
16	67.7 68.8	34.3 35.4	01.5	69.3 70.5	37.8 38.9	06.9 08.1		47.3 48.5		90.8		16
17	69.9	36.5	03.8	71.6		09.2	79.1	49.7				18
19	71.0	37.6	04.9	72.7	41.2	10.4	80.2	50.8	.22.2	94.4	67.5	19
20		1638.8	1706.0	1773.9		1911.5		2052.0	2123.4		2268.8	20
21	73.2	39.9	07.1	75.0	43.5	12.7	82.6	53.2			70.0	1
22	74.3	41.0	08.3	76.1	44.6 45.8	13.8 15.0					71.2 72.5	
23	75.4	42.1	10.5	77·2 78·4	46.9	16.2	86.1	56.8		2200.5	73.7	24
25	77.6	44.3	11.6	79.5	48.1	17.3						
26	78.7	45.5	12.8	80.6		18.5	88.4					l .
27	79.8	46.6	13.9		50.4	19.6				1	77.4	
28	80.9 82.1	47·7 48·8	15.0 16.1	83.o 84.1	51.5 52.7	20.8		61.5 62.7	33.0 34.2		78.6 79.8	28 29
30		1649.9			· ·	•		,			,,	1 1
31	84.3	51.0	19.4	86.4	55.0	24.3	94.3	65.1	36.6	09.0	82.3	31
32	85.4		19.5	87.5	56.1	25.4		66.2			83.5	32
33	86.5	53.3	20.7	88.6		26.6						
34	87.6	54.4	21.8	89.8	58.4	27.8 28.9	97.8					
35	88.7	55.5 56.6	22.9 24.0	90.9	59.6 60.7		99.0	71.0	1 1 1		88.4	
37	90.9		25.2	93.2	61.9	31.3		72.2	43.8		89.7	37
38	92.0	58.9	26.3	94.3		32.4	02.5			1 -	90.9	
39	93.1	60.0	27.4	95.5	64.2	33.6	'	74.5	i	· ·	92.1	1
40	1594.3	1661.1 62.2	1728.6 29.7		1865.3 66.5	1934.7 35.9	2004.9	2075.7 76.9	48.6	2219.9	94.6	40 41
42	96.5	63.4	30.8					78.1	49.8			42
43	97.6		31.9	1800.0	68.8			1 2 2	51.0			43
44	98.7	65.6	33.1	01.2					1			44
45	99.8	66.7	34.2 35.3	02.3 03.5	71.1 72.2	40.5			53.4 54.6	27.2	99.5 2300.7	45
46	02.0	67.8 69.0	36.5			42.9		84.0		28.5	02.0	
48	03.1		1	05.7	74.5	44.0	1		57.0	29.7		
49	04.2	71.2	38.7		75.7	45.2	1		l	,		1
50 51	1605.4 06.5	1672.3				1946.4 47.5	2016.6 17.8	2087.6 88.8	2159.4	2232.1 33.3	2305.7	50 51
52	07.6		42.1									52
53	08.7		43.2		80.3	49.9	20.2	91.2	63.1	35.8		
54	09.8	76.8	44.4	12.6								
55	10.9					52.2 53.4						
56	13.1				1							
58	14.2					55.7	26.0	97.1	69.1	41.9	15.5	58
59	15.4							98.3	70.3	43.1	16.8	59

	LATITUDE.											
Min	36°	37°	38°	39°	40°	41°	42°	43°	44°	45°	46°	Min.
0			2468.3									Э
1 2	20.5	93.9		46.2			83.1 84.4	64.5 65.8				I
3	21.7	96.4	72.1	48.8	1						19.9	3
4	23 0	97.7	73.4				87.1	68.5				4
5	24 2	98.9	74.6	51.4	29.2							5
6		2400.2		52.7	36.5	09.6	89.8	71.3		38.4	24.2	6
7 8	26.7	01.4	77.1	54.0		10.9		72.7	55.6	39.8	25.7	7 8
8	27.9	02.7	78.5 79.7	55.3 56.6	33. ₂ 34.5	12.2	92.5	74.1 75.4	57.0 58.3			8
10		-		1	i .		1			1 ' '	3130.0	1 -
II	31.6	06.4	82.2	59.1	37.1	16.2	96.5	78.2	61.1	45.5	31.5	1.1
12	32.9		83.5	60.4		17.5	97.9		62.5			12
13	34.1	09.0	84.8	61.7				80.9				13
14	35.3	10.2	86.1	63.0			2800.6					
15	36.6	11.5	87.4			J	02.0				37.2	15
16	37.8	12.7	88.6	65.6 66.9	r : .		03.3					ŀ
17 18	39.0 40.3	15.2	89.9 91.2	68.2	44.9 46.3	24.2 25.5	04.7					17
19	41.5	16.5	92.4		47.6		07.3					
20			2493.7					2890.5				20
21	44.0	19.0	95.0	72.0	50.2		10.1	91.9	75.1			
22	45.3	20.3	96.3	73.3		30.8			76.5	(47.4	22
23 24	46.5	21.5	97.6 98.8	74.6 75.9	52.8 54.1		12.8	94.7	77.9	62.6		23
25	47·7 49·0		2500.1	77.9								24 25
26	50.2	25.3	01.4		56.8		16.8				53.2	26
27	51.5	26.5	02.7	79.8		37.5		2900.2	83.5			27
28	52.7	27.8	03.9	81.1	59.4		19.5	01.5			1 - 1	28
29	54.0	29.1	05.2	82.4	60.7	40.2	20.9	02.9	86.3	71.1	57.5	29
30 31	2355.2 56.5	2430.3 31.6	2506.5 07.8	2583.7 85.0	2662.0 63.3		2822.3 23.6	2904.3 05.7		3072.6 74.0	3159.0 60.4	3o 31
32	57.7	32.9	09.0		64.6		25.0		90.5	75.4		32
33	58.9	34.1	10.3	87.6	66.0		26.3	08.4	91.9		63.3	33
34	60.2	35.4	11.6	88.9			1	09.7	93.3	78.3	64.8	34
35	61.4	36.7	12.9	90.2	68.6		29.0	11.2	94.7	79.7	66.2	35
36	62.7	37.9		91.5	69.9		30.4	12.6	96.1	81.1	67.7	36
37	63.9	39.2	15.4	92.8	71.2	50.9		14.0	97.5	82.6	69.1	37
38	65.2	40.4	16.7	94.1	72.5	52.2	33.1	15.3	98.9	84.0	70.6	38
39	66.4	41.7	18.0	95.4	73.9		34.5		3000.3	85.4	72.0	39
40 41	68.9	44.2	2519.3 20.5	98.0	76.5	56.2	37.2	19.5	03.2	88.3	75.0	40 41
42	70.2	45.5	21.8	99.3	77.8	57.6	38.6	20.9	04.6	89.7	76.4	42
43	71.4	46.8		2600.5	79.1	58.9	39.9	22.3	06.0	91.2	77.9	43
44	72.6	48.0	24.4	01.9	80.5	60.2	4í.3	23.6	07.4	92.6	79.3	44
45	73.9	49.3	25.7	03.2	81.8	61.5	42.6	25.0	08.8			
46	75.1	5ó.6	27.0	04.5	83.1		44.0	26.4	10.2	95.5	82.3	46
47	76.4	51.8	28.3	05.8	84.4		45.4	27.8	11.6	96.9	83.7	47
48	77.6 78.9	53.1 54.3	29.5 30.8	07.1 08.4	85.7 87.1	65.6 66.9	46.7 48.1	29.2 30.6	13.0 14.4	98.3	85.2 86.6	48
49 50	1 1		2532.1			•			- 1	99.7	- 1	49
51	81.4	56.9	33.4	11.0	89.7	69.6	50.8	33.3	17.2	02.6	89.6	50 51
52	82.6	58.1	34.7	12.3	91.0	71.0	52.2	34.7	18.7		91.0	52
53	83.9	59.4	36.0	13.6	92.3	72.3	53.5	36.1	20.1	o5.6	92.5	53
54	85.1	60.7	37.2	14.9	93.7	73.7	54.9	37.5	21.5	07.0	94.0	54
55 56	86.4	61.9	38.5	16.2	95.0	75.0	56.3	38.9	22.9	08.4	95.4	55
56 57	87.6 88.9	63.2 64.5	39.8 41.1	17.5 18.8	96.3	76.3	57.7	40.3	24.3	09.8	96.9	56
58	90.2	65.8	42.4	20.1	97.6 99.0	77·7 79·0	59.0 60.5	41.7 43.1	25.7 27.1	11.2	98 .4 99. 8	57 58
59	91.4	67.0	43.6		2700.3		61.7	44.4	28.5		3201.3	59
-9	7***	57.0	70.0		_,50.0	50-4		44.4	20.0	14.1	020100	٠,

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					LA	riru	DE.					
Min.	47°	48°	49°	50°	51°	52°	53°	54°	55°	56°	57°	Min.
0		3291.5	3382.1									0
I	04.2	93.0	83.6	76.0	70.4	66.8	65.4	66.3	69.7	75.7	84.5	1
2	05.7	94.5	85.1	77.6	72.0	68.4	67.1	68.0	71.5	77.5	86.3	2
3	07.1	96.0	86.7	79.1	73.6	70.1	68.8	69.7	73.2	79.3	88.1	3
4	08.6	97.5	88.2	80.7	75.2	71.7	70.4	71.5	75.0	81.1	90.0	4
5	10.1	99.0	89.7	82.3	76.8	73.3	72.1	73.2	76.7	82.9	91.8	5
6		3300.5	91.3	83.8	78.4	75.0	73.7	74.9	78.4	84.7	93.7	6
7 8	13.0	02.0	92.8	85.4	79.9	76.6	75.4	76.6	80.2	86.4	95.5	78
8	14.5	03.5	94.3	87.0	81.5	78.2	77.1	78.3	82.0	88.2	97.3	8
9	15.9	05.0	95.8	88.5	83.1	79.8	78.7	80.0	83.7	90.0	99.2	9
10	3217.4	3306.5	3397.4	3490.1	3584.7	3681.5	3780.4	3881.7	3985.4	4091.8	4201.0	10
11	18.9	08.0	98.9	91.6	86.3	83.1	82.1	83.4	87.2	93.6	02.9	11
12	20.3	09.5	3400.4	93.2	87.9	84.7	83.7	85.1	88.9	95.4	04.7	12
13	21.8	11.0	02.0	94.7	89.5	86.4	85.4	86.8	90.7	97.2	06.6	13
14	23.3	12.5	03.5	96.3	91.1	88.0	87.1	88.5	92.5	99.0	08.4	14
15	24.8	14.0	05.0	97.9	92.7	89.6	88.8	90.2		4100.8	10.3	15
16	26.2	15.5	06.6	99.4	94.3	91.3	90.4	92.0	96.0	02.6	12.1	16
17	27.7	17.0		3501.0	95.9	92.9	92.1	93.7	97.7	04.4	14.0	17
18	29.2	18.5	09.6	02.6	97.5	94.5	93.8	95.4	99.5	06.2	15.8	18
19	30.7	20.0	11.1	04.1	99.1	96.2	95.5		4001.2	08.0	17.7	19
- 1	1 1					'	,					
20				3505.7								20
21	33.6	23.0	14.2	07.3	02.3	99.4		3900.5	04.7	11.6	21.4	21
22	35.1	24.5	15.7	08.8		3701.1		02.2	06.5	13.4	23.2	22
23	36.6	26.0	17.3	10.4	05.5	02.7	02.2	04.0	08.3	15.2	25.1	23
24	38.0	27.5	18.8	12.0	07.1	04.4	03.8	05.7	10.0	17.1	27.0	24
25	39.5	29.0	20.4	13.5	08.7	06.0	05.5	07.4	11.8	18.9	28.8	25
26	41.0	30.6	21.9	15.1	10.3	07.6	07.2	09.1	13.5	20.7	30.6	26
27	42.5	32.1	23.5	16.7	11.9	09.3	08.9	10.8	15.3	22.5	32.5	27
28	44.0	33.6	25.0	18.3	13.6	10.9	10.5	12.5	17.1	24.3	34.4	28
29	45.4	35.1	26.5	19.8	15.1	12.6	12.2	14.3	18.8	26.1	36.2	29
3о	32/6.0	3336.6	3428.0	3521.4	3616.7	3714.2	3813.0	3016.0	4020.6	4127.0	4238.1	30
31	48.4	38.1	29.6	23.0	18.4		15.6	17.7	22.4	29.7	40.0	3 r
32	49.9	39.6	31.1	24.6	20.0	17.5	17.3	19.4	24.1	31.5	41.8	32
33	51.4	41.1	32.7	26.1	21.6	,	18.9	21.2	25.9	33.3	43.7	33
34	52.8	42.6	34.2	27.7	23.2	20.8	20.6	22.9	27.7	35.2	45.5	34
35	54.3	44.1	35.8		24.8	22.4	22.3		29.4	_	47.4	35
	55.8	1 1 1			26.4		24.0	26.3	31.2	38.8	49.3	36
36		45.7	1	32.4	28.0		25.7		33.0		51.1	37
37	57.3	47.2	1				٠.					38
38	58.8	48.7			29.6			29.8	34.8	42.4		
39	60.3	50.2	1	1	31.3	,	29.1	31.5	36.5	44.2	54.9	39
40	3261.7	3351.7		3537.1					4038.3	4146.1		40
41	63.2	53.2			34.4		1		40.1	47.9	58.6	41
42	64.7	54.7	46.6	40.3	36.1			36.7	41.8	49.7	60.5	42
43	66.2	56.2	48.1	41.9	37.7			38.4	43.6	51.5	62.3	43
44	67.7	57.8	49.7	43.5	39.3	37.3			45.4		64.2	44
45	69.2	59.3	51.2	45.0	40.9	38.9	39.2	41.9	47.2	55.2	66.1	45
46	70.7			46.6	42.5	40.6			49.0	57.0	68.0	46
47	72.1			48.2	44.1	42.2	42.6	45.4			69.8	47
48	73.6	63.8			45.8							48
49	75.1	65.4										
50	1 -	3366 0	3/58 0	3553.0	3640 0	37/7.2	38/7.7	3050.6	/o56.1	116/.3	1275.5	50
5 i	78.1					48.8			57.8	66.1	77.4	-
52												
53	79.6									1		53
54	82.6					1						
55	84.1								11			
56	85.6									.,	1 00 0	
57	87.1								. 1			
58	88.5	1 : .						1				
59	90.0											

			-		LA	TITU	DE.					
Min.	58°	59°	60°	61°	62°	63°	64°	65°	66°	67°	68°	Min.
0 1 2	4294.3 96.2 98.1	4409.1 11.1 13.0	4527.4 29.4 31.4	51.3	77.1	07.1	41.7	81.2	26.0	76.6		0 I 2
3 4	4300.0	15.0	33.4	55.4	81.4	11.6	46.3	85.9	30.9	81.7	38.8 41.5	3 4
5 6	03.7 05.6 07.5	18.9 20.8 22.8	37.4 39.4 41.4			18.2	53.1	93.1	38.3	89.4	46.9	5 €
7 8 9	09.4	24.7		65.8	92.1	22.6	57.7	97.8 5200.2	43.2	94.5	52.3	8
10 11 12	15.1	4428.6 30.6 32.5	4547.4 49.4 51.4	72.0	4796.3 98.5 4800.6	29.2	64.6	04.9	50.7	5502.3		11
13	17.0 18.9 20.8	34.5 36.4	53.5 55.5	76.1 78.2	02.8	33. ₇ 35. ₉	69.2 71.5	09.7	55.6 58.1	07.4	65. ₇ 68. ₄	13 14
15	22.7 24.6 26.5	38.4 40.3 42.3	57.5 59.5 61.5	80.3 82.4 84.5	07.1 09.2 11.4	40.3	76.1	16.9	63.1	15.2	73.8	15 16
18	28.4 30.3	44.2 46.2	63.5 65.6	86.5 88.6	13.5 15.7	44.8 47.0	80.7 83.0	21.6	68.0 70.5	20.4 23.0	79.2 81.9	18
20 21 22	4332.2 34.1 36.0	4448.2 50.1 52.1	4567.6 69.6 71.6	92.8	20.0	51.5	87.6	28.8	75.5	28.1		1
23 24 25	37.9 39.8 41.8	54.1	73.6 75.7	97.0	24.3	55.9 58.2	92.3 94.6	33.6 36.0	83.0	33.3 35.9	92.7 95.5	23 24 25
26 27 28 29	43.7 45.6 47.5 49.4	61.9	79.7 81.7	o3.2 o5.3	30.8 32.9 35.1 37.3	64.9 67.1	99.2 5101.5 03.8	40.8 43.2	90.5	43.8 46.4	06.3	26 27 28 29
30 31	4351.3 53.2	4467.8 69.8	4587.8 89.9	4711.6 13.7	4839.4 41.6	4971.6 73.8	5108.5 10.8	52.9	5398.0 540 0. 5	5551.6 54.2	5711.8 14.5	30 31
32 33 34	55.1 57.1 59.0	71.8 73.7 75.7	93.9 96.0	17.9 20.0	45.9 48.1	78.3 80.6	15.5 17.8	57.7 60.1	o5.5 o8.1	59.4 62.1	20.0	33 34
35 36 37 38	60.9 62.8 64.7 66.7	77·7 79·7 81.6 83.6	4600.0 02.1	22.1 24.2 26.3 28.4	52.4 54.6	85.1 87.3 89.6	22.4 24.8 27.1	67.4	13.1 15.6		28.2 30.9	35 36 37 38
39	68.6 4370.5	85.6 4487.6		30.5 4732.6	59.0 4861.1	4994.1	5131.8		20.6 5423.2	75.2 5577.8	36.4 5739.2	39 40
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26	67.8	42.7	26.5	20.0	24.5	41.3	72.2	19.2	84.7	71.9	84.7	26
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38	5902.2	78.8	64.3	60.0	66.8	86.3					50.8	38
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57	57.2					58.8	97.7	53.9 58.3	30.2	1		57
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In computing compound interest for long periods of time, it is necessary to have the following logarithms to more than six places.

Number.	Logarithm.	Number.	Logarithm.
1.0025	.00108 43813	1.0425	,01807 60636
1.0050	.00216 60618	ì.0450	.01911 62904
1.0075	.00324 50548	1.0475	.02015 40316
1.0100	.00432 13738	1.0500	.02118 92991
1.0125	.00539 50319	1.0525	.02222 21045
1.0150	.00646 60422	1.0550	.02325 24596
1.0175	.00753 44179	1.0575	.02428 03760
1.0200	.00860 01718	1.0600	.02530 58653
1.0225	.00966 33167	1.0625	.02632 89387
1.0250	.01072 38654	1.0650	.02734 96078
1.0275	.01178 18305	1.0675	.02836 78837
1.0300	.01283 72\$47	1.0700	.02938 37777
1.0325	.01389 00603	1.0725	.03039 73009
1.0350	.01494 03498	1.0750	.03140 84643
1.0375	.01598 81054	1.0775	.03241 72788
1.0400	.01703 33393	1.0800	.03342 37555

NUMBERS OFTEN USED IN CALCULATIONS.

		Logarithms.
Circumference of a circle to diameter 1)		
Surface of a sphere to diameter 1	3.1415926	0.497150
Area of a circle to radius 1		
Area of a circle to diameter 1	.7853982	9.895090
Capacity of a sphere to diameter 1	.5235988	9.718999
Capacity of a sphere to radius 1	4.1887902	0.622080
$1 \div 3.1415026$	0.3183099	9.502850
Arc equal to radius expressed in degrees5	7°.2957795	1.758123
Arc equal to radius expressed in seconds	205264".8	5.314425
Length of 1 degree in parts of radius	.0174533	8.241877
Length of 1 minute in parts of radius	.0002909	6.463726
Sine of 1 second	.00000485	4.685575
Sine of 2 seconds	.00000970	4.986605
Sine of 3 seconds.	.00001454	5.162696
Sine of 4 seconds.	.00001939	5.287635
Sine of 5 seconds =	.00002424	5.384545
Sine of 6 seconds	.00002000	5.463726
Sine of 7 seconds	.00003394	5.530673
Sine of 8 seconds ==	.00003879	5.588665.
Sine of 9 seconds.	.00004363	5.639817
Base of Napier's system of logarithms	2.7182818	0.434294
Modulus of the common logarithms	.4342945	9.637784
360 degrees expressed in seconds	1296000	6.112605
24 hours expressed in seconds.	86400	4.936514
Number of feet in one mile	5280	3.722634

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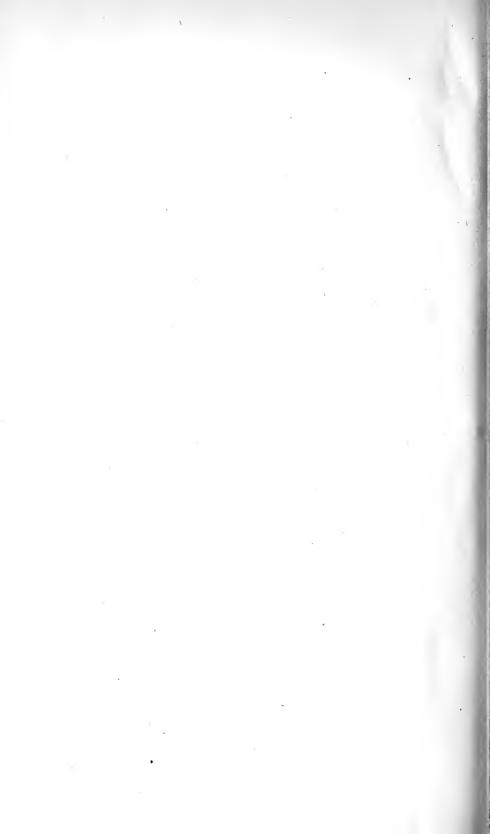
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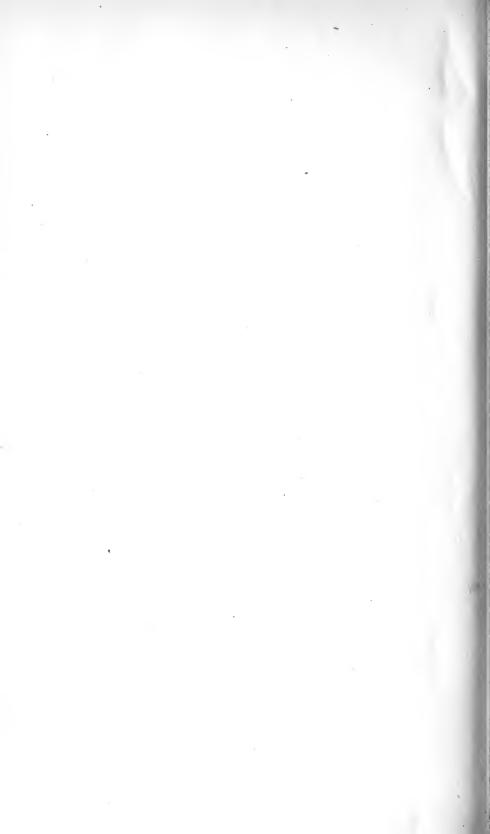
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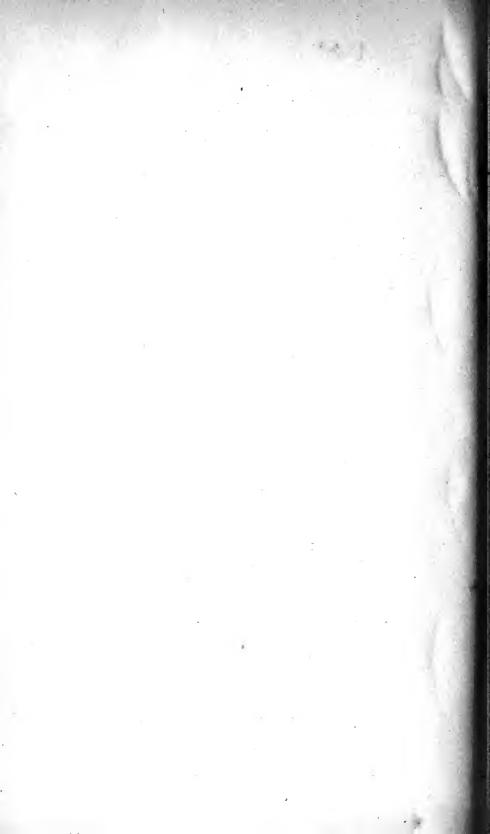
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